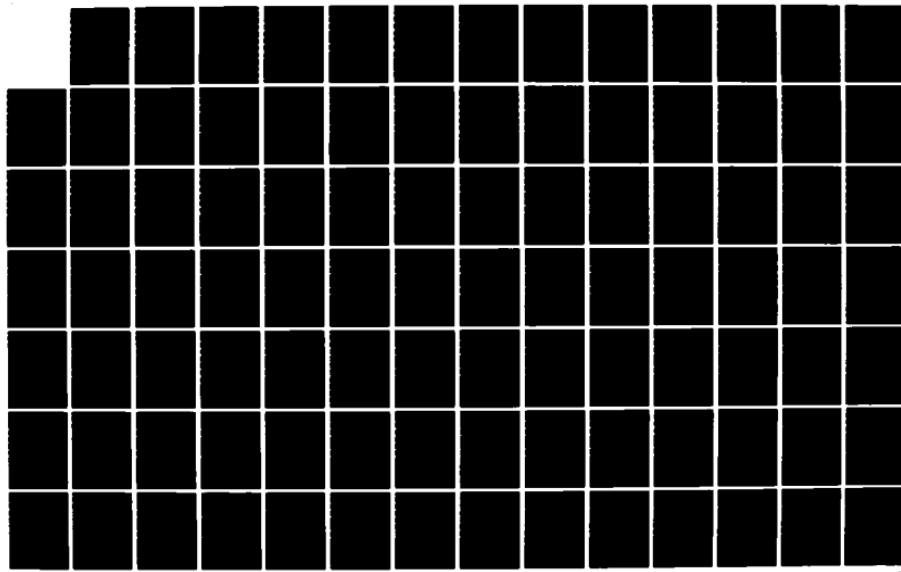
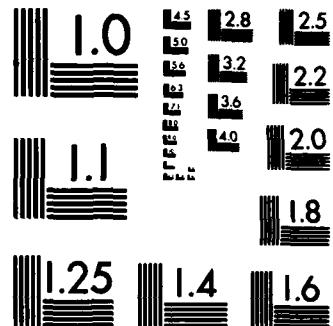


AD-A153 206 SURVEILLANCE REPORT STAGE I DISSECTED MOTORS/
PROPELLANTS MOTOR NUMBER 00. (U) OGDEN AIR LOGISTICS
CENTER HILL AFB UT PROPELLANT ANALYSIS LA.
UNCLASSIFIED J A THOMPSON MAR 85 MANPA-503(85) 1/2

F/G 21/8.2 NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

AD-A153 206

HEADQUARTERS
OGDEN AIR LOGISTICS CENTER
UNITED STATES AIR FORCE
HILL AIR FORCE BASE, UTAH 84056-5149

**SURVEILLANCE REPORT
STAGE I
DISSECTED MOTORS/PROPELLANTS
MOTOR NUMBER 0012199
PHASE XV**

PROPELLANT ANALYSIS LABORATORY

**MANPA REPORT NR
503(85)**

MARCH 1985

APR 29 1985

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MANPA REPORT NR 503(85)
MMWRM PROJECT M46288C

SURVEILLANCE REPORT
STAGE I DISSECTED MOTORS
PHASE XV PROPELLANT & COMPONENT TESTING

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March 1985

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ABSTRACT

Testing was performed to determine the useful shelf/service life for LGM-30, Stage I Rocket Motors. A three year storage program for propellant and components was started in May 1961. This program was then extended to a ten year study and later continued indefinitely to assure that a deterioration in motor physical characteristics could be detected in time to take some corrective actions before the weapon system performance deteriorated below an acceptable level.

This report covers propellant test data for motor S/N 0012199. Planned dissection of selected motors in the future will provide samples for continued component testing.

The data is presented in the form of regression analysis and the trends are projected 24 months beyond the last test date.

From the statistical analysis of all data tested to date, significant degradation of the propellant does not appear likely for at least two years past the oldest data point.

Future testing and reporting will be conducted on individual dissected motors.

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GLOSSARY OF TERMS AND ABBREVIATIONS

Aging Trend	A change in properties or performance resulting from aging of material or component
CSA	Cross Sectional Area
DB	Dogbone
Degradation	Gradual deterioration of properties or performance
E	Modulus (psi), defined as stress divided by strain along the initial linear portion of the curve.
EB	End Bonded
EGL	Effective Gage Length
em	Strain at maximum stress
er	Strain at rupture
"F" ratio	The ratio of the variance accounted for by the regression function to the random unexplained variance. The regression function having the most significant "F" ratio is used for plotting data. The ratio is also used in detecting significant changes in random variation between succeeding time points
JANNAF	Joint Army, Navy, NASA, Air Force Committee
MANPA	Propellant Lab Section at Ogden Air Logistics Center
Ogden ALC	Ogden Air Logistics Center, Air Force Logistics Command
r or R	The Correlation Coefficient is a measure of the degree of closeness of the linear relationship between two variables
Regression Equation	The general form of the regression equation is $Y = a + bx$
Regression Line	Line representing mean test values with respect to time
S_b	Standard error of estimate of the regression coefficient

GLOSSARY OF TERMS AND ABBREVIATIONS (cont)

S _e or S _{y,x}	Standard deviation of the data about the regression line
S _m	Maximum Stress
S _r	Stress at rupture
Standard Deviation (S _y)	Square root of variance
Strain Rate	Crosshead speed divided by the EGL
"t" test	A statistical test used to detect significant differences between a measured parameter and an expected value of the parameter (determines if regression slope differs from zero at the 95% confidence level)
Variance	The sum of squares of deviations of the test results from the mean of the series after division by one less than the total number of test results
3 Sigma Band	The area between the upper and lower 3 sigma limit. It can be expected that 99.73% of the inventory represented by the test samples would fall within this range assuming that the population is normally distributed.
90-90 Band	It can be stated with 90% confidence that 90% of the inventory represented by the test samples would fall within this range assuming that the population is normally distributed

INTRODUCTION

A. PURPOSE:

This report contains test data from samples of LGM-30 Stage I, Wing II TP-H1011 propellant obtained from dissected motor S/N 0012199. Testing was performed by the Propellant Analysis Laboratory (MANPA) for the Minuteman Motor Engineers (MMGR) under Project M46288C. This report is the fifteenth in this series. Data from this test period and propellant test data from the fourteen previous reports, for motor S/N 0012199, were entered into the G085 computer for regression analysis. The regressions are shown in this report.

B. TEST PROGRAM:

The LGM-30 laboratory and component program includes the testing of materials used in the main case and main grain propellant. Table 1 outlines the test program.

C. HISTORICAL BACKGROUND:

In May 1961, Thiokol began a three year LGM-30 laboratory storage and test program to determine the rate of degradation with age for Stage I materials. During June 1962 and again in August 1963, additional samples were included. New samples were added in July and August 1964 when the surveillance test program was extended to ten years (Test Plan 0717-62-0967, 53-8). The samples added to the inventory in 1964 were considered to be a new population, but were combined in regression analysis with the three dissected motors.

The history of testing of these materials is found in MQQP Report Nos. 109A(67), 144(68), 208(71), MANCP Report Nr. 358(76) and MANPA Report Nr. 482(82). Physical transfer of the specimens from Thiokol to Ogden ALC was made in June 1967.

Until 1982, due to a limited number of dissected motor samples, data from all motors were combined for statistical analyses. In 1982, key LRS LA parameters were reported for individual motors (MANPA Report Nr. 470(82)).

STATISTICAL ANALYSIS

The objective of this statistical analysis is to determine the effect aging has on Stage I propellant from motor S/N 0012199. This analysis will assist Service Engineering in predicting Stage I serviceability.

The method used to accomplish this analysis was regression analysis. The linear equation $Y = a + bX$ was found to be the best fit model for this data. The unique mathematical regression equations are on the top of each plot. Each point on a regression plot represents a data mean value at its particular age at test. The sample sizes for the mean values may vary in the number of specimens tested at each test period. The sample size at a particular test period can be found in the Sample Size Summaries. All regressions are calculated on individual data values.

The variance about each regression trend line was used to compute a tolerance interval such that at 90% confidence 90% of the sample distribution will fall within this interval. This tolerance interval is extrapolated 24 months beyond the age of the last test date.

The 't' value and the significance of this statistic will be given as an indication of the "statistical significance" of the slope of the trend lines as it is compared to a line of zero slope. When a regression slope is labeled as significant, it should be noted that the slope of the trend line is significant from a statistical standpoint and a change over time is occurring. A significant indication does not necessarily mean that the change in test values obtained during testing is significant in regards to motor fleet operational performance.

In 1961, a program was undertaken to determine the rate of degradation for the propellant used in Stage I Minuteman Motors (TP-H1011). With the use of TP-H1011 propellant, obtained from dissected Stage I motors, a normal distribution population was assumed for each motor and the data from

three motors (0012099, 0012199, and STM 012) were statistically combined. The combined data has been analyzed using a multi-symbol regression program that displays unique plot codes for each motor. This method of data plotting allows a visual display of the overall relationship between motors and their relationship with the combined least squared aging trend line. The combined motor composite regressions indicate that data masking of individual motor trends may be inprocess and a closer investigation is required.

Each dissected motor will be individually analyzed using linear regressions. The individual motor regressions were then analyzed for compatibility using the Analysis of Covariance. At this time, using the 5% significance level, these three motors are not statistically combinable.

As previously recommended, each motor will be individually plotted and analyzed to eliminate errors and provide more accurate regressions.

This report contains data and analysis for motor S/N 0012199. The analysis will be based on this motor only. The regression summaries can be found in table 2. The three motor combined composite regression plots, which also included motor S/N 0012199, has also been included to allow a visual display of the overall relationship between motors (results can also be found in table 2). The combined motor regressions should not be used for any purpose other than visual display only.

The symbols used for each of the three motors are as follows:

0012099 = 0

0012199 = 1

STM-012 = S

TABLE 1
TEST PROGRAM

<u>Test</u>	<u>Conditions</u>	<u>Config- uration</u>	<u>Nr Specimen</u>	<u>Total Specimens</u>
Tensile, Low Rate	77°, 2 & 20 in/min	JANNAF Dogbone	5	40
Creep	77°, 10 & 12 lb Load	JANNAF Dogbone	3	24
Stress Relaxation	77°, 3 & 5% Strain	1/2"x1/2"x4"	3	24
Hardness	77°, Init & 10 sec	Dogbone Ends	5	40
HOE	77°	1/2"x3/8"x1"	5	40
DTA	77° Start	0.040" Wafers	3	12
Sol Gel	77°	1/2"x1/2"x1/2"	6	24
High Rate Tensile	77°, 1000 in/in/min	3/4" GL Dogbones	5	15
Triaxial High Rate	77°, 1000 in/in/min	3/4" GL Rail	3	9
Dynamic Response	77°, 70 gm ct. wt.	3.3"x.33"x690" Disc	3	9
Biaxial Constant Strain	77°	3/4" GL Rail	3	9
Tear Energy	77°F ± 2°	0.1"x1.18"x3"	8	16
Poisson's Ratio (Strain Dilatation) 10, 15, 20, 25, 30%	77°F ± 2°	0.50"x0.50"x4"	6	30

TEST RESULTS

Regression analysis is the method of evaluation used in the analysis of motor S/N 0012199 test results. The regressions are presented in this report. In addition, regressions for the three dissected motors combined are presented in this report for visual comparison only to motor S/N 0012199.

A. TENSILE:

1. Low Rate Tensile (2.0 in/min):

The strain at maximum stress and strain at rupture trend lines show a statistically significant gradual decrease (figures 1 and 3). Maximum stress, stress at rupture and modulus regression trend lines show statistically significant increases (figures 2, 4 and 5).

For the dissected motor relationship (combined data) the respective regressions are included (figures 1A thru 5A).

2. Low Rate Tensile (20.0 in/min):

Strain at maximum stress and strain at rupture trend lines show a statistically significant decrease (figures 6 and 8). Maximum stress, stress at rupture and modulus show a statistically significant increase in the trend line direction (figures 7, 9 and 10).

The combined regressions are shown in figures 6A through 10A.

3. High Rate Tensile (1000 in/in/min):

The strain at maximum stress regression trend line shows a statistically significant increase (figure 11). Strain at rupture, maximum stress and stress at rupture regressions show a non-significant trend line (figures 12, 13 and 14). A statistically significant decreasing trend line direction for modulus is seen in figure 15.

The combined respective regressions are shown in figures 11A thru 15A.

4. High Rate Triaxial Tensile at 600 psi (1000 in/in/min):

The maximum stress and stress at rupture regression trend lines show a statistically significant increase (figures 17 and 19). The remaining regressions have a non-significant trend direction (figures 16, 18 and 20).

The respective combined regressions are shown in figures 16A thru 20A.

B. CREEP:

All of the regressions for the ten pound load test demonstrates a non-significant trend direction (figures 21 thru 24).

For the 12 pound load test at 10, 20 and 1000 second testing, also demonstrate a non-significant trend direction (figures 25, 26 and 27).

The respective combined motor regressions are shown in figures 21A thru 27A.

C. STRESS RELAXATION:

The stress relaxation modulus for the 3% and 5% strains show a statistically significant trend in the increasing direction for 10, 50, 100 and 1000 seconds (figures 28 thru 35).

The respective combined motor data regressions are shown in figures 28A thru 35A.

D. CONSTANT STRAIN:

The regression trend line has a non-significant slope direction (figure 36).

The combined motor data regression is shown in figure 36A.

E. HARDNESS:

The Shore A 10 second hardness regression trend line has a non-significant direction (figure 37).

The combined motor data regression is shown in figure 37A.

F. TEAR ENERGY:

The tear energy regression shows a non-significant trend direction (figure 38).

The combined motor data regression is shown in figure 38A.

G. SOL GEL:

The crosslink density and percent extractables have significant positive direction trend lines (figures 39 and 40). The gel swell ratio (figure 41) shows a non-significant trend direction and the density has a statistically significant negative trend line direction (figure 42).

The respective regressions for the combined motor data are shown in figures 39A thru 42A.

H. HEAT OF EXPLOSION:

The trend line for the regression is non-significant (figure 43).

The respective regression for the combined motor data is shown in figure 43A.

I. BURNING RATE:

The burning rate at 500 psi test pressure shows a statistically significant increasing trend line direction (figure 44). The regression for the 1000 psi shows a non-significant trend line direction (figure 45).

The respective regressions for the burning rate combined motor data are shown in figures 44A and 45A.

J. FAILURE ENVELOPE:

The failure envelope for motor S/N 0012199 is shown in figure 46.

TABLE 2
REGRESSION TREND LINE SUMMARY

<u>Test</u>	<u>Motor 0012199</u>	<u>Composite Motor</u>
Low Rate Tensile, 77°F, 2.0 in/min		
Strain at Max Stress	S(-)	NS
Maximum Stress	S(+)	S(+)
Strain at Rupture	S(-)	NS
Stress at Rupture	S(+)	S(+)
Modulus	S(+)	NS
Low Rate Tensile, 77°F, 20.0 in/min		
Strain at Max Stress	S(-)	S(-)
Maximum Stress	S(+)	S(-)
Strain at Rupture	S(-)	S(-)
Stress at Rupture	S(+)	NS
Modulus	S(+)	NS
High Rate Tensile, 77°F, 1750 in/in/min		
Strain at Max Stress	S(+)	NS
Maximum Stress	NS	NS
Strain at Rupture	NS	S(-)
Stress at Rupture	NS	NS
Modulus	S(-)	S(-)
High Rate Triaxial Tensile, 77°F, 1750 CHS, 600 psi		
Strain at Max Stress	NS	S(+)
Maximum Stress	S(+)	S(+)
Strain at Rupture	NS	S(+)
Stress at Rupture	S(+)	S(+)
Modulus	NS	S(-)
Creep, 10 lb Load, 10 sec	NS	S(-)
20 sec	NS	S(-)
1000 sec	NS	S(-)
10,000 sec	NS	S(-)
Creep, 12 lb Load, 10 sec	NS	S(-)
20 sec	NS	S(-)
1000 sec	NS	S(-)
Stress Relaxation, 3% Strain, 10 sec	S(+)	S(+)
50 sec	S(+)	S(+)
100 sec	S(+)	S(+)
1000 sec	S(+)	NS
Stress Relaxation, 5% Strain, 10 sec	S(+)	S(+)
50 sec	S(+)	S(+)
100 sec	S(+)	S(+)
1000 sec	S(+)	NS

TABLE 2 (cont)

<u>Test</u>	<u>Motor 0012199</u>	<u>Composite Motor</u>
Constant Strain	NS	S(-)
Hardness, Shore A, 77° F, 10 sec	NS	S(-)
Sol Gel		
Crosslink Density	S(+)	NS
% Extractables	S(+)	S(+)
Weight Swell Ratio	NS	S(+)
Density	S(-)	S(-)
Heat of Explosion	NS	S(+)
Burning Rate, 500 psi	S(+)	NS
1000 psi	NS	S(-)

NS = Non-significant trend from a line of zero slope

+ = Significant slope in a positive direction

- = Significant slope in a negative direction

NOTE: All testing performed at the 5% significance level

SUMMARY

A. TENSILE, CREEP, STRESS RELAXATION AND CONSTANT STRAIN:

For those regressions where statistically significant trend line direction are seen, the changes are gradual and no problems are indicated. The propellant has shown less strain capability and higher tensile strength as the age increases.

B. HARDNESS AND CROSSLINK DENSITY:

The hardness and crosslink density is gradually increasing as the propellant ages. As the crosslinking continues, the propellant becomes more rigid. This correlates well with increasing hardness, decreasing strain and greater stress properties.

C. THERMAL AND COMBUSTION PROPERTIES:

From the analysis, the thermal properties are not undergoing any drastic changes at this time with respect to age.

CONCLUSIONS AND RECOMMENDATIONS

A. CONCLUSIONS:

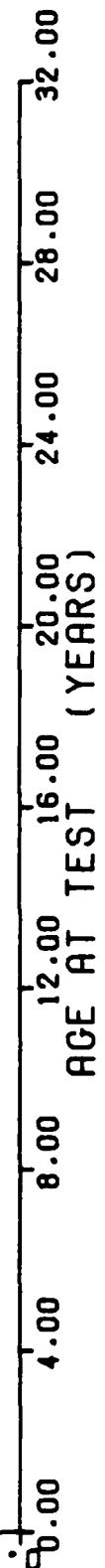
1. The test results show that, under present storage conditions, some of the physical and combustion properties of the propellant indicate statistically significant aging trends. However, where a significant trend is indicated, the slope of the trend line is gradual and no operational problems are expected for at least two years beyond the last test period.
2. Although some aging trends have been observed, it does not appear that significant degradation will occur in the propellant within the next two years.

B. RECOMMENDATIONS:

It is recommended that testing and reporting be continued on propellant from motor S/N 0012199 on an individual basis to eliminate the biasing created by combined motor regressions.

$F = +1.4608144E+01$ $Y = ((+2.6728386E-01) + (-1.3009801E-04) \cdot X)$
 $R = -3.4802401E-01$ $F = \text{SIGNIFICANT}$
 $\sigma_s = +3.8220602E+00$ $S_f = +1.6997176E-02$
 $N = 108$ $R = \text{SIGNIFICANT}$
 $Degrees of Freedom = 106$ $S_o = +3.4038714E-05$
 $N = \text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$ $S_r = +1.6009595E-02$
 $N = \text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

PARAMETER = STRAIN RT MAX STRESS
 UNIT OF MEASURE = IN/IN
 0.16 0.20 0.24 0.28 0.32 0.36



STAGE 1 DISSECTED MOTOR=0012199,LOW RATE CHS=2.0 IN/MIN,STRAIN MAX STRESS

Figure 1

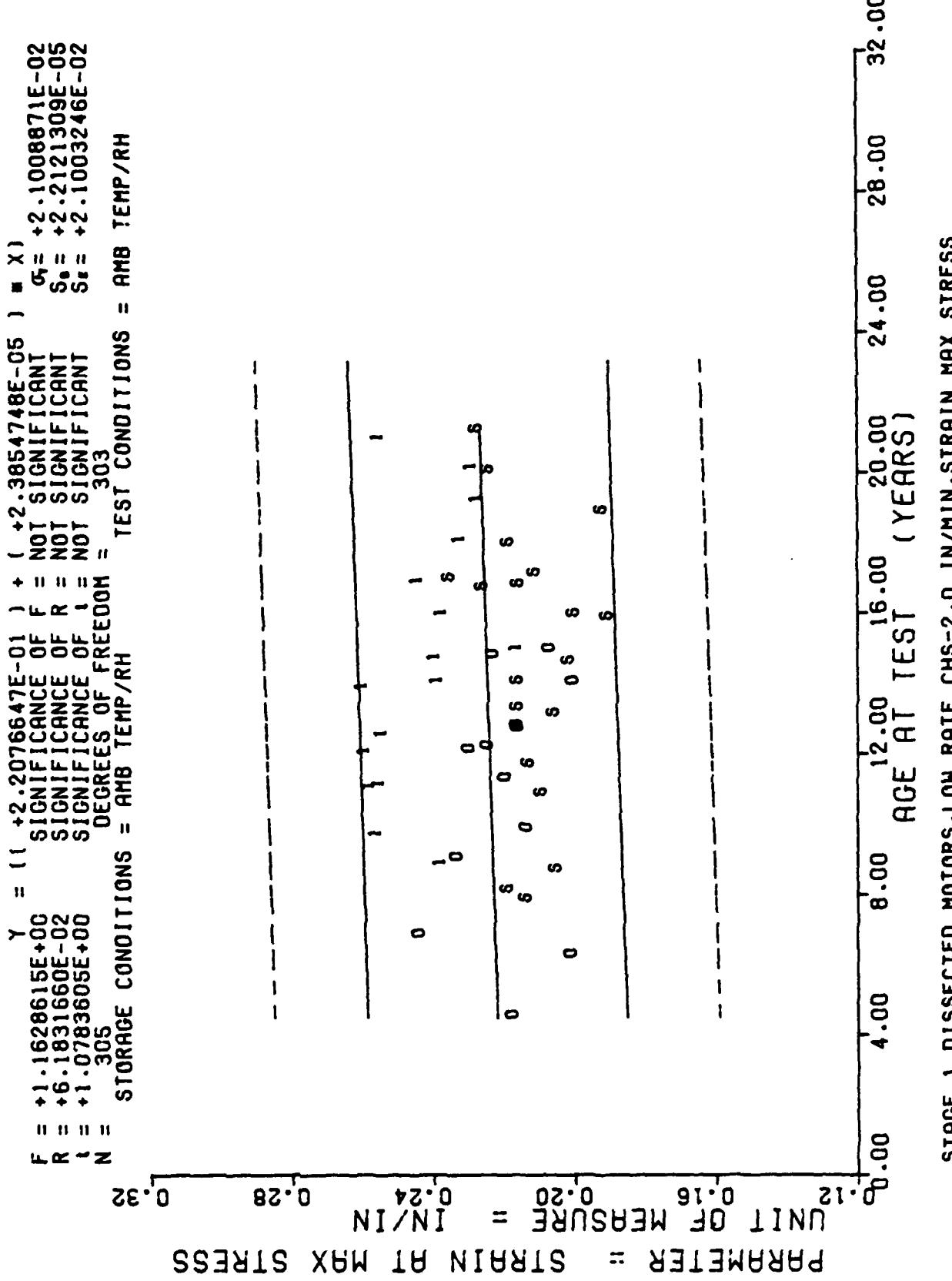


Figure 1A

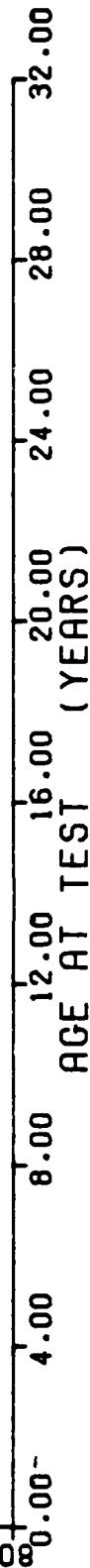
卷之三

MAX 35.1 DS
MIN 30.0 SATH

$F = +7.9689360E+00$
 $R = +2.6442768E-01$
 $I = +2.8229304E+00$
 $N = 108$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $Y = ((+1.2150543E+02) + (+4.9590511E-02) * X) / (+8.5272103E+00)$
 $S_r = +1.7567032E-02$
 $S_o = +8.2623886E+00$
 $S_t = +8.2623886E+00$
 $\text{DEGREES OF FREEDOM} = 106$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

PARAMETER = MAXIMUM STRESS
 UNIT OF MEASURE = PSI
 80.00 100.00 120.00 140.00 160.00 180.00

- 16 -



STAGE 1. DISSECTED MOTOR=0012199 LOW RATE CHS=2.0 IN/MIN. MAXIMUM STRESS.

Figure 2

$F = +7.7767004E+00$ $\gamma = ((+1.1791568E+02) + (+2.9494624E-02) \times X)$
 $R = +1.5818797E-01$ SIGNIFICANCE OF F = SIGNIFICANT
 $S_0 = +1.0576578E-02$ SIGNIFICANCE OF R = SIGNIFICANT
 $S_L = +1.0042013E+01$ SIGNIFICANCE OF t = SIGNIFICANT
 $t = +2.7886736E+00$ DEGREES OF FREEDOM = 303
 $N = 305$ TEST CONDITIONS = AMB TEMP/RH
 $N =$ STORAGE CONDITIONS = AMB TEMP/RH

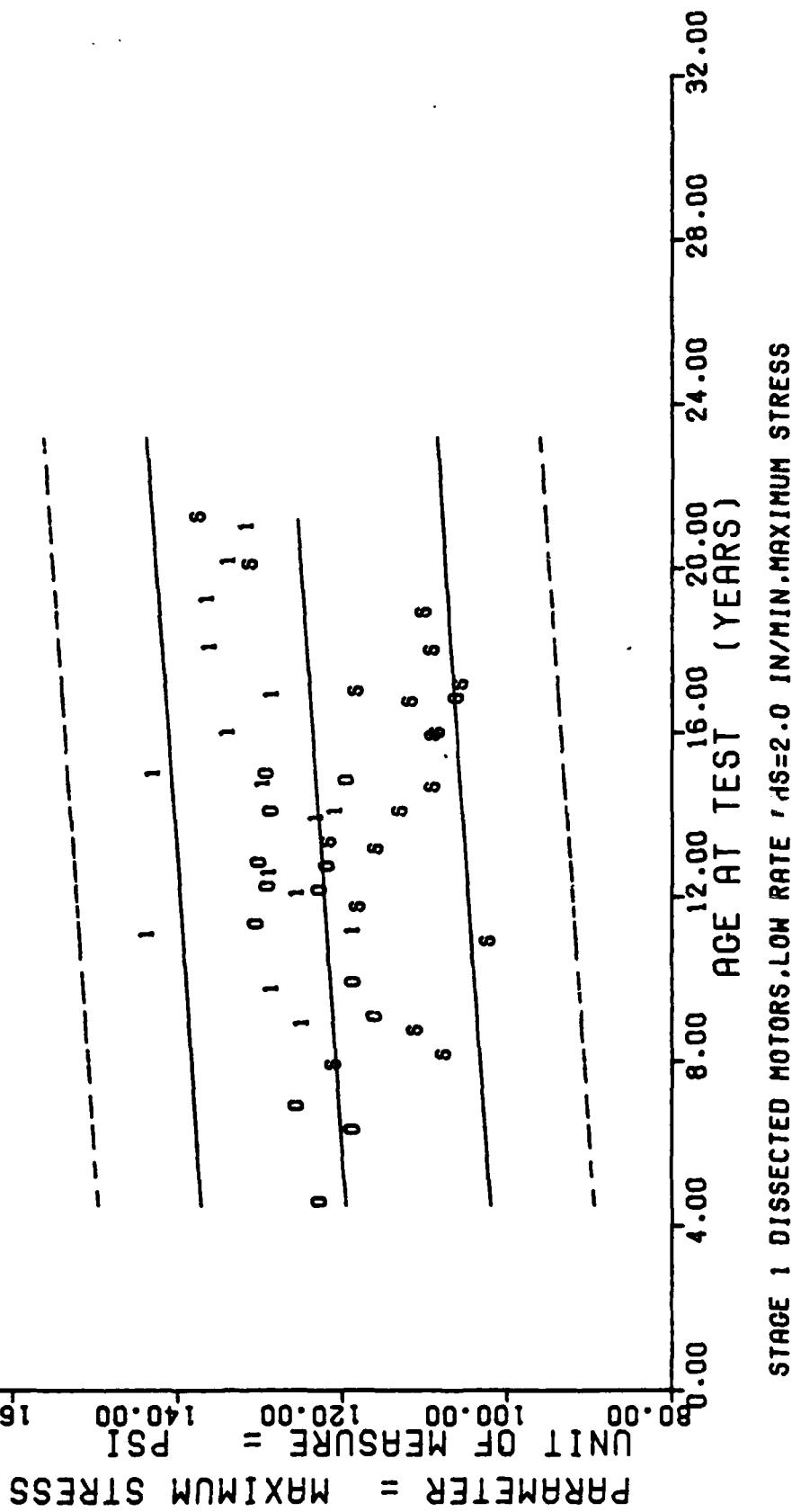


Figure 2A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	5	+1.2419999E+02	+4.7116375E+00	+1.2800000L+02	+1.1600000E+02	+1.2676202E+02
116.0	5	+1.2800000E+02	+2.8284271L+00	+1.3300000L+02	+1.2600000E+02	+1.2725791E+02
132.0	9	+1.4302323E+02	+1.5599791E+00	+1.4546999L+02	+1.4110998E+02	+1.2805137E+02
133.0	10	+1.1808496E+02	+1.2756730E+01	+1.346098E+02	+1.0400000E+02	+1.2810096E+02
144.0	5	+1.2485189E+02	+4.5344939E-01	+1.2520999E+02	+1.2412998E+02	+1.2864645E+02
150.0	8	+1.2635241E+02	+2.7744090E+00	+1.3153999E+02	+1.2439999E+02	+1.2894400E+02
166.0	5	+1.2251591E+02	+2.0232536E+00	+1.2544999E+02	+1.2055999E+02	+1.2973744E+02
168.0	3	+1.2019326E+02	+2.7322975E+00	+1.2327999E+02	+1.1809999E+02	+1.2983662E+02
176.0	5	+1.2901992E+02	+4.0229006E+00	+1.3303999E+02	+1.2500000E+02	+1.3023335E+02
179.0	5	+1.4228988E+02	+2.9554797E+00	+1.4488999E+02	+1.3736999E+02	+1.3038212E+02
191.0	8	+1.3332864E+02	+3.4865955E+00	+1.3782998E+02	+1.2877999E+02	+1.3097721E+02
202.0	3	+1.2796246E+02	+5.9602999E+00	+1.3619999E+02	+1.2009999E+02	+1.3152270E+02
216.0	8	+1.3545614E+02	+2.5353801E+00	+1.3852999E+02	+1.3007998E+02	+1.3221697E+02
239.0	8	+1.3582617E+02	+3.9676508L+00	+1.4368998L+02	+1.3298999E+02	+1.3291123E+02
241.0	8	+1.3314486E+02	+4.1273089E+00	+1.4010998E+02	+1.2988999E+02	+1.3345674E+02
251.0	10	+1.3098089E+02	+3.3284024E+00	+1.3636999E+02	+1.2644999E+02	+1.3395263E+02

STAGE 1. DISSECTED MOTOR=0012199, LOW RATE CHS=2.0 IN/MIN, MAXIMUM STRESS.

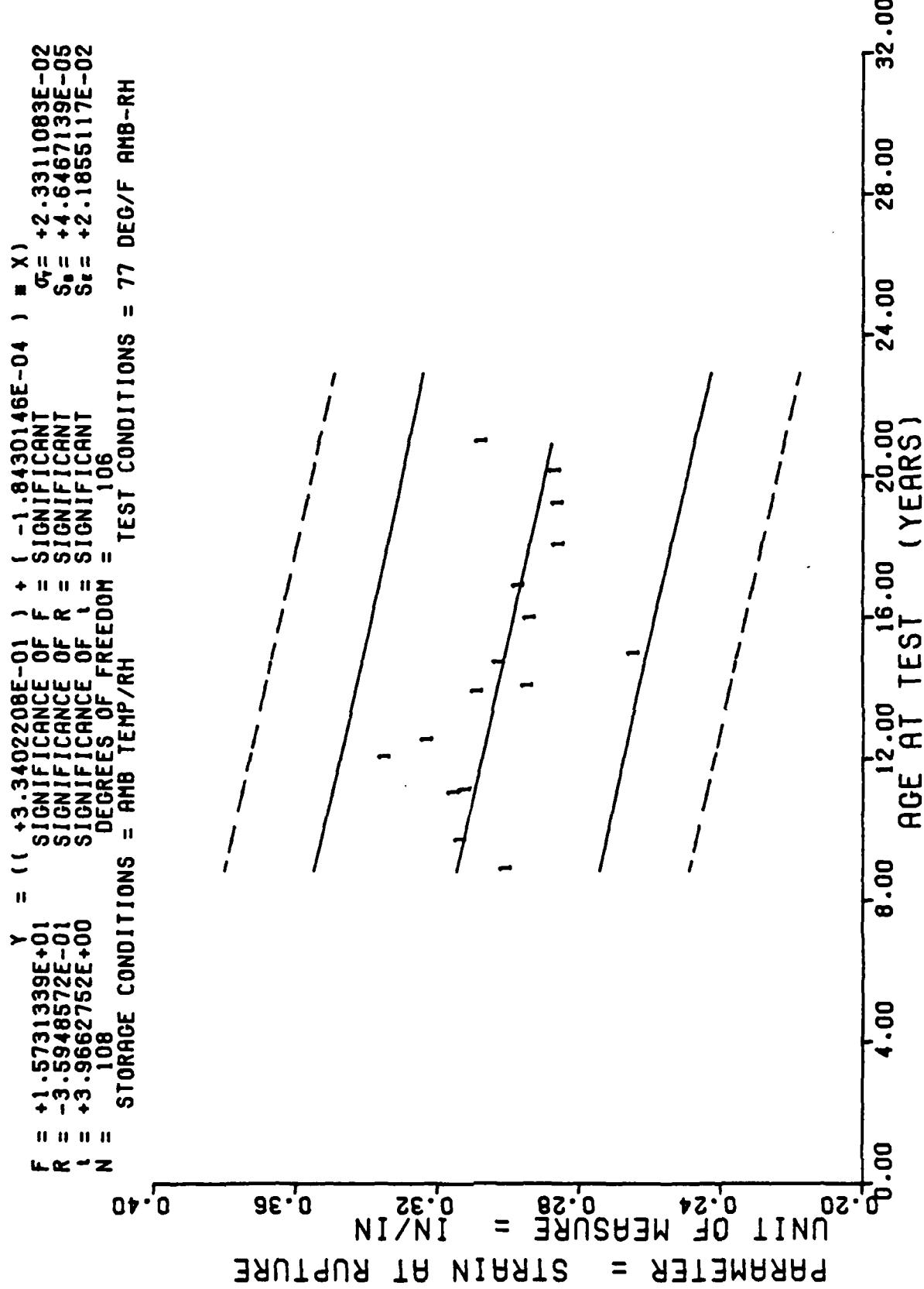
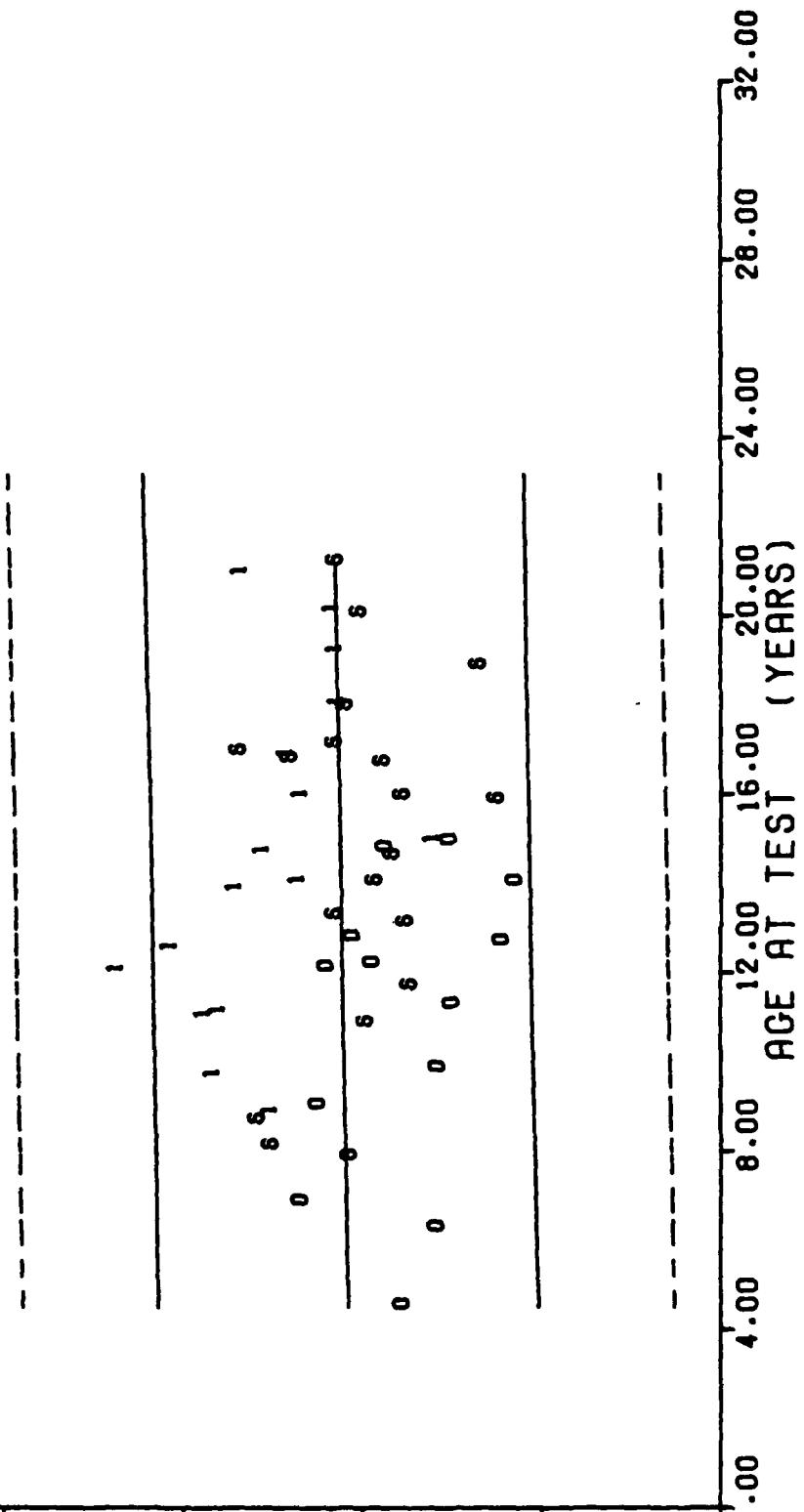


Figure 3

$\gamma = ((+2.8211867E-01) + (+1.5166345E-05) \times X)$
 $F = +3.5315632E-01$ SIGNIFICANCE OF F = NOT SIGNIFICANT
 $R = +3.4120016E-02$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $\epsilon = +5.9426957E-01$ SIGNIFICANCE OF ϵ = NOT SIGNIFICANT
 $N = 305$ DEGREES OF FREEDOM = 303
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG/F AMB-RH

PARAMETER = STRAIN AT RUPTURE
 UNIT OF MEASURE = IN/IN
 0.20 0.24 0.28 0.32 0.36 0.40



STAGE 1 DISSECTED MOTORS, LOW RATE CHS=2.0 IN/MIN, STRAIN AT RUPTURE

*** LINEAR INTERPOLATION ANALYSIS ***

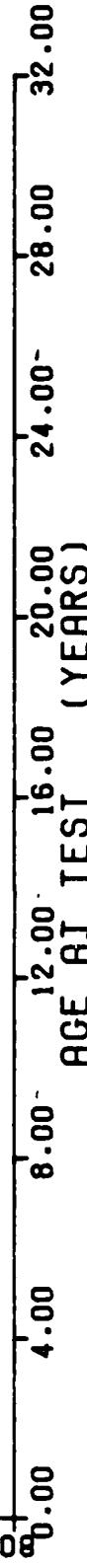
*** ANALYSIS OF TIME STEPS ***

ANALYSIS (ELEMNT.)	STRAIN (ELEMNT.)	STRAIN UP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
100.0	5	+2.9639991F-01	+2.5993757L-02	+3.4299999E-01	+2.7999999F-01	+3.144H603F-01	
110.0	5	+3.1219977L-01	+0.6069271L-03	+3.2199990L-01	+3.03999996F-01	+3.1264311L-01	
120.0	9	+3.1+1.8859L-01	+1.9246.009L-02	+3.4893997E-01	+2.9199999F-01	+3.0969424F-01	
130.0	10	+3.10379776F-01	+1.9150.704L-02	+3.2649996E-01	+2.7099996L-01	+3.0050993L-01	
140.0	5	+3.33099976F-01	+9.9597381L-03	+3.4749996L-01	+3.2119995E-01	+3.074H265L-01	
150.0	8	+3.2132466E-01	+9.57+1.201L-03	+3.3299994E-01	+3.07599926F-01	+3.0637681L-01	
160.0	5	+3.0745983L-01	+2.0130041L-02	+3.2719999L-01	+2.7859997F-01	+3.0342792E-01	
170.0	3	+2.9333529F-01	+3.3312.334E-02	+3.1599993E-01	+2.5499999L-01	+3.0305939L-01	
180.0	3	+3.0120661L-01	+9.7546.370L-03	+3.1009995E-01	+2.9079997F-01	+3.0158501E-01	
190.0	5	+2.6357981L-01	+1.9173457L-02	+2.3229.699E-01	+2.42599996L-01	+3.0103206L-01	
200.0	8	+2.0273712L-01	+1.1382005L-02	+3.1169998F-01	+2.7379995F-01	+2.9882049F-01	
210.0	-						
220.0	-						
230.0	8	+2.8494954L-01	+1.793503L-02	+3.0199993F-01	+2.4399995F-01	+2.916371L-01	
240.0	8	+2.3566205L-01	+2.8660470L-02	+3.0899995L-01	+2.3599994E-01	+2.8060537L-01	
250.0	10	+3.0617970L-01	+1.2067115E-02	+3.226999L-01	+2.7999997L-01	+2.8776240F-01	

TABLE I PLASTIC CYCLE RATE=0.012199, STRAIN RATE CHG=2.0 IN/MIN, STRAIN AT RUPTURE

$F = +2.1341157E+01$ $Y = ((+1.0694638E+02) + (+7.2630189E-02) \cdot X) \quad ;$
 $R = +4.0937808E-01$ $F = \text{SIGNIFICANT}$
 $N = +4.6196490E+00$ $R = \text{SIGNIFICANT}$
 $108 = \text{DEGREES-OF FREEDOM} \quad 106 = \text{SIGNIFICANT}$
 STORAGE CONDITIONS = AMB-TEMP/RH TEST CONDITIONS = AMB- TEMP/RH

PARAMETER = STRESS AT RUPTURE
 UNIT OF MEASURE = PSI



STAGE 1.DISSECTED MOTOR=0012199.LOW RATE CHS=2.0 IN/MIN.STRESS AT RUPTURE.

Figure 4

$F = +5.0969037E+00$ $\gamma = ((+1.0873378E+02) + (+2.4116727E-02) \cdot x) / (+1.0210514E+01)$
 $R = +1.2862030E-01$ $S_f = +1.0682309E-02$
 $t^2 = +2.2576323E+00$ $S_o = +1.0142400E+01$
 $N = 305$ DEGREES OF FREEDOM = 303
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = STRESS AT RUPTURE
 UNIT OF MEASURE = PSI
 50.00 60.00 70.00 80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00

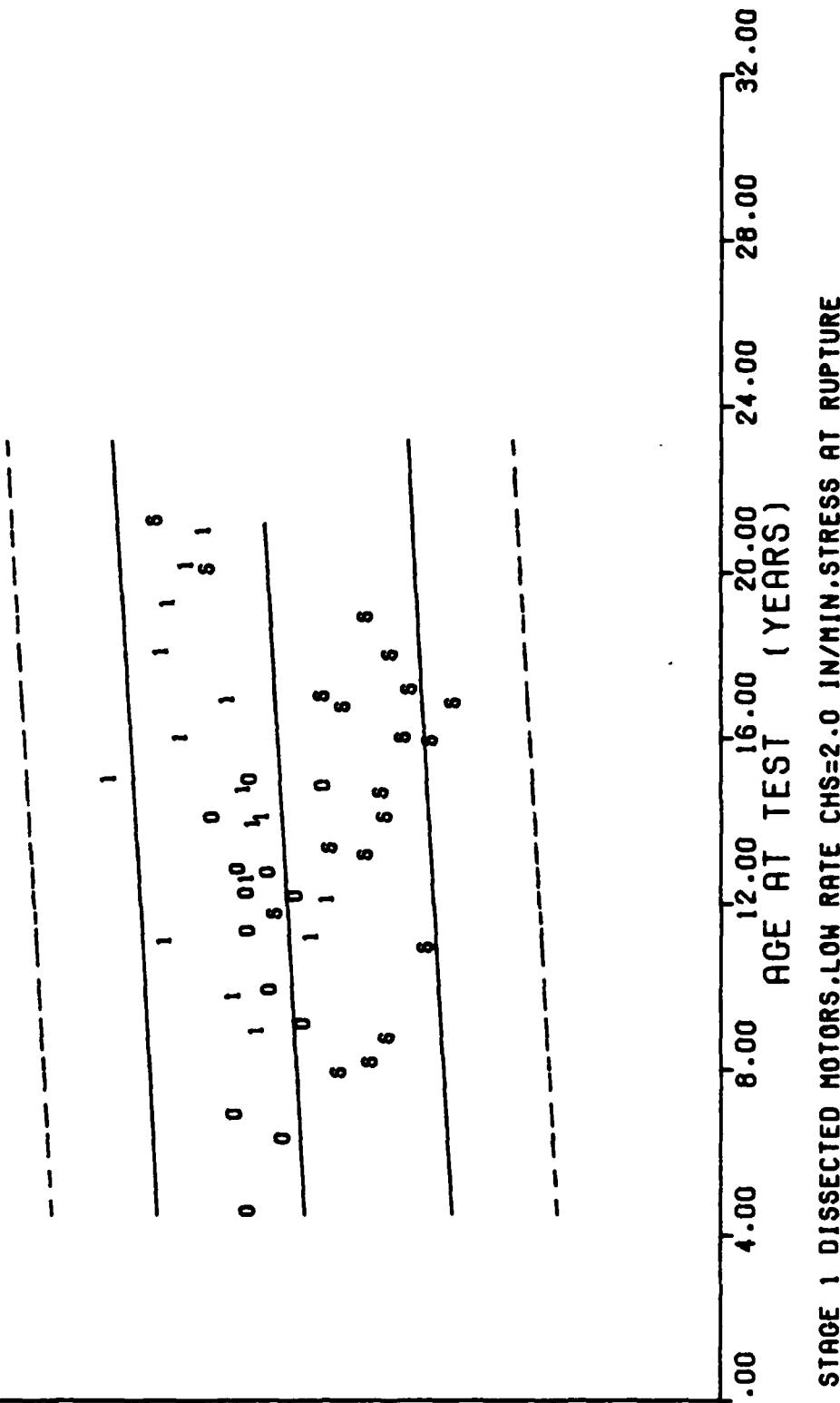


Figure 4A

**** LINEAR REGRESSION ANALYSIS ****
 *** ANALYSIS OF TIME STRENGTHS ***

AGE (MONTHS)	SPECIMENS PLR GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
100.0	5	+1.151999E+02	+7.0851958E+00	+1.2100000E+02	+1.0300000E+02	+1.1464517E+02
116.0	5	+1.1800000E+02	+1.8708286E+00	+1.2100000E+02	+1.1600000E+02	+1.1537147E+02
132.0	9	+1.2632099E+02	+3.5167607E+00	+1.3064999E+02	+1.2004998E+02	+1.1653356E+02
133.0	10	+1.0868698E+02	+7.6735505E+00	+1.1900000L+02	+1.0111999E+02	+1.1660618E+02
144.0	5	+1.0674594E+02	+3.3354907L+00	+1.1002999E+02	+1.0140998E+02	+1.1740512L+02
150.0	8	+1.1645367E+02	+3.9645105E+00	+1.2200000E+02	+1.0929998E+02	+1.1784091F+02
156.0	5	+1.1564393E+02	+3.7064829E+00	+1.2129998E+02	+1.1175000E+02	+1.1900299E+02
168.0	3	+1.1458657E+02	+4.7396500E+00	+1.2000000L+02	+1.1119999E+02	+1.1914825F+02
176.0	3	+1.1682991E+02	+3.8598576E+00	+1.201499E+02	+1.1259999E+02	+1.1972929F+02
179.0	5	+1.3299789E+02	+5.4633130E+00	+1.4128999E+02	+1.2678999E+02	+1.194718L+02
- 191.0	8	+1.2436114E+02	+4.3855068L+00	+1.2893998E+02	+1.1760998E+02	+1.2081874E+02
- 202.0	8	+1.1872488E+02	+6.0911562E+00	+1.2929998E+02	+1.0959999E+02	+1.2161767F+02
- 216.0	8	+1.2669744E+02	+3.2387581E+00	+1.3122999E+02	+1.2100000E+02	+1.2263450E+02
230.0	8	+1.2593490E+02	+4.3085561E+00	+1.3529998E+02	+1.2159999E+02	+1.2365132F+02
241.0	8	+1.2368615E+02	+6.2735394E+00	+1.3389999E+02	+1.1819999E+02	+1.2445025E+02
251.0	10	+1.2154089E+02	+3.0718152E+00	+1.2777999E+02	+1.1832998E+02	+1.251765bf+02

STAGE 1, DISSECTED MUTOR=0012199, LOW RATE CHS=2.0 IN/MIN. STRESS AT RUPTURE.

$\gamma = ((8.4823243E+02)^{-1} + (1.3122032E+00)^{-1}) \cdot X$
 $\sigma_f = +1.6780123E+02$
 $S_b = +3.6703489E-01$
 $S_t = +1.5845398E+02$
 $F = +1.2781666E+01$ SIGNIFICANT
 $R = +3.4278032E-01$ SIGNIFICANT
 $t = +3.5751457E+00$ SIGNIFICANT
 $N = 98$ DEGREES OF FREEDOM = 96
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$ TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = PSI
 $*10^3$
 PARAMETER = MODULUS
 0.00 4.00 8.00 12.00 16.00 20.00 24.00 28.00 32.00

STAGE 1 DISSECTED MOTOR=0012199.LOW RATE CHS=2.0 IN/MIN. MODULUS.

Figure 5

$F = +2 \cdot 1843689E-01$ $Y = ((+1 \cdot 1763037E+03) + (+1 \cdot 0093406E-01) \cdot X)$
 $R = +2 \cdot 79699C2E-02$ SIGNIFICANCE OF F = NOT SIGNIFICANT $\sigma_f = +1 \cdot 9938807E+02$
 $t = +4 \cdot 6737232E-01$ SIGNIFICANCE OF R = NOT SIGNIFICANT $S_b = +2 \cdot 1596072E-01$
 $N = 281$ SIGNIFICANCE OF t = NOT SIGNIFICANT $S_r = +1 \cdot 9966693E+02$
DEGREES OF FREEDOM = 279 STORAGE CONDITIONS = AHB TEMP/RH TEST CONDITIONS = AHB TEMP/RH

UNIT OF MEASURE = PSI $*10^3$
PARAMETER = MODULUS

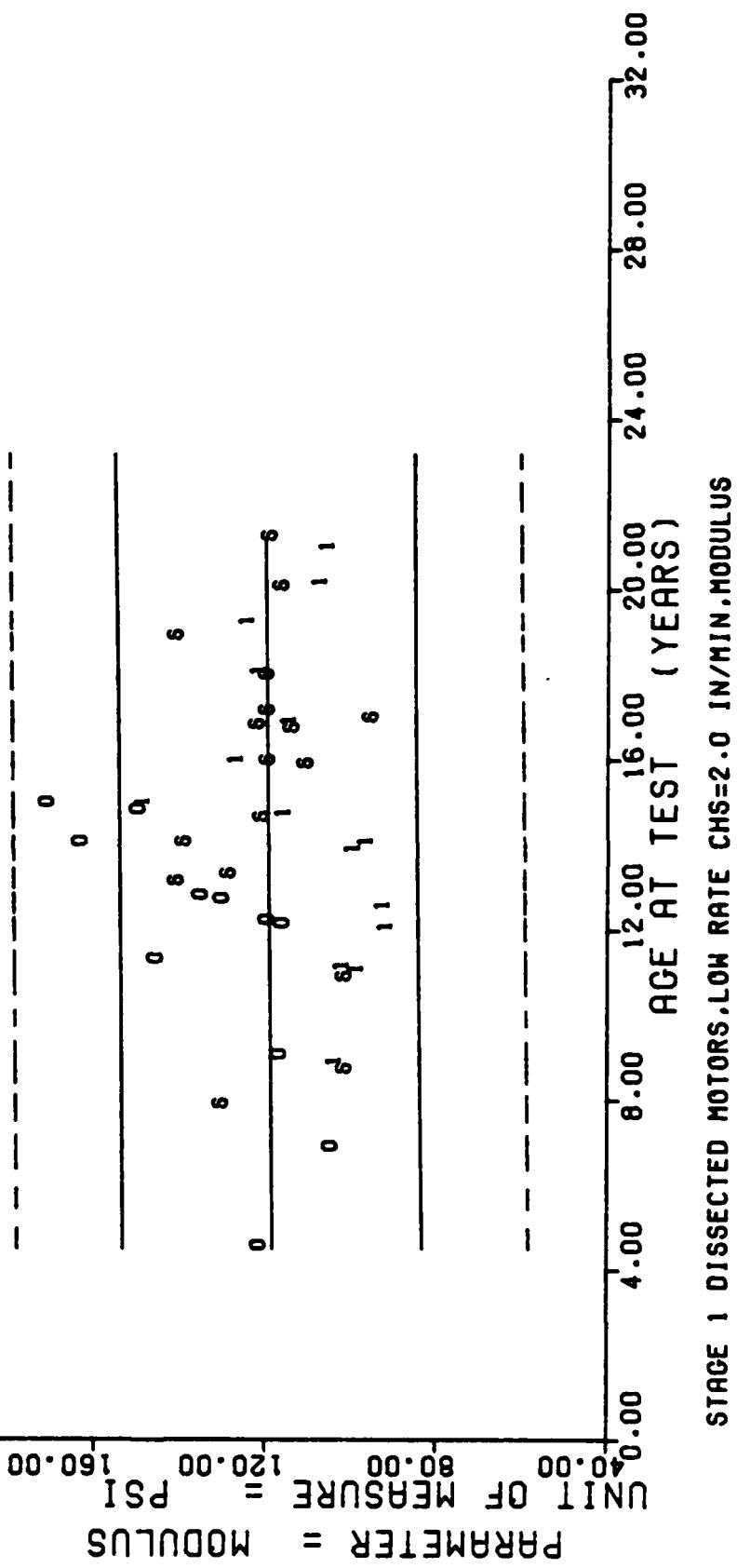


Figure 5A

***+4 L100 M8 C1000000000000000 ANALYSIS ***

***+4 ANALYSIS OF TIME SERIES ***

SPC DATA 4.5

COORDINATE	TIME GROUP	MEAN Y	STANDARD DEVIATION Y	MAXIMUM Y	MINIMUM Y	PREDICTION Y
1.35+0	5	+1.0260000E+03	+1.0350571E+02	+1.1200000E+03	+0.5000000E+02	+9.8732592E+02
1.25+0	6	+9.7577759E+02	+1.234E+02	+1.1430000E+03	+8.0800000E+02	+1.0214431E+03
1.15+0	6	+1.0085993E+03	+1.104E+02	+1.1550000E+03	+9.7000000E+02	+1.0227553E+03
1.04+0	5	+9.006599d5L+02	+5.194E+01	+9.0400000L+02	+8.5400000F+02	+1.0371896E+03
1.04+0	6	+9.1337500d5E+02	+7.753E+01	+1.0000000E+03	+8.5000000E+02	+1.0450627E+03
1.04+0	5	+9.3555935E+02	+4.467E+01	+1.0620000E+03	+9.4700000E+02	+1.0660561E+03
1.05+0	5	+9.5433325L+02	+1.700E+01	+9.710E+00	+9.3700000E+02	+1.0686824E+03
1.05+0	3	+1.1470000E+03	+1.313E+02	+1.3070000E+03	+1.0390000E+03	+1.0791601E+03
1.05+0	3	+1.4771999E+03	+4.34E+02	+1.499E+03	+1.430000E+02	+1.0831160E+03
1.04+0	6	+1.2577500E+03	+3.750E+02	+1.2950000E+03	+1.2030000E+03	+1.0088030E+03
1.04+0	3	+1.1345000E+03	+1.600E+02	+1.3590000E+03	+9.3800000E+02	+1.1132973E+03
1.04+0	3	+1.2055000E+03	+5.217E+02	+1.26E+03	+1.1240000E+03	+1.1316682E+03
1.05+0	6	+1.2323750E+03	+6.013E+02	+1.3110000E+03	+1.1030000E+03	+1.1500490E+03
1.04+0	3	+1.0627500E+03	+1.371E+02	+1.3060000E+03	+9.5500000E+02	+1.1644733E+03
1.04+0	10	+1.0461999E+03	+7.42E+02	+1.1970000E+03	+9.4700000E+02	+1.1775652E+03

DATA 1. DISCUSSION MUL=0.012199, LOG RATE C16=2.0 IN/MIN, MODULUS.

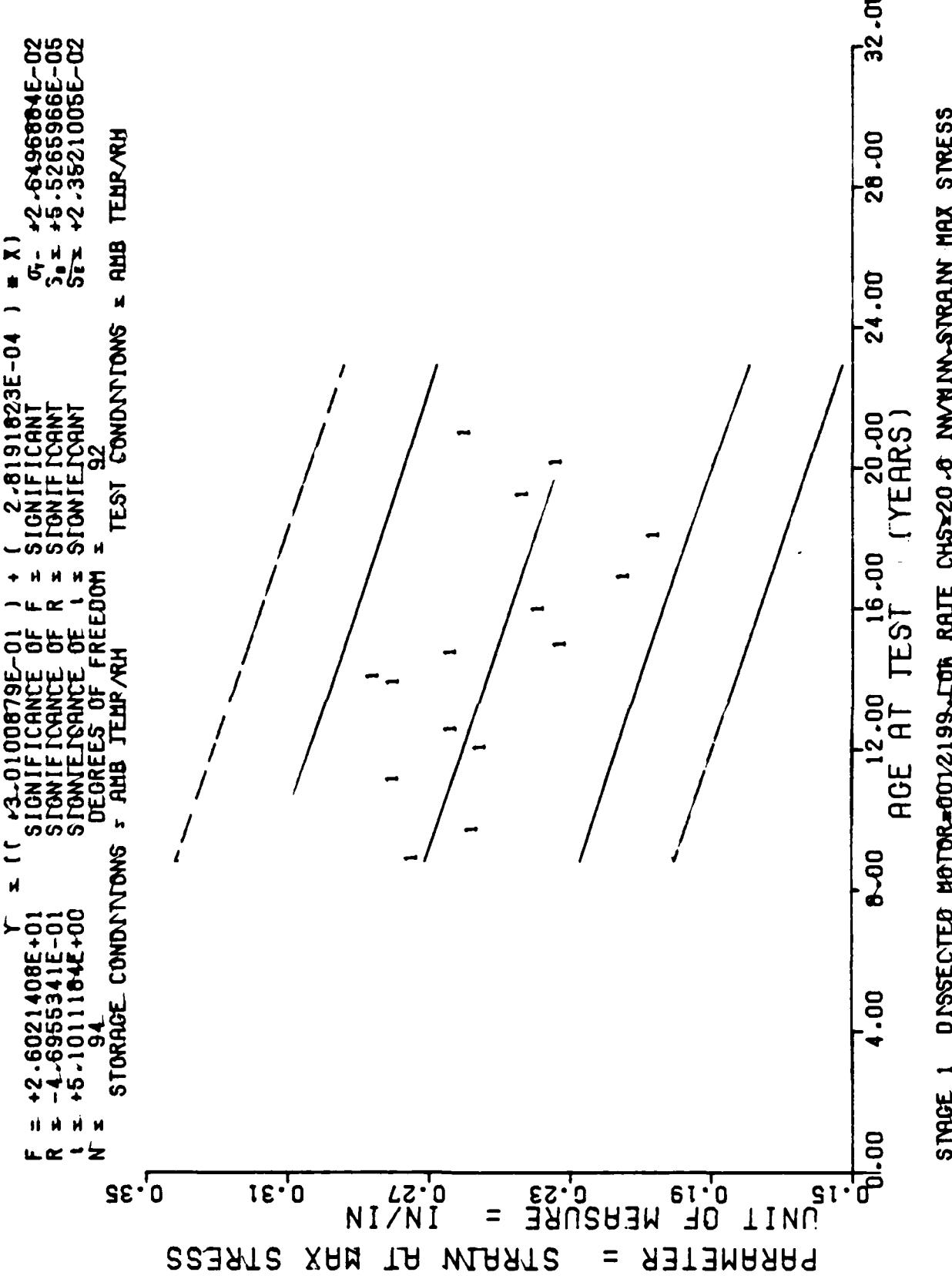


Figure 6

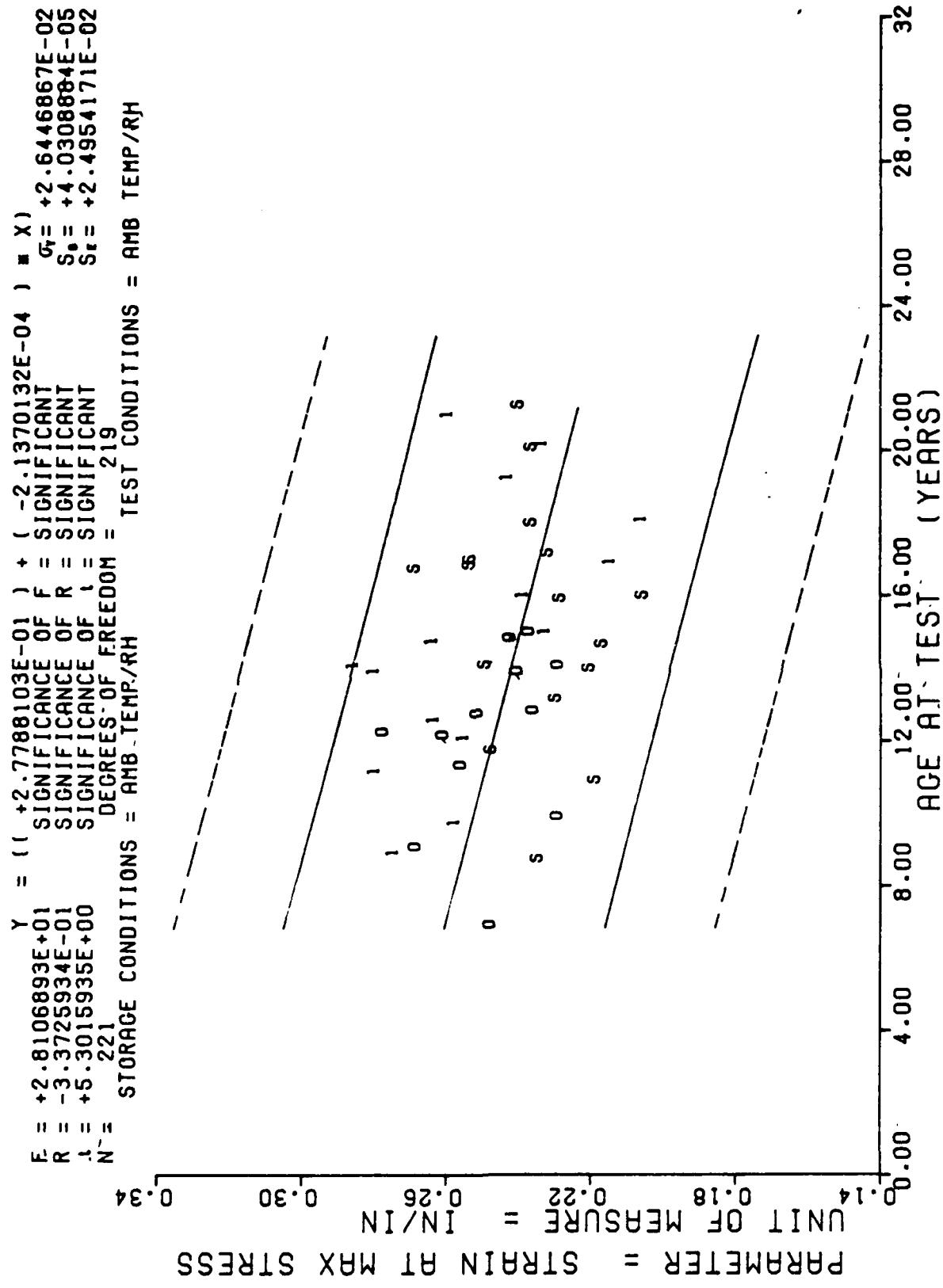


Figure 6A

**** LINEAR REGRESSION ANALYSIS ****
 *** ANALYSIS OF TIME SERIES ***

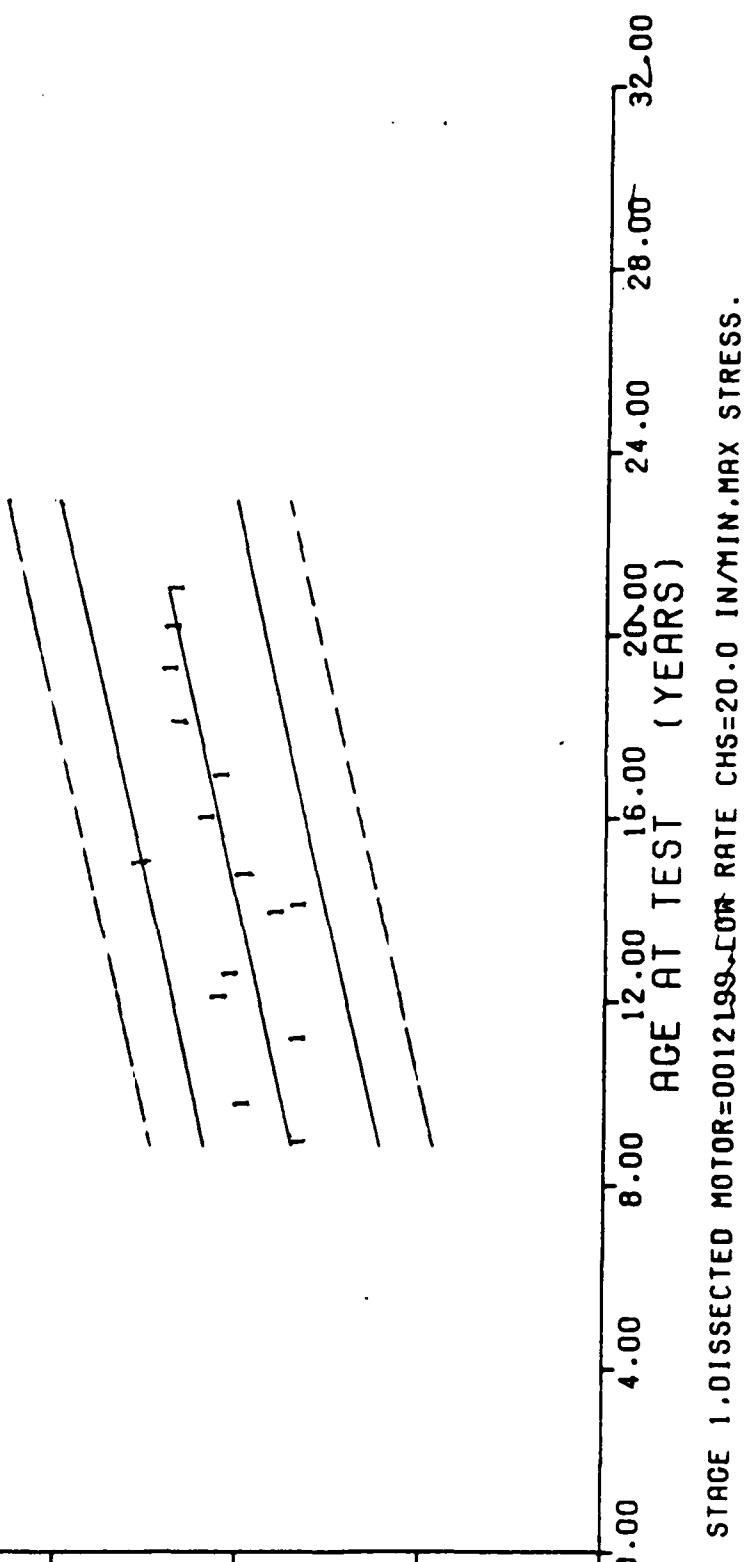
AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
100.0	5	+2.7359980E-01	+1.0445070E-02	+2.4399997E-01	+2.5999999E-01	+2.7112543E-01
110.0	5	+2.5659978E-01	+1.3431138E-02	+2.7999997E-01	+2.4899995E-01	+2.6830625E-01
133.0	4	+2.7891081E-01	+9.9499704E-03	+2.9299998E-01	+2.6429998E-01	+2.6351362E-01
144.0	4	+2.5424981E-01	+2.3436458E-02	+2.3099995E-01	+2.3199999E-01	+2.6041251E-01
150.0	9	+2.6248342E-01	+1.2791937E-02	+2.7699995E-01	+2.3709994E-01	+2.5872105E-01
166.0	5	+2.7695981E-01	+4.8522512E-03	+2.8429996E-01	+2.7229994E-01	+2.5421035E-01
169.0	3	+2.8466659E-01	+1.5947957E-02	+3.0299997L-01	+2.7399998E-01	+2.5364649E-01
176.0	3	+2.6269996E-01	+8.006440E-03	+2.7239996E-01	+2.5599998E-01	+2.5139117E-01
179.0	3	+2.3163986E-01	+3.2674051E-03	+2.3469996E-01	+2.2699999E-01	+2.5054538E-01
191.0	3	+2.3784983E-01	+1.6565079E-02	+2.5329995E-01	+2.0669996E-01	+2.4716240E-01
202.0	6	+2.1374973E-01	+2.1607133E-02	+2.4399995E-01	+1.9299995E-01	+2.4406120E-01
- 216.0	3	+2.0511221E-01	+1.0079520E-02	+2.2129994E-01	+1.9449996E-01	+2.4011445E-01
- 230.0	9	+2.4225527E-01	+1.2546044E-02	+2.7299994E-01	+2.3229998E-01	+2.3616755E-01
- 241.0	3	+2.3269993E-01	+4.5106245E-03	+2.3789995E-01	+2.2979998E-01	+2.3306643E-01
- 251.0	10	+2.5878971E-01	+9.5627912E-03	+2.7209997L-01	+2.4009996E-01	+2.3024725E-01

STAGE 1 DISSOLVED MOTOR=0012199,LOW RATE CHS=20.0 IN/MIN, STRAIN MAX STRESS

$F = +6.0610720E+01$
 $R = +6.3023058E-01$
 $t = +7.7858024E+00$
 $N = 94$
 STORAGE CONDITIONS = AMB TEMP/RH
 DEGREES OF FREEDOM = 92
 TEST CONDITIONS = AMB TEMP/RH

$\gamma = N + 1.2839603E+02$
 $F = SIGNIFICANCE OF F = 1.8821921E-01$
 $R = SIGNIFICANCE OF R = 31.80173E+01$
 $t = SIGNIFICANCE OF t = 2.4174670E-02$
 $S_r = +1.0288656E+01$

UNIT OF MEASURE = PSI
 PARAMETER = MAXIMUM STRESS
 80.00 120.00 160.00 200.00 240.00 280.00



STAGE 1 DISSECTED MOTOR=0012199-L001 RATE CHS=20.0 IN/MIN. MAX STRESS.

Figure 7

$\gamma = ((+1.3550250E+02) + (+9.2227093E-02)) \times X$
 $F = +1.3757039E+01$
 $R = +2.4311462E-01$
 $S = +3.7090482E+00$
 $L = 221$
 $N = 219$
 $F = +1.3550250E+02$
 $R = +2.4311462E-01$
 $S = +3.7090482E+00$
 $L = 221$
 $DEGREES OF FREEDOM = 219$
 $STORAGE CONDITIONS = AMB TEMP/RH$
 $TEST CONDITIONS = AMB. TEMP/RH$

UNIT OF MEASURE = PSI
 PARAMETER = MAXIMUM STRESS

STAGE 1 DISSECTED-MOTORS,LOW RATE CHS=20.0 IN/MIN.MAXIMUM STRESS

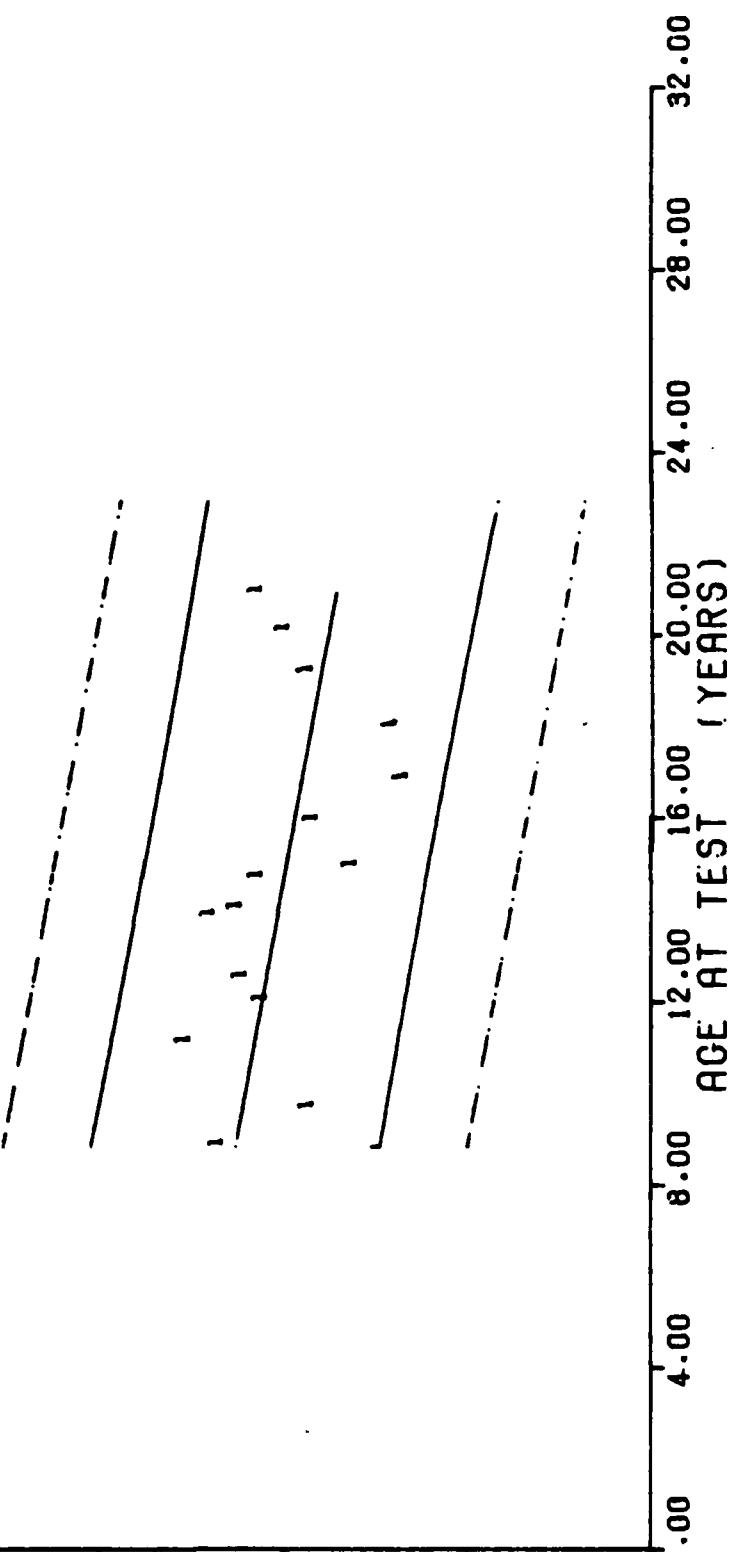
**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PLR GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
1.06..0	5	+1.4539999E+02	+1.1401754E+00	+1.4700000E+02	+1.4400000E+02	+1.4834725E+02
1.16..0	5	+1.5779998E+02	+5.8906705E+00	+1.6300000E+02	+1.5000000E+02	+1.5022946E+02
1.33..0	9	+1.4562550E+02	+1.8129338E+01	+1.6710998E+02	+1.2800000E+02	+1.5342918E+02
1.44..0	4	+1.6316491E+02	+9.004990E+00	+1.7140598E+02	+1.5039999E+02	+1.5549958E+02
1.50..0	9	+1.6055654E+02	+5.7467006E+00	+1.0950000E+02	+1.5562998E+02	+1.5662890E+02
1.66..0	5	+1.5049194E+02	+2.7810708E+00	+1.5372999E+02	+1.4684999E+02	+1.5964041E+02
1.68..0	3	+1.4558992E+02	+1.5274839E+00	+1.4714999E+02	+1.4411999E+02	+1.6001686E+02
1.76..0	3	+1.5740322E+02	+2.7589509E+00	+1.6057998E+02	+1.5564999E+02	+1.6152261E+02
1.79..0	5	+1.8026391E+02	+2.9412120E+00	+1.8273999E+02	+1.7536999E+02	+1.6208726E+02
1.91..0	3	+1.6575241E+02	+7.5057718E+00	+1.7664999E+02	+1.5643998E+02	+1.6434590F+02
2.02..0	8	+1.6239987E+02	+1.1881877E+01	+1.7589999E+02	+1.4789999F+02	+1.6641630E+02
- 216..0	8	+1.7199243E+02	+4.6476210E+00	+1.7795999E+02	+1.6335998E+02	+1.6905137E+02
33 230..0	9	+1.7388323E+02	+5.1922320E+00	+1.8154998E+02	+1.6819999F+02	+1.7168644E+02
- 241..0	3	+1.7332656E+02	+5.9083106E+00	+1.7707598E+02	+1.6651998E+02	+1.7375685E+02
251..0	10	+1.7268588E+02	+4.8429620E+00	+1.7704998E+02	+1.6259999E+02	+1.7563905E+02

$y = 11 + 3.7284602E-01 x + (-3.0210463E-04) x^2$
 $F = +1.4601980E+01$ SIGNIFICANCE OF F = $\sigma_f = +3.6023903E-02$
 $R = -3.7010355E-01$ SIGNIFICANCE OF R = $S_r = +7.9059032E-05$
 $t = +3.8212638E+00$ SIGNIFICANCE OF t = $S_t = +3.3647262E-02$
 $N = 94$ DEGREES OF FREEDOM = 92
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = STRAIN AT RUPTURE
 UNIT OF MEASURE = IN/IN
 0.00 0.16 0.24 0.32 0.40 0.48 0.56



STAGE 1 DISSECTED MOTOR=0012199,LOW RATE CHS=20.0 IN/MIN,STRAIN AT RUPTURE

Figure 8

$\gamma = ((+3.3770904E-01) + (-1.5086944E-04) \cdot X)$
 F = SIGNIFICANT OF F = SIGNIFICANT
 R = SIGNIFICANT OF R = SIGNIFICANT
 L = SIGNIFICANT OF L = SIGNIFICANT
 N = 221 DEGREES OF FREEDOM = 219
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

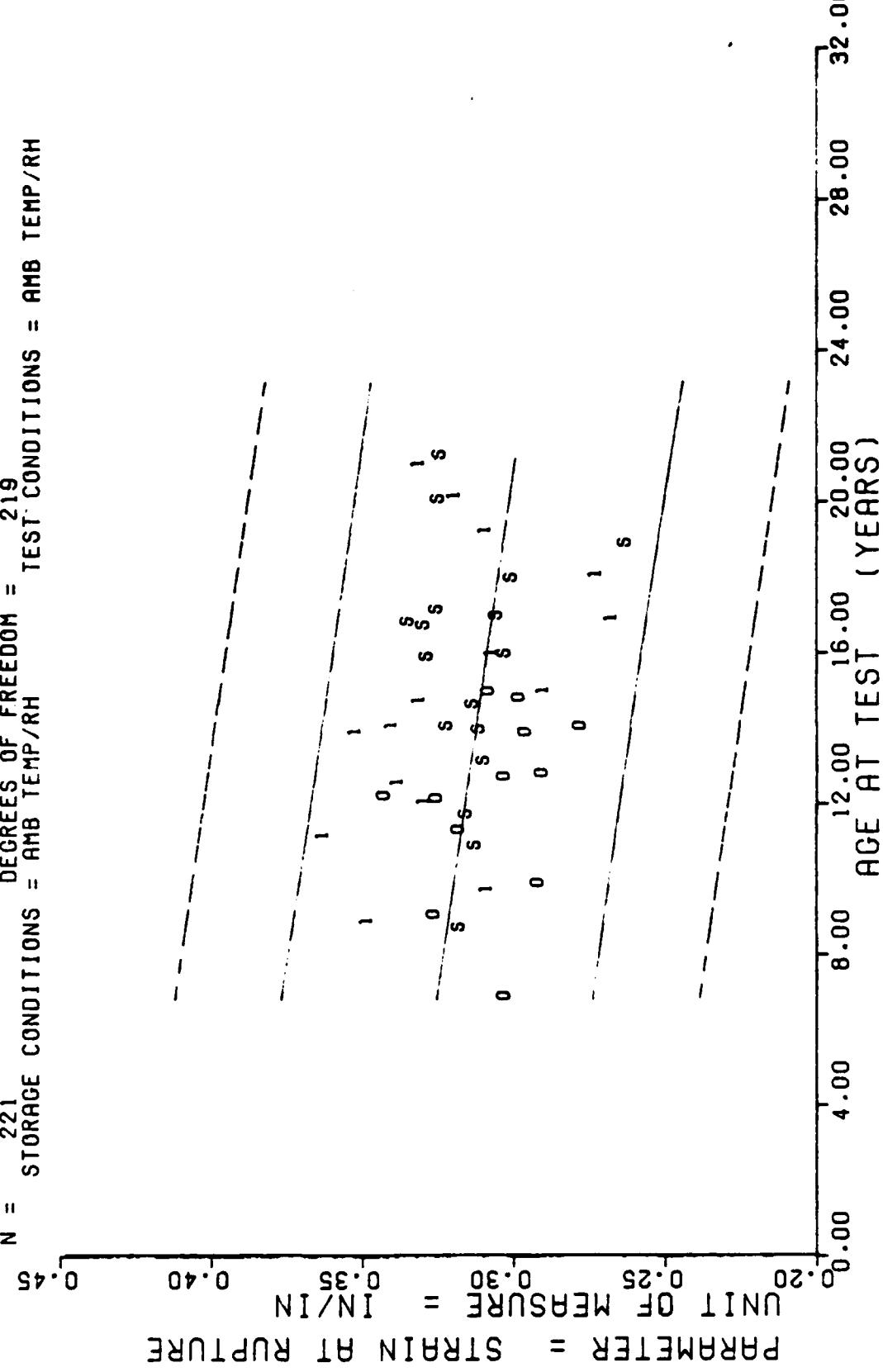


Figure 8A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD		MINIMUM Y	REGRESSION Y
			DEVIATION	MAXIMUM Y		
100.0	5	+3.4719961E-01	+2.0235265E-02	+3.679997E-01	+3.1599998E-01	+3.4082287E-01
116.0	5	+3.0759978E-01	+1.7688302E-02	+3.3299994E-01	+2.8299999E-01	+3.3780187E-01
133.0	9	+3.6161059E-01	+1.6592326E-02	+3.9699995E-01	+3.4099996E-01	+3.3266609E-01
144.0	4	+3.2827472E-01	+3.4613049E-02	+3.7199997E-01	+2.9869997E-01	+3.2934290E-01
150.0	9	+3.3699965E-01	+1.9222032E-02	+3.6099994E-01	+2.9899996E-01	+3.2753032E-01
166.0	5	+3.5083961E-01	+3.6953573E-03	+3.5659998E-01	+3.4729999E-01	+3.2269662E-01
168.0	3	+3.3899974E-01	+1.7326479E-02	+3.5899996E-01	+3.2899999E-01	+3.2209241E-01
176.0	3	+3.2986658E-01	+4.3023919E-03	+3.3239996E-01	+3.2489997E-01	+3.1967556E-01
179.0	5	+2.8893983E-01	+9.4803047E-03	+2.9809999E-01	+2.7589994E-01	+3.1876927E-01
191.0	6	+3.0583715E-01	+4.041991E-02	+3.4329998E-01	+2.1779996E-01	+3.1514400E-01
202.0	6	+2.6649975E-01	+2.8762047E-02	+3.0299997E-01	+2.2799998E-01	+3.1182086E-01
216.0	8	+2.7162480E-01	+1.1146937E-02	+2.8999996E-01	+2.5399994E-01	+3.0759137E-01
230.0	9	+3.0813300E-01	+3.2158108E-02	+3.5099995E-01	+2.5019997E-01	+3.0336195E-01
241.0	3	+3.1833326E-01	+1.3501815E-02	+3.3599996E-01	+3.0699998E-01	+3.0003875E-01
251.0	10	+3.3018970E-01	+1.5808676E-02	+3.4629994L-01	+2.9139995E-01	+2.9701775E-01

STAGE 1 DISSECTED MOTOR=0012199,LOW RATE CHS=20.0 IN/MIN,STRAIN AT RUPTURE

$F = +2.1360523E+01$ $Y = ((+1.3201605E+02) + (+1.1101782E-01) * X)$
 $R = +4.3408524E-01$ SIGNIFICANCE OF F = SIGNIFICANT
 $I = +4.6217446E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $N = 94$ SIGNIFICANCE OF I = SIGNIFICANT
DEGREES OF FREEDOM = 92 TEST CONDITIONS = AMB TEMP/RH
STORAGE CONDITIONS = AMB TEMP/RH

PARAMETER = STRESS AT RUPTURE

UNIT OF MEASURE = PSI

0.00 4.00 8.00 12.00 16.00 20.00 24.00 28.00 32.00

STAGE 1.DISSECTED MOTOR=0012199.LOW RATE CHS=20.0 IN/MIN.STRESS AT RUPTURE.

Figure 9

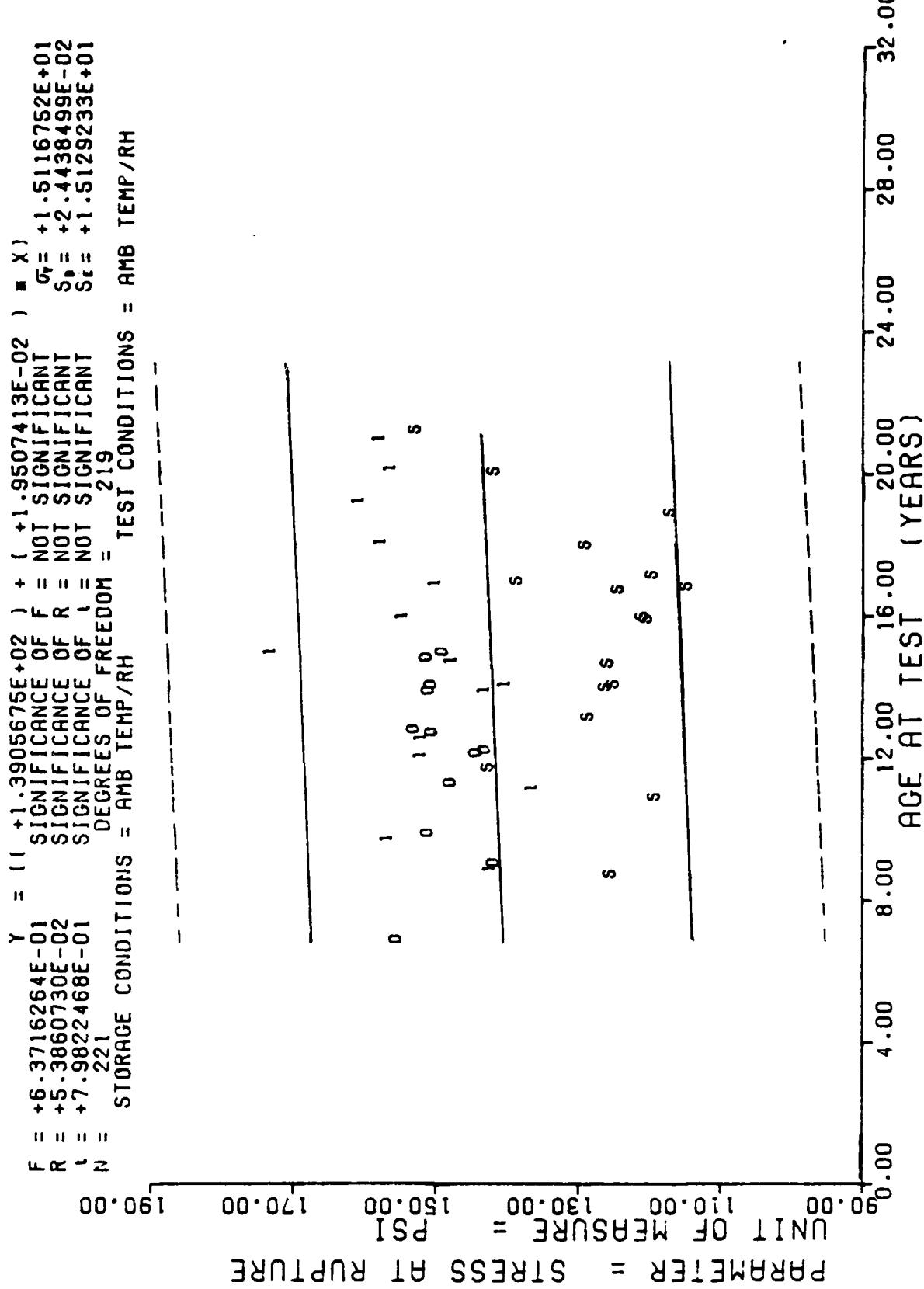


Figure 9A

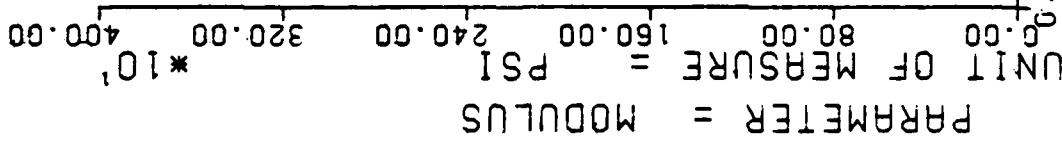
**** LINEAR REGRESSION ANALYSIS ****

**** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	5	+1.4200000E+02	+7.0710678E-01	+1.4300000E+02	+1.4100000E+02	+1.4378393E+02
116.0	5	+1.5639999E+02	+6.5421708E+00	+1.6100000E+02	+1.4700000E+02	+1.4489411E+02
133.0	9	+1.3611994E+02	+1.2542600E+01	+1.5085998E+02	+1.2100000E+02	+1.4678141E+02
144.0	4	+1.5178485E+02	+9.7755807E+00	+1.6177999E+02	+1.4029998E+02	+1.4800260E+02
150.0	9	+1.5171101E+02	+5.4151206E+00	+1.6000000E+02	+1.4564999E+02	+1.4866871E+02
166.0	5	+1.4296391E+02	+3.9280589E+00	+1.4617999E+02	+1.3654998E+02	+1.5044500E+02
168.0	3	+1.4005989E+02	+1.6887985E+00	+1.4123999E+02	+1.3813999E+02	+1.5066703E+02
176.0	3	+1.4750325E+02	+3.4042401E+00	+1.5141999E+02	+1.4531999E+02	+1.5155517E+02
179.0	5	+1.7289788E+02	+3.9573571E+00	+1.7591999E+02	+1.6612998E+02	+1.5188822E+02
191.0	8	+1.5439489E+02	+9.3510893E+00	+1.6657998E+02	+1.4237998E+02	+1.5322044E+02
202.0	8	+1.4976239E+02	+1.1379018E+01	+1.6369999E+02	+1.3329998E+02	+1.5444165E+02
216.0	8	+1.5747738E+02	+5.3541638E+00	+1.6284999E+02	+1.4659999E+02	+1.5599589E+02
230.0	9	+1.6055543E+02	+7.2916759E+00	+1.7279998E+02	+1.4919999E+02	+1.5755014E+02
241.0	3	+1.5614656E+02	+6.8852199E+00	+1.6013999E+02	+1.4819999E+02	+1.5877134E+02
251.0	10	+1.5769886E+02	+4.7399551E+00	+1.6689999E+02	+1.5116999E+02	+1.5988151E+02

STAGE 1. DISSECTED MOTOR=0012199. LOW RATE CHS=20.0 IN/MIN. STRESS AT RUPTURE.

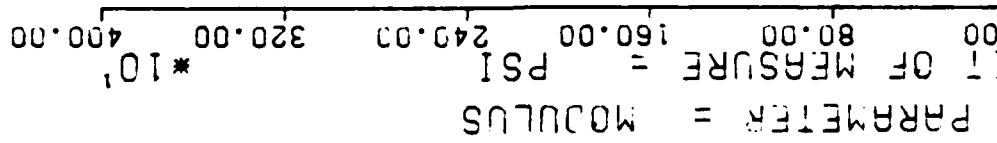
$F = +4.8456380E+00$ $Y = ((+1.2409489E+03) + (+3.2518538E+00) * X_1)$
 $R = +2.4331994E-01$ $F = \text{SIGNIFICANT}$ $\sigma_r = +4.9159871E+02$
 $t = +2.2012810E+00$ $S_r = +1.4772552E+00$
 $N = 79$ $S_b = +4.7991052E+02$
 $Degrees of Freedom = 77$ $S_t = +4.7991052E+02$
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



STAGE-1 DISSECTED MOTOR=0012199,LOW RATE,CHS=20.0 IN/MIN,MODULUS.

Figure 10

$Y = ((+1.5307935E+03) + 1 * 2.0152095E+00) * X$
 F = +3.5235781E+00 SIGNIFICANCE OF F = NOT SIGNIFICANT
 R = +1.3707681E-01 SIGNIFICANCE OF R = NOT SIGNIFICANT
 L = +1.8771196E+00 SIGNIFICANCE OF L = NOT SIGNIFICANT
 N = 186 DEGREES OF FREEDOM = 184
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



PARAMETER = MODULUS

STAGE 1 DISSECTED MOTORS, LOW RATE CHS=20.0 IN./MIN. MODULUS

Figure 10A

44381 LINEAR INTERPOLATION AT ANY LS ***

*** AT ANY LS OR WHICH EVER IS ***

LINE NUMBER	DATA GROUP	DATA Y	STANDARD EQUATION	MAXIMUM Y	MINIMUM Y	PREGRESSION Y
1.000	4	*1.3007500F+9.3	*1.5479314F+02	*1.6320000F+03	*1.2900000F+03	*1.6734453E+03
1.000	4	*1.3797500F+03	*5.763039L+01	*1.6420000F+03	*1.4300000F+03	*1.7092158E+03
1.000	0	+1.4915554E+03	+1.9134331F+02	+1.7620000F+03	+1.0530000F+03	+1.7287270E+03
1.000	6	+1.7643995F+03	+5.7112170F+01	+1.6230000F+03	+1.6820000F+03	+1.7807565L+03
1.000	3	+1.5330000F+03	+4.1302905F+02	+1.9650000F+03	+1.1420000F+03	+1.7872602E+03
1.000	3	+1.3110000F+03	+1.9974384F+01	+1.5230000F+03	+1.2890000F+03	+1.3132751E+03
1.000	5	+1.3092999L+02	+1.9e320001L+02	+2.23709000L+03	+1.7270000E+03	+1.8230307E+03
1.000	9	+2.0193750F+03	+4.1416302F+02	+2.5480000F+03	+1.4550000F+03	+1.8620520I+03
1.000	3	+2.7761250I+03	+5.1336266I+02	+3.1950000F+03	+2.0400000F+03	+1.8973232F+03
1.000	6	+2.2832750I+03	+4.4223107I+02	+2.7500000F+03	+1.2810000F+03	+1.9433493I+03
1.000	9	+1.9705554I+03	+1.4557002I+02	+2.1386000F+03	+1.7050000E+03	+1.9886752I+03
1.000	3	+1.5260000F+03	+1.4432710I+02	+1.6720000L+03	+1.4210000F+03	+2.0246457I+03
1.000	10	+1.0190000I+03	+2.2307404I+02	+2.1000000F+03	+1.3010000E+03	+2.0571640F+03

ANALYSIS OF THE DATA AT 0.12179, 1.0M GAUSSIAN, $\sigma_{\text{LS}}=20 \pm 0$ IN/MIN. MODULUS.

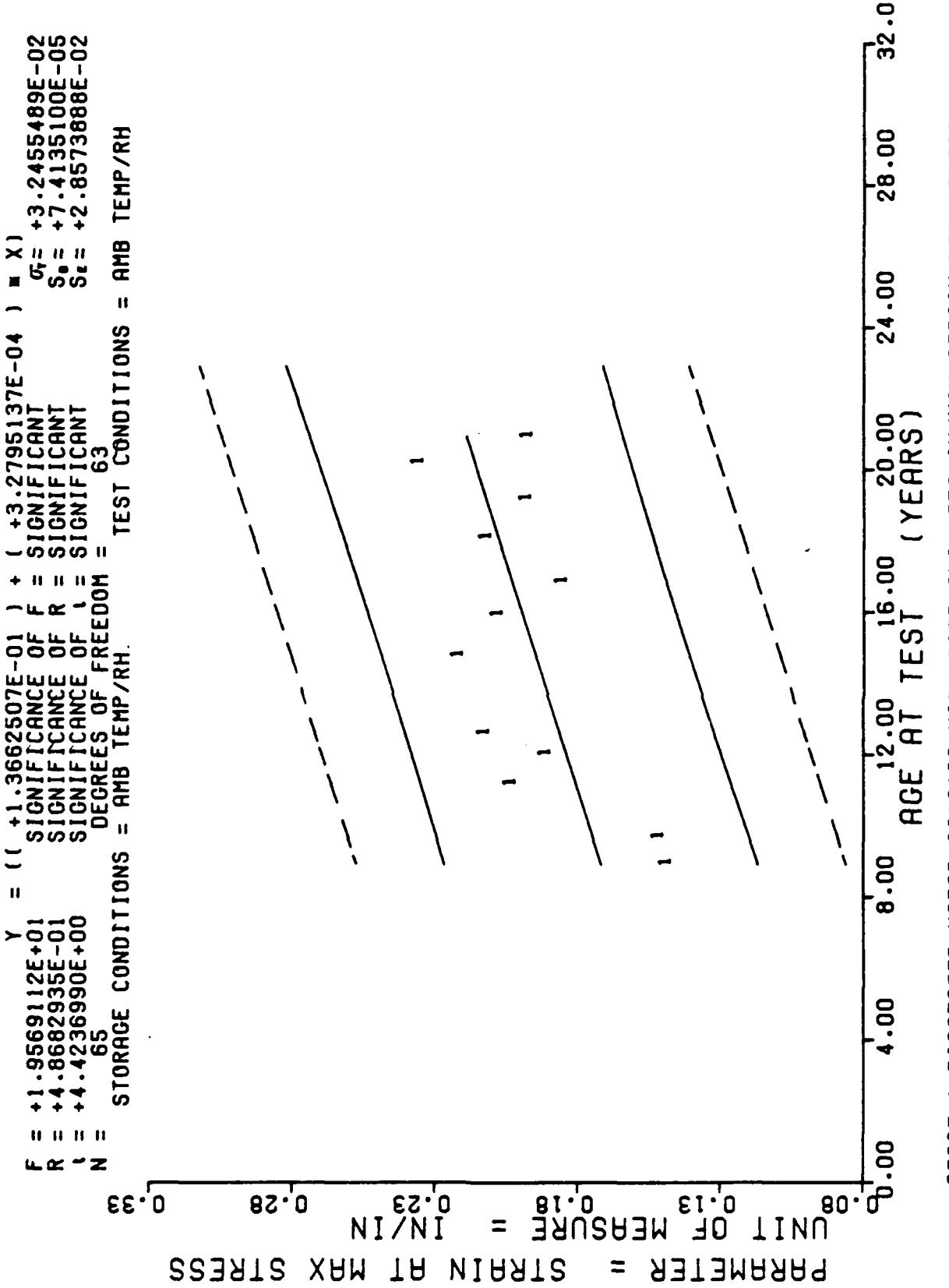
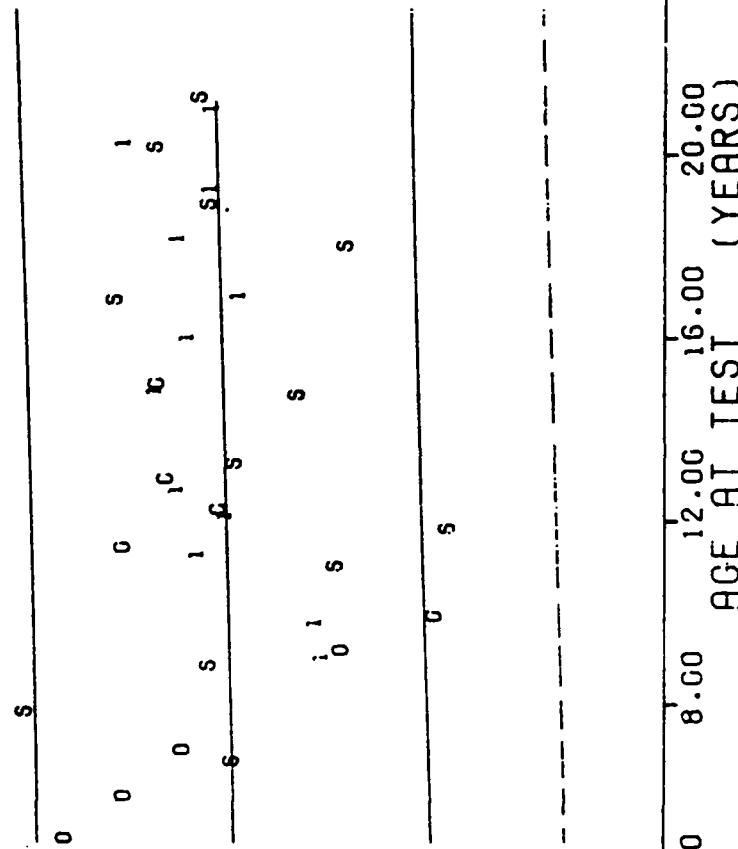
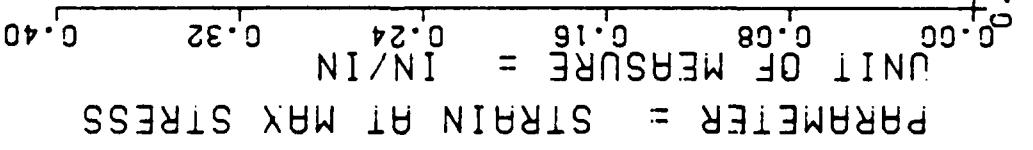


Figure 11

$F = +6.0614175E-01$ $\gamma = ((+1.8462364E-01) + (+4.8648609E-05) ■ X)$
 $R = +5.79323C9E-02$ SIGNIFICANCE OF F = NOT SIGNIFICANT
 $C = +7.7855106E-01$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $N = 182$ DEGREES OF FREEDOM = 180
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



STAGE 1 DISSECTED MOTORS, HIGH RATE CHS=1750 IN/MIN, STRAIN MAX STRESS

Figure 11A

*** LINEAR REGRESSION ANALYSIS ***

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PLK GRUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
107.0	5	+1.4759993E-01	+1.3145107E-02	+1.6199594E-01	+1.3399994E-01	+1.7171585E-01
116.0	6	+1.5049993E-01	+3.3351092E-02	+1.9599997E-01	+1.0499995E-01	+1.7466741E-01
134.0	5	+2.0217990E-01	+4.0187017E-02	+2.2319996E-01	+1.3059997E-01	+1.8057054E-01
144.0	5	+1.8997997E-01	+2.0181864E-02	+2.1459996E-01	+1.6019999E-01	+1.8385004E-01
151.0	5	+2.1135973E-01	+1.0450773E-02	+2.2559994E-01	+1.9729995E-01	+1.8614572E-01
177.0	6	+2.2083312E-01	+9.7075748E-03	+2.3799997E-01	+2.0999997E-01	+1.9467246E-01
191.0	5	+2.0693987E-01	+3.6089004E-02	+2.4839997E-01	+1.5759998E-01	+1.9926375E-01
202.0	6	+1.8431663E-01	+1.7907310E-02	+2.0139998E-01	+1.5649998E-01	+2.0287120E-01
217.0	5	+2.1091991E-01	+8.6918641E-03	+2.2169995E-01	+2.0389997E-01	+2.0779049E-01
230.0	5	+1.9689995E-01	+6.8038571E-03	+2.0349997E-01	+1.8799996E-01	+2.1205383E-01
242.0	6	+2.34633308E-01	+2.7743720E-02	+2.6579999E-01	+1.9159996E-01	+2.1598929E-01
251.0	6	+1.9644987E-01	+5.3150602E-03	+2.0199996E-01	+1.8899995E-01	+2.1894085E-01

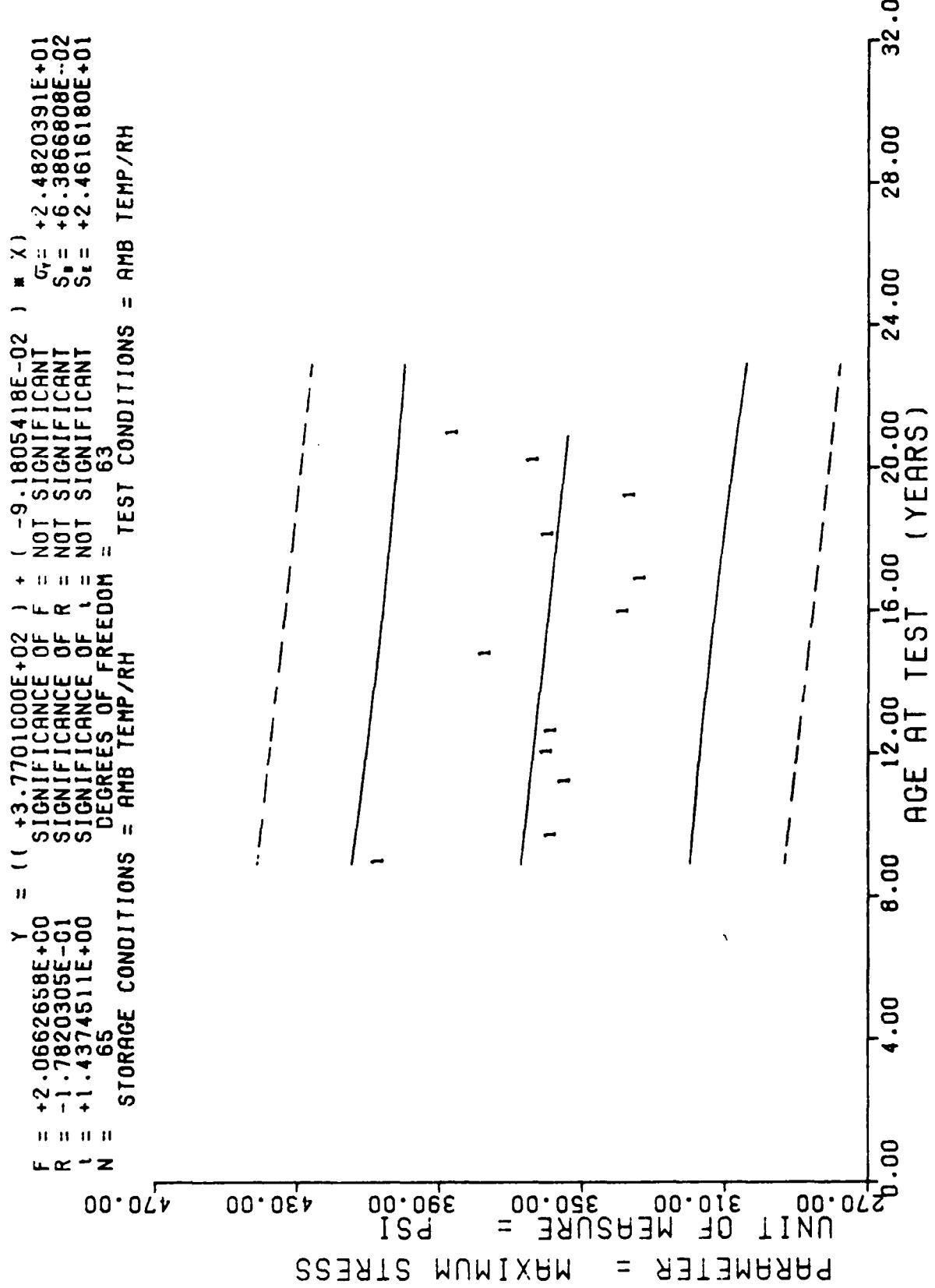


Figure 12

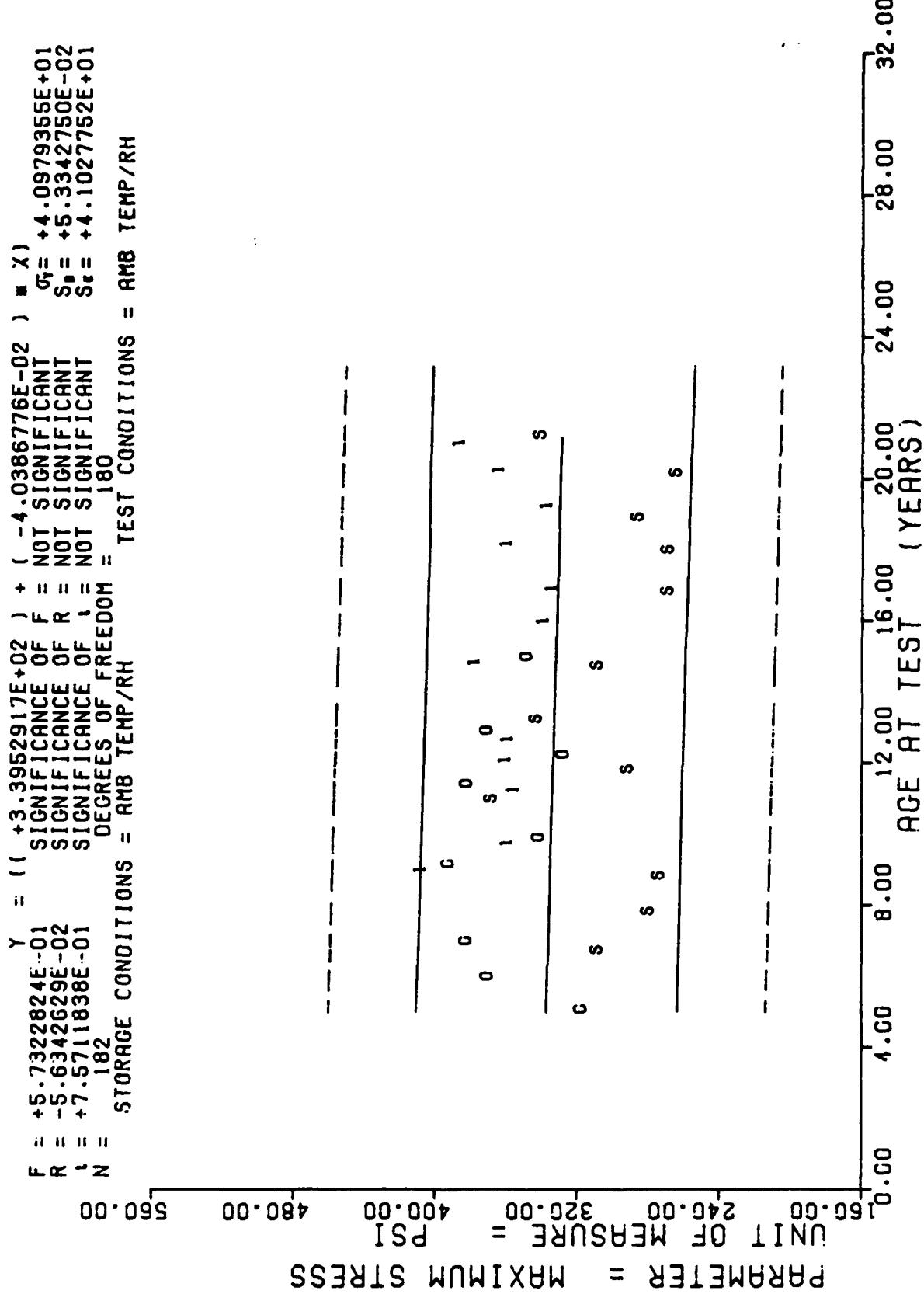


Figure 12A

*** LIGAER KINETIC ANALYSIS ***

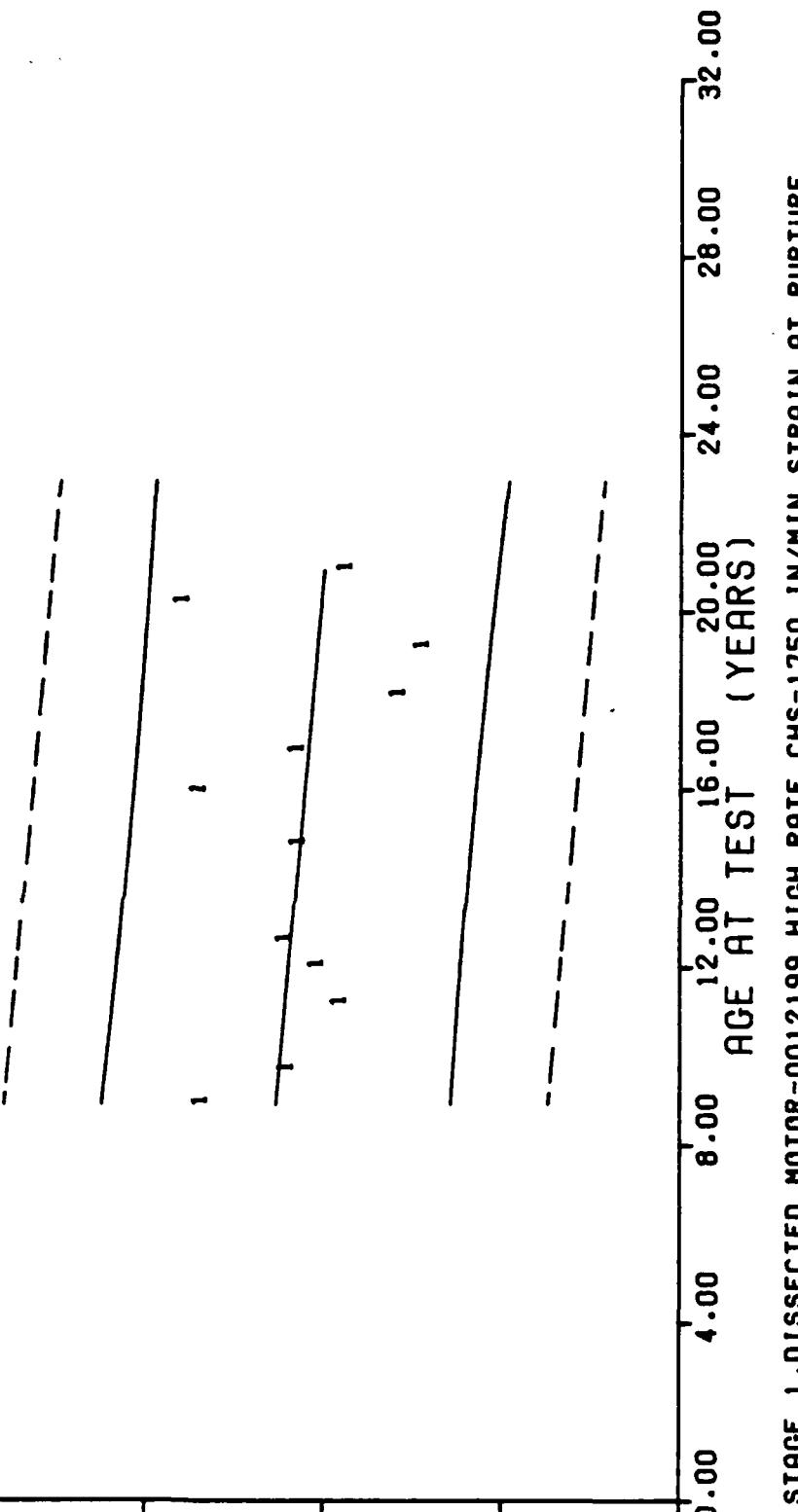
*** ANALYSIS OF TIME SLEEPS ***

ANALYSIS (GEOM.)	DISPLACEMENT (IN. GRAD)	MEAN Y	STANDARD DEVIATION Y	MAXIMUM Y	MINIMUM Y	PRECSSION Y
167.0	6	+4.000000E+02	+4.2154383E+00	+4.200000E+02	+4.000000E+02	+3.6718676E+02
118.0	6	+3.575000E+02	+6.1237243L+00	+3.703000E+02	+3.550000E+02	+3.662E035L+02
154.0	6	+3.5370776L+02	+1.1019034L+01	+3.693253L+02	+3.4551977E+02	+3.6470300E+02
164.0	7	+3.5878586E+02	+1.650524E+01	+3.809293L+02	+3.3694995E+02	+3.6378979E+02
131.0	5	+3.5750390L+02	+6.9630651L+00	+3.7012988L+02	+3.4733984E+02	+3.6314721L+02
177.0	4	+3.7609814F+02	+1.0400236E+01	+4.03645990E+02	+3.5144995E+02	+3.607E025F+02
141.0	5	+3.3750781E+02	+3.2675392L+00	+3.4128977E+02	+3.3345996E+02	+3.5947509F+02
102.0	6	+3.3266479L+02	+3.4120061E+01	+3.627978E+02	+2.9976977E+02	+3.584E508F+02
117.0	7	+3.5852363E+02	+2.1591422E+00	+3.6157583E+02	+3.5661987F+02	+3.570E613F+02
139.0	5	+3.3950195F+02	+4.3301720L+00	+4.4126977L+02	+3.2923990L+02	+3.5589453L+02
142.0	6	+3.6271972L+02	+1.7657354L+01	+3.9601937L+02	+3.5057983E+02	+3.5479296F+02
151.0	6	+3.8516137E+02	+1.4313740L+01	+4.0934980E+02	+3.7025976E+02	+3.5490679E+02

TABLE 1. DISSECTED MOTOR=0012199.0151 RATE CHS=1750 IN/IN. MAXIMUM STRESS.

$y = ((+3.5674617E-01) + (-1.4710134E-04) * x)$
 $F = +1.9441199E+00$ SIGNIFICANCE OF F = NOT SIGNIFICANT
 $R = -1.7301812E-01$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $t = +1.3943170E+00$ SIGNIFICANCE OF t = NOT SIGNIFICANT
 $N = 65$ DEGREES OF FREEDOM = 63
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = STRAIN AT RUPTURE
 UNIT OF MEASURE = IN/IN
 0.16 0.24 0.32 0.40 0.48 0.56

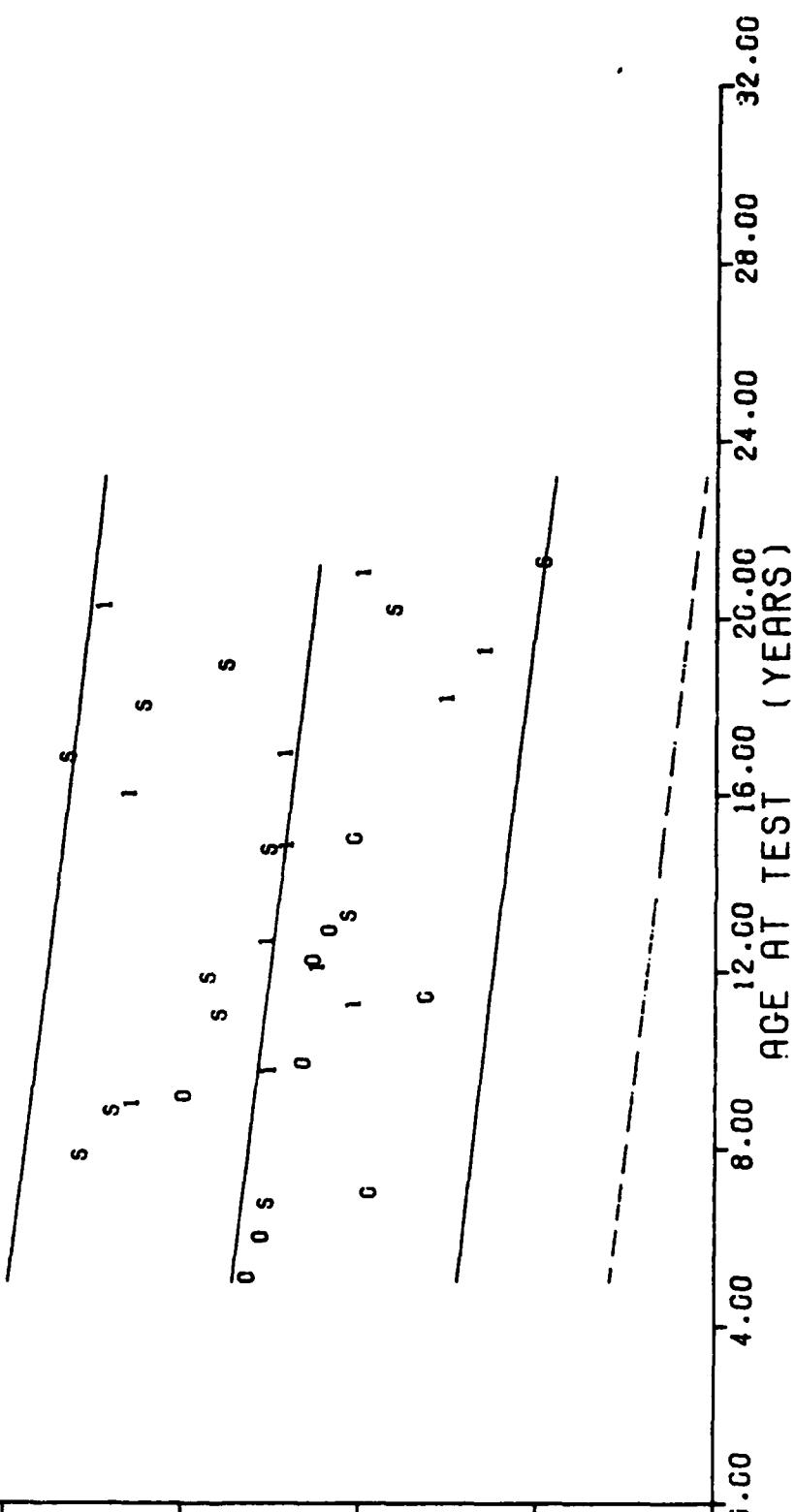


STAGE 1 DISSECTED MOTOR=0012199.HIGH RATE CHS=1750 IN/MIN, STRAIN AT RUPTURE.

Figure 13

$F = +6.9822823E+00$
 $R = -1.9324064E-01$
 $I = +2.6424008E+00$
 $N = 182$
 $\gamma = ((+3.529708CE-01) + (-1.2153740E-04) \equiv X)$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF I = SIGNIFICANT
 DEGREES OF FREEDOM = 180
 STORAGE CONDITIONS = AMB TEMP/RH

PARAMETER = STRAIN AT RUPTURE
 UNIT OF MEASURE = IN/IN
 0.21 0.26 0.31 0.36 0.41 0.46



STAGE 1 DISSECTED MOTORS, HIGH RATE CHS=1760 IN/MIN. STRAIN AT RUPTURE

Figure 13A

* * * * * LUDWIG REINHOLD'S ANALYSIS * * * *

* * * STRAINS OF LIQUID STEEL * * *

ANALYSIS	STRAIN	STANDARD	MAXIMUM Y	MINIMUM Y	PRESSESION Y
(0.001,0.0)	DISPLACEMENT	DISPLACEMENT	DISPLACEMENT	DISPLACEMENT	DISPLACEMENT
1.07*0	5	+3.7259978E-01	+1.5357545E-02	+3.4299999E-01	+3.4100627E-01
1.10*0	6	+3.3010634E-01	+1.3724713E-02	+3.1799955E-01	+3.3968240E-01
1.36*0	5	+3.1019973E-01	+1.4721062E-02	+3.2389959E-01	+3.3703458E-01
1.44*0	5	+3.2057970E-01	+3.6394853E-02	+2.8869998E-01	+3.356354E-01
1.61*0	5	+3.3499902E-01	+1.68217E-02	+3.0099939E-01	+3.1099998E-01
1.77*0	6	+3.2949972E-01	+1.2130567E-02	+3.4379594E-01	+3.1519007E-01
1.91*0	5	+3.7401962E-01	+1.8145567E-02	+3.9229955E-01	+3.4649997E-01
2.07*0	6	+3.2999953E-01	+4.7064620E-02	+3.9599936E-01	+3.2703167E-01
2.17*0	5	+2.3459934E-01	+1.707074E-02	+2.9396946E-01	+3.2482516E-01
2.33*0	5	+3.7379989E-01	+9.3669495E-02	+2.3299939E-01	+3.2291281E-01
2.42*0	6	+3.8133290E-01	+5.3763305E-02	+4.2096554E-01	+3.2114762E-01
2.51*0	6	+3.0816550E-01	+2.0451704E-02	+3.2099959E-01	+3.1982374E-01

Liquid 1.0155110 AUTOR=0012199,0134 FATT, CHG=1750 IN/MIN. STRAIN AT RUPTURE.

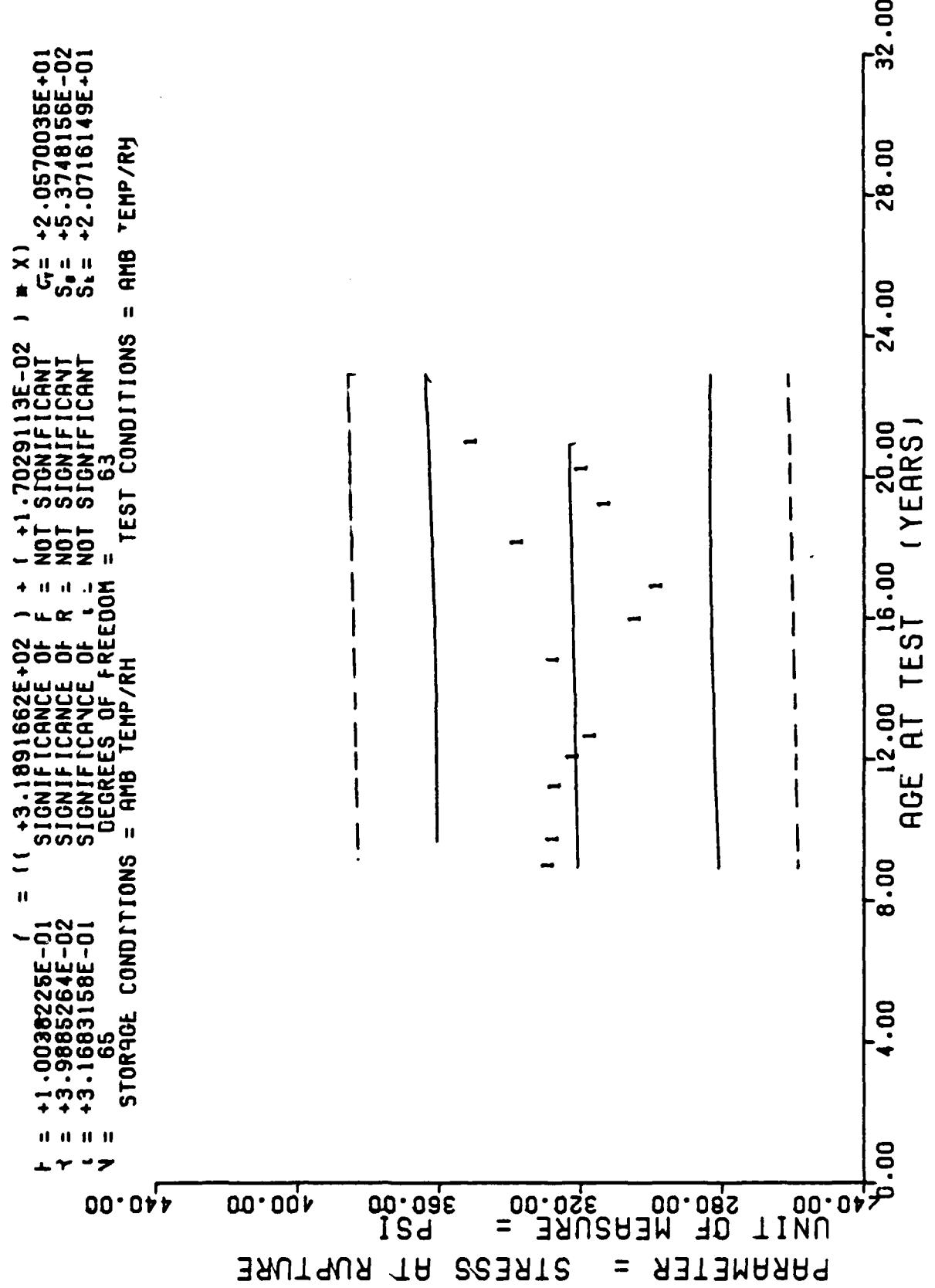


Figure 14

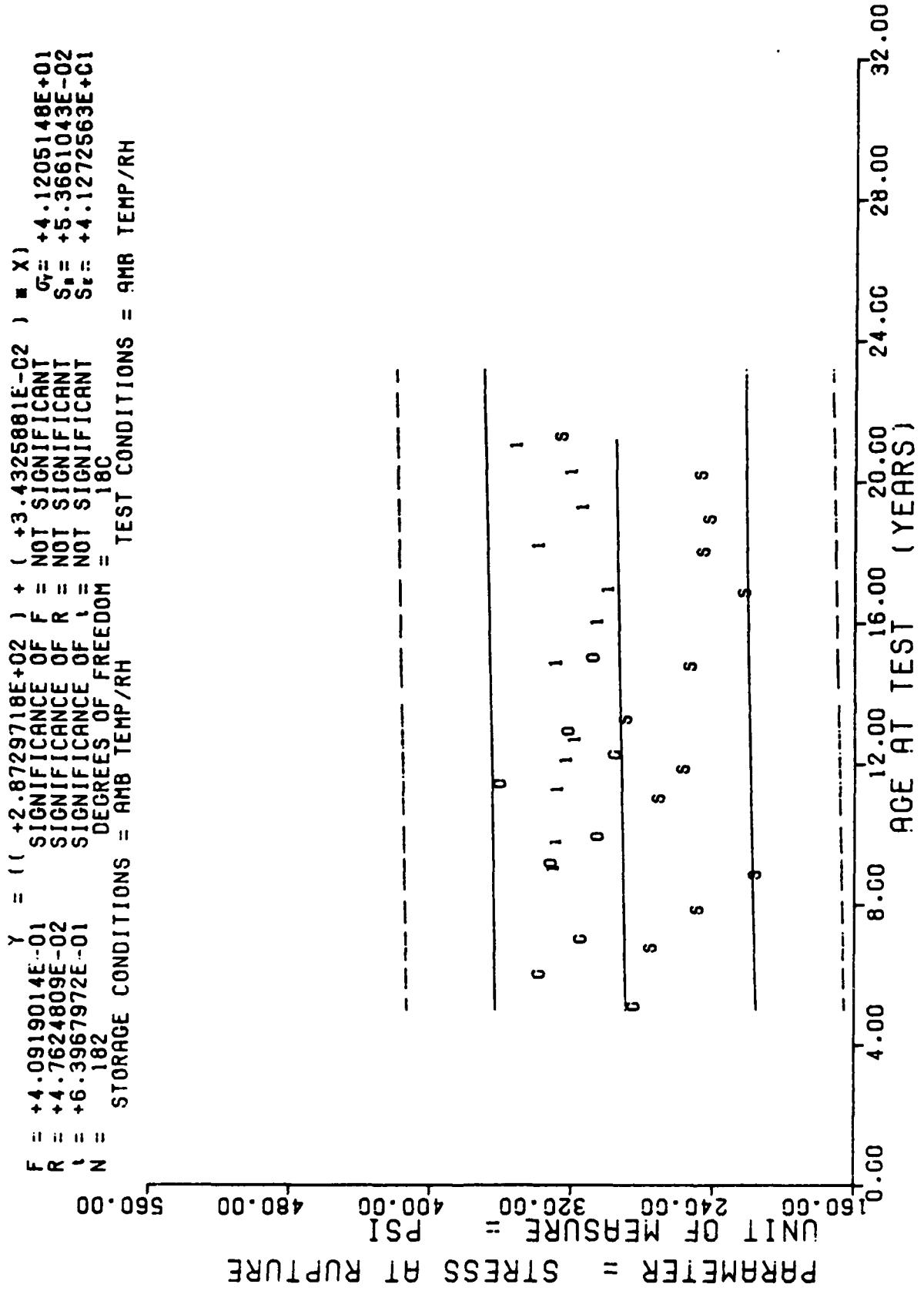


Figure 14A

*** LINEAR REGRESSION ANALYSIS ***

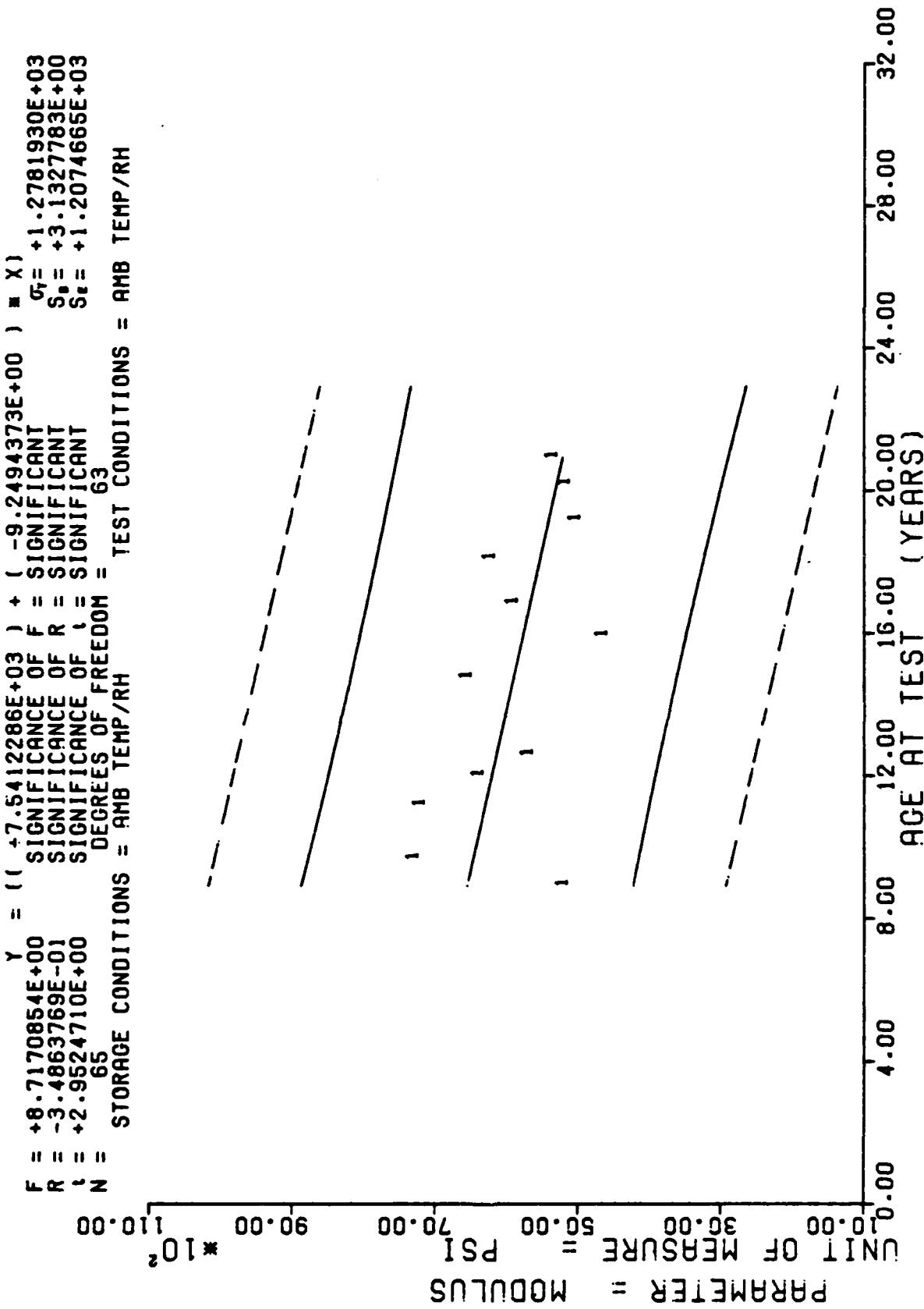
*** ANALYSIS OF TIME SERIES ***

Ave. Calif. (hrs.)	SPE. C.P.H.N.D DATA GROUP	STANDARD		REGRESSION Y	
		MEAN Y	DEVIATION	MAXIMUM Y	MINIMUM Y
1.07 • 0	5	+3.2600000E+02	+7.5823754E+00	+3.3500000E+02	+3.2000000E+02
1.10 • 0	6	+3.2666650E+02	+7.5227720E+00	+3.3500000E+02	+3.2089184E+02
1.34 • 0	5	+3.2600360E+02	+1.2442235E+01	+3.4665991E+02	+3.1779980E+02
1.43 • 0	5	+3.2095335E+02	+2.4116321E+01	+3.3871997E+02	+2.9500000E+02
1.51 • 0	5	+3.1607933E+02	+1.1130769E+01	+3.3305995E+02	+3.0629980E+02
1.77 • 0	6	+3.2666098E+02	+1.5344678E+01	+3.55064990E+02	+3.0910986E+02
1.81 • 0	5	+3.0366791E+02	+3.2310114E+00	+3.0096948E+02	+3.0126977E+02
1.91 • 0	6	+2.5739990E+02	+3.4105447E+01	+3.3969995E+02	+2.6409985E+02
2.17 • 0	5	+3.3689990E+02	+4.1360334E+00	+3.4129980E+02	+3.3139990E+02
2.30 • 0	5	+3.1197993E+02	+5.9607723E+00	+3.1919995E+02	+3.0300000E+02
2.42 • 0	6	+3.1836645E+02	+2.2071578E+01	+3.0150000E+02	+2.9099935E+02
2.61 • 0	6	+3.4976660E+02	+1.4713102E+01	+3.7650000E+02	+3.3569995E+02

TABLE 1. DIESLECTD MOTOR=0012199, HIGH RATE CH5=1750 IN/MIN. STRESS AT RUPTURE.

Figure 15

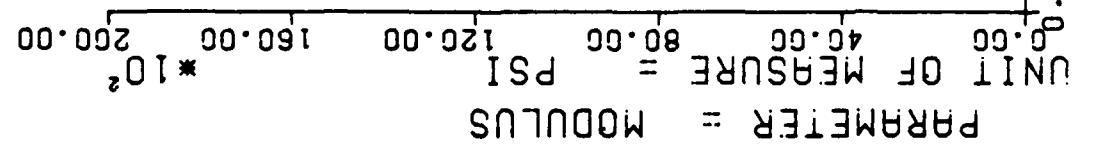
STAGE 1. DISSECTED MOTOR=0012199, HIGH RATE CHS=1750 IN/MIN, MODULUS.



$F = +7.9328545E+00$
 $R = -2.0545342E-01$
 $t = +2.8165323E+00$
 $N = 182$
 STORAGE CONDITIONS = AMB TEMP/RH

$\gamma = ((+7.4008810E+03) + (-6.5293611E+00) * X)$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF t = SIGNIFICANT
 DEGREES OF FREEDOM = 18C

TEST CONDITIONS = AMB TEMP/RH



STAGE 1 DISSECTED MOTORS.HIGH RATE CHS=1750 IN/MIN.MODULUS

*** LINEAR REGRESSION ANALYSIS ***

*** ANALYSIS OF TIME SERIES ***

AGE (HOURS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
107.0	5	+5.160000E+03	+2.6076309E+02	+5.300000E+03	+4.700000E+03	+6.5515351E+03
116.0	6	+7.250000E+03	+4.7217115E+02	+7.900000E+03	+6.900000E+03	+6.4682929E+03
134.0	5	+7.1641992E+03	+1.6984923E+03	+9.252000E+03	+4.772000E+03	+6.3018007E+03
144.0	5	+6.3445976E+03	+1.1460434E+03	+7.506000E+03	+4.489000E+03	+6.2093085E+03
151.0	5	+5.6535970E+03	+1.2753544E+03	+6.705000E+03	+4.007000E+03	+6.1445625E+03
177.0	6	+6.5138320E+03	+1.5559174E+03	+8.406000E+03	+4.225000E+03	+5.9040781E+03
191.0	5	+4.615000E+03	+1.1406537E+03	+5.951000E+03	+3.478000E+03	+5.7745859E+03
202.0	6	+5.8655000E+03	+5.8876727E+02	+6.666000E+03	+5.112000E+03	+5.6728398E+03
217.0	5	+6.1871992E+03	+1.8057429E+02	+6.440000E+03	+5.970000E+03	+5.5340976E+03
230.0	5	+4.9920000E+03	+1.5038772E+03	+6.2230000E+03	+2.255000E+03	+5.4138554E+03
242.0	6	+5.1380000E+03	+1.0026835E+03	+7.057000E+03	+4.233000E+03	+5.3028632E+03
- 251.0	6	+5.3113320E+03	+6.8442520E+02	+6.2910000E+03	+4.6170000E+03	+5.2196171E+03

STAGE 1, DISSECTED MOTOR=0012193, HIGH RATE CHS=1750 IN/MIN, MODULUS.

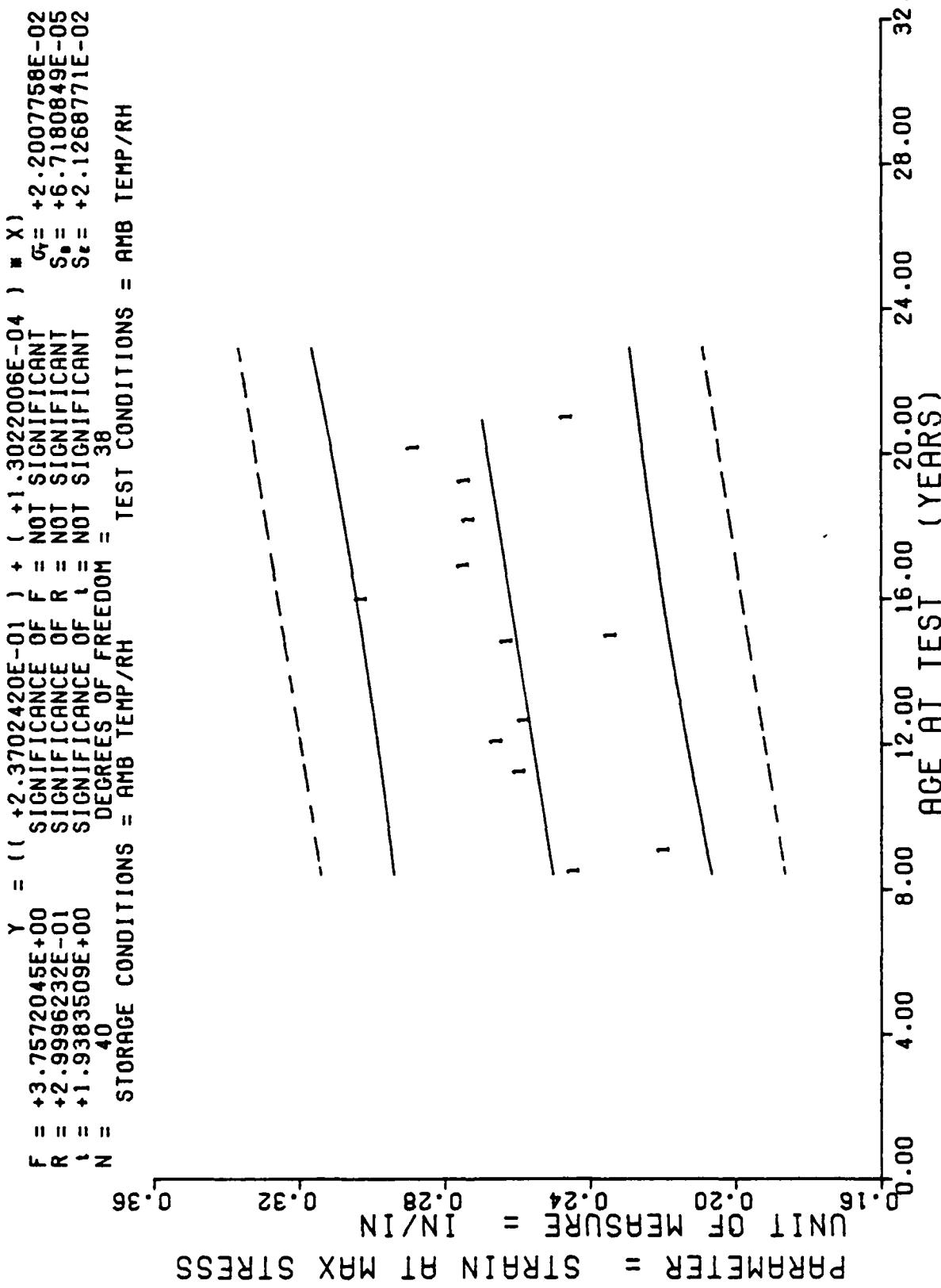
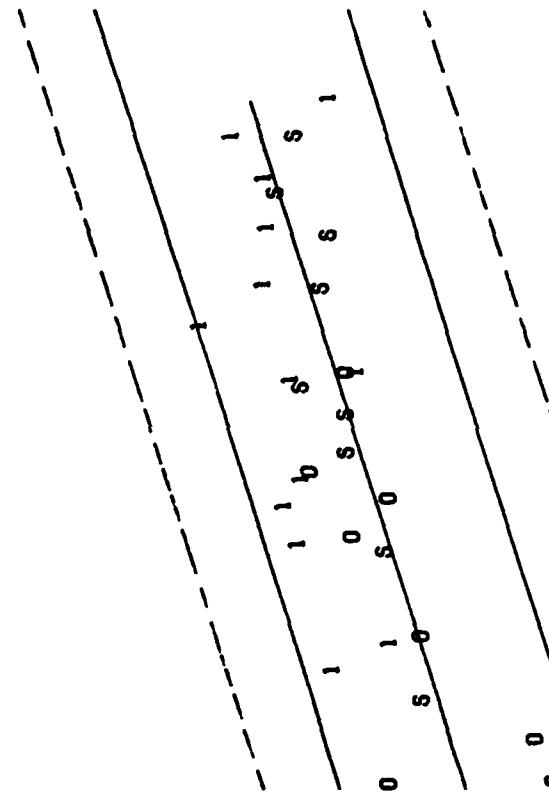


Figure 16

$\gamma = ((+1.5011907E-01) + (+5.2394432E-04) * X) * X$
 $F = +9.5530734E+01$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = +7.2146813E-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $t = +9.7739825E+00$ SIGNIFICANCE OF t = SIGNIFICANT
 $N = 90$ DEGREES OF FREEDOM = 88
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = STRAIN AT MAX STRESS
 UNIT OF MEASURE = IN/IN
 0.00 0.08 0.16 0.24 0.32 0.40 0.48



DISSECTED TP-H1011.H.R.TRIAXIAL CHS=1750 IN/MIN.600 PSI.STRAIN MAX STRS.

Figure 16A

**** LINEAR REGRESSION ANALYSIS ****

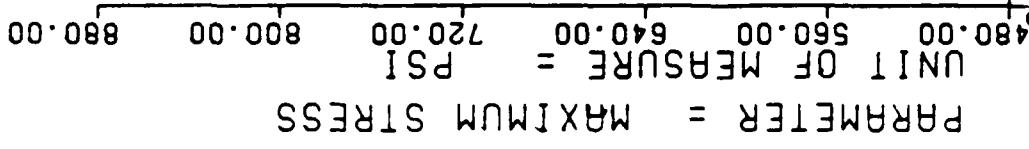
*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PLK GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
101.0	3	+2.4333328E-01	+1.0503744E-02	+2.5399994E-01	+2.3299998E-01	+2.5017642E-01
108.0	2	+2.1849995E-01	+7.7784373E-03	+2.2399997E-01	+2.1299999E-01	+2.5108790E-01
134.0	4	+2.5824975E-01	+2.3615550E-02	+2.8199994E-01	+2.3599994E-01	+2.5447368E-01
144.0	2	+2.6454997E-01	+1.7747857E-04	+2.6459597E-01	+2.6449996E-01	+2.5577586E-01
151.0	3	+2.5686663E-01	+4.0054300E-03	+2.6069998E-01	+2.5269997E-01	+2.5668740E-01
177.0	3	+2.6166659E-01	+1.1150359E-02	+2.6999598E-01	+2.4899995E-01	+2.6007312E-01
179.0	1	+2.3299998E-01	+0.000000E+07	+2.3299998E-01	+2.3299998E-01	+2.6033353E-01
191.0	3	+3.0156660E-01	+9.2083226E-03	+3.0909997E-01	+2.9129999E-01	+2.6189619E-01
202.0	3	+2.73633330E-01	+4.9090398E-03	+2.7929997E-01	+2.7059996E-01	+2.6332861E-01
217.0	3	+2.7209997E-01	+1.8350040E-02	+2.3599995E-01	+2.5129997E-01	+2.6528191E-01
230.0	3	+2.7326661E-01	+7.5814519E-03	+2.7989995E-01	+2.6499998E-01	+2.66997480E-01
241.0	3	+2.3733325E-01	+5.5081478E-03	+2.9299998E-01	+2.8199994E-01	+2.6840722E-01
251.0	7	+2.4528557E-01	+4.2774511E-03	+2.5199997E-01	+2.4099999E-01	+2.6970940E-01

STAGE 1, DISCTED MOTOR=0012199, TRIAXIAL CHS=1750 IN/MIN.600 PSI. STRAIN MAX STRS.

$F = +4.5243806E+00$ $\gamma = 11 +5.8352356E+02$ $\sigma_f = +2.35564312E-01$ $S_f = +3.6623412E+01$
 $R = +3.2618243E-01$ SIGNIFICANCE OF F = SIGNIFICANT
 $v = +2.1270591E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $N = 40$ SIGNIFICANCE OF γ = SIGNIFICANT
DEGREES OF FREEDOM = 38

STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



STAGE 1 .DISCTED MOTOR=0012199 .TRIAxIAL CHS=1750 IN/MIN.600 PSI .MAXIMUM STRESS.

Figure 17

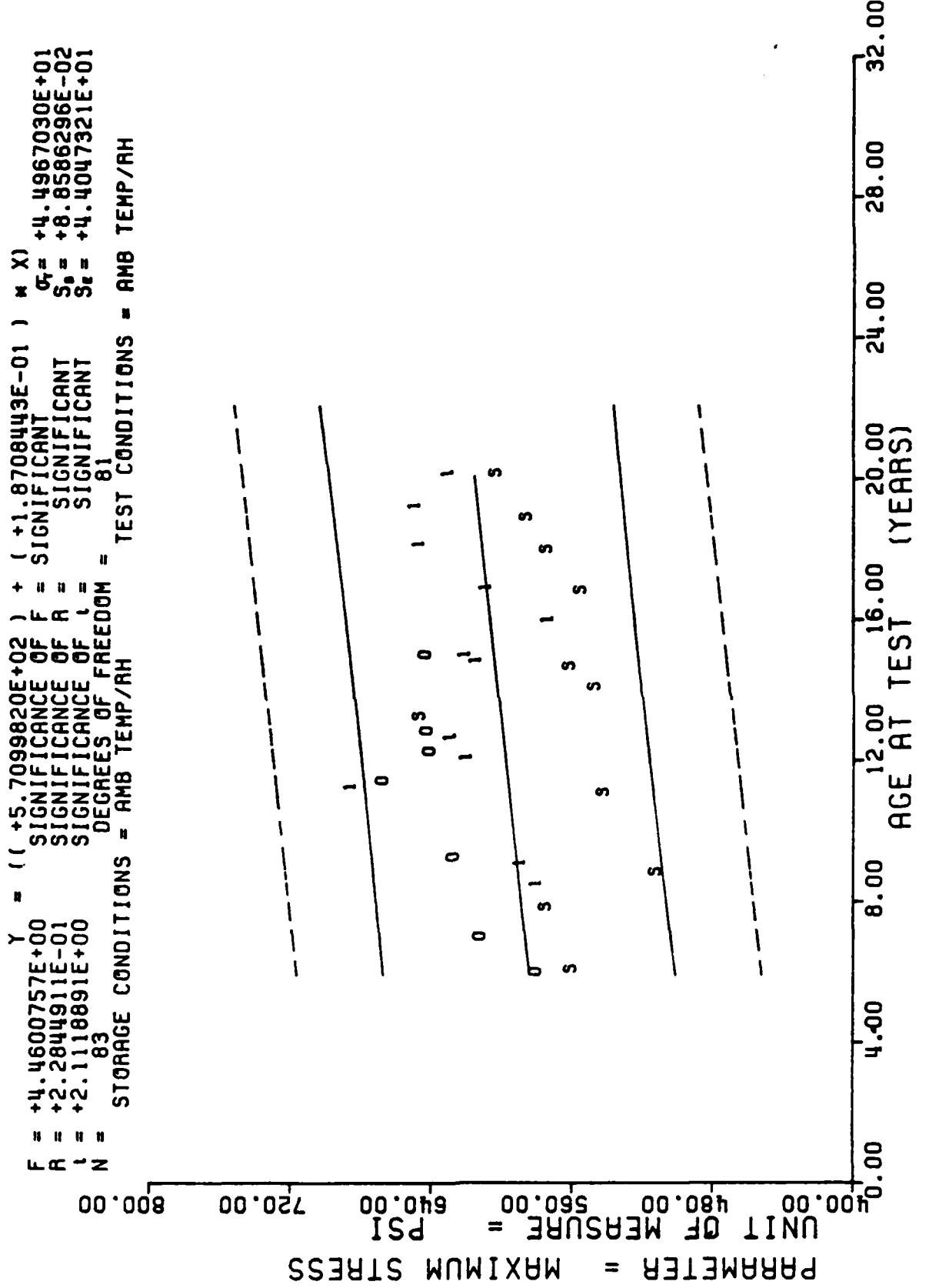
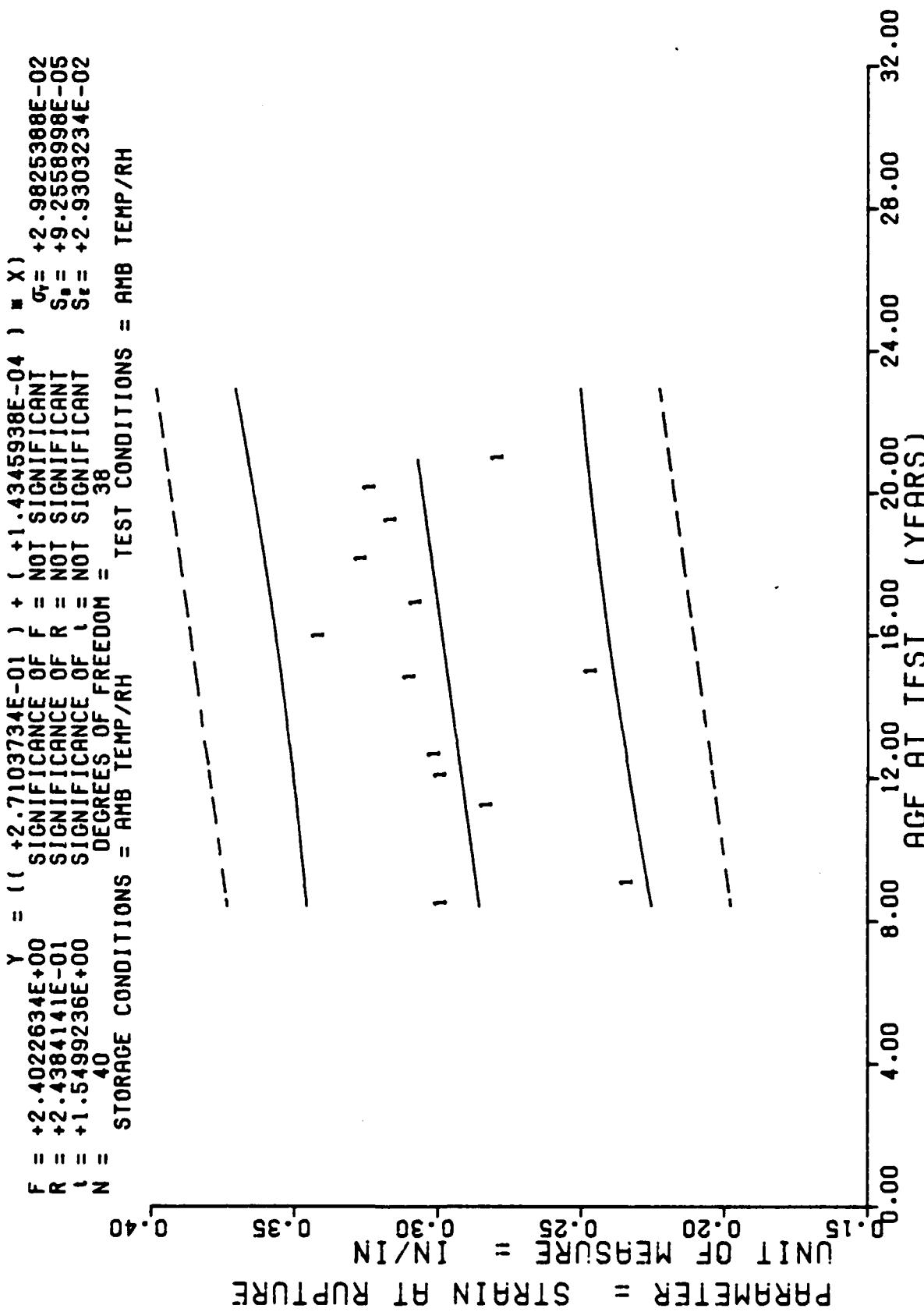


Figure 17A

**** LINEAR REGRESSION ANALYSIS ****
 **** ANALYSIS OF TEST SERIES ****

TEST (AVERAGE)	SPECIMENS PER GROUP	STANDARD		MAXIMUM Y	MINIMUM Y	REGRESSION Y
		DEVIATION	DEVIATION			
1.01±0	3	+5.7636301E+02	+3.3463439E+00	+5.873E987E+02	+5.7091992E+02	+6.0732348E+02
1.04±0	2	+5.3750000L+02	+3.355339L+00	+5.9000000L+02	+5.8500000E+02	+6.0897290E+02
1.04±0	4	+6.8J845335E+02	+1.7545287E+01	+7.0579580E+02	+6.6309985E+02	+6.1509960E+02
1.04±0	2	+6.1826439E+02	+1.7449432E+01	+6.3059585E+02	+6.0592993E+02	+6.1745605E+02
1.04±0	3	+6.2729321E+02	+1.1372668E+01	+6.3505981E+02	+6.1425000E+02	+6.1910546E+02
1.07±0	3	+6.1272973E+02	+1.1471972E+01	+6.2438989E+02	+6.0209985E+02	+6.2523217E+02
1.09±0	1	+6.1889990E+02	+0.0000000L+07	+6.1869690L+02	+6.1889990E+02	+6.2570361E+02
1.01±0	3	+5.7182324E+02	+9.0138333E+03	+5.7920596L+02	+5.6095996E+02	+6.2853125F+02
-0.01±0	3	+6.0717051E+02	+5.5697278E+00	+6.1257983E+02	+6.0143994E+02	+6.3112329E+02
0.17±0	3	+6.4525976E+02	+2.3294733L+01	+6.7731982L+02	+6.2669995L+02	+6.3465795E+02
2.50±0	3	+6.4702304E+02	+1.1927594E+01	+6.5552578E+02	+6.1889990E+02	+6.3772143E+02
-0.41±0	2	+6.2386937L+02	+1.2232940L+01	+6.4069995E+02	+6.1616992E+02	+6.4031347E+02
-0.41±0	7	+6.3520361E+02	+5.1246162E+01	+6.8344995E+02	+5.8785936E+02	+6.42666992E+02

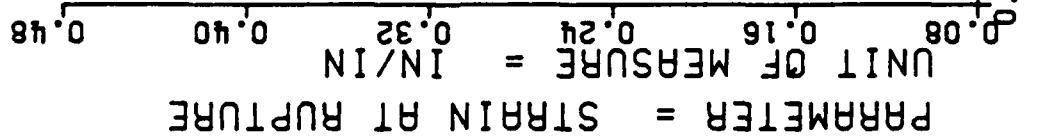
TABLE 1. DISCTED MULUR=0012190, TRIAXIAL CHS=1750 IN/MIN.000 PSI, MAXIMUM STRESS.



STAGE 1.DISCTED MOTOR=0012199.TRIAXIAL CHS=1750 IN/MIN.600 PSI. STRAIN AT RUPT.

Figure 18

$F = +8.1054701E+01$ $\gamma = ((+1.9652909E-01) + (+5.3325896E-04) \times X)$
 $R = +7.0722611E-01$ F = SIGNIFICANT
 $S_1 = +9.0030384E+00$ F R = SIGNIFICANT
 $N = 83$ DEGREES OF FREEDOM = 81
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



DISSECTED TP-H1011, H.R. TRIAXIAL CHS=1750 IN/MIN, 600 PSI, STRAIN AT RUPTURE

Figure 18A

**** LINEAR REGRESSION ANALYSIS ****

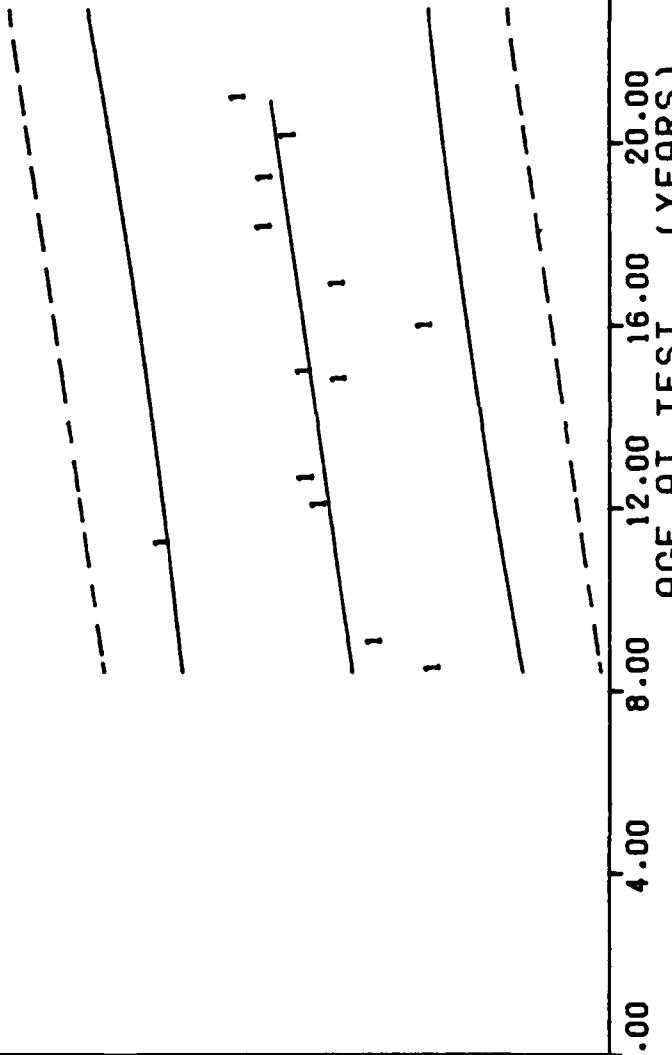
*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
101.0	3	+2.9733324E-01	+1.6041907E-02	+3.1399995E-01	+2.8199994E-01	+2.8552669E-01
108.0	2	+2.3249995E-01	+1.2021142E-02	+2.4099999E-01	+2.2399997E-01	+2.8653091E-01
134.0	4	+2.8149986E-01	+2.9012293E-02	+3.0699998E-01	+2.5299996E-01	+2.9026085E-01
144.0	2	+2.9749995E-01	+9.7593888E-03	+3.0439996E-01	+2.9059994E-01	+2.9169547E-01
151.0	3	+2.9966658E-01	+1.2503392E-02	+3.1399995E-01	+2.9099994E-01	+2.9269969E-01
177.0	3	+3.0833327E-01	+2.0647064E-02	+3.3199995E-01	+2.9399996E-01	+2.9642963E-01
179.0	1	+2.4499994E-01	+0.0000000E+07	+2.4499994E-01	+2.4499994E-01	+2.9671657E-01
191.0	3	+3.4026652E-01	+5.4680221E-03	+3.4589999E-01	+3.3499997E-01	+2.9843807E-01
202.0	3	+3.0616664E-01	+4.9918559E-03	+3.1169998E-01	+3.0199998E-01	+3.001610E-01
217.0	3	+3.2533329E-01	+3.7166382E-02	+3.5599994E-01	+2.8399997E-01	+3.0216801E-01
230.0	3	+3.1499993E-01	+1.5522556E-02	+3.2999998E-01	+2.9899996E-01	+3.0403298E-01
241.0	3	+3.2233327E-01	+9.2899460E-03	+3.2999998E-01	+3.1999997E-01	+3.0561101E-01
251.0	7	+2.7771401E-01	+9.9008212E-03	+2.8899997E-01	+2.6599997E-01	+3.0704563E-01

STAGE 1. DISCTED MOTOR=0012199,TRIAXIAL CHS=1750 IN/MIN,600 PSI STRAIN AT RUPT.

$\gamma = ((+5.6811758E+02) + (+2.3782797E-01) * X)$
 $F = +4.3357988E+00$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = +3.2002262E-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $I = +2.0822581E+00$ SIGNIFICANCE OF I = SIGNIFICANT
 $N = 40$ DEGREES OF FREEDOM = 38
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = PSI
 PARAMETER = STRESS AT RUPTURE
 480.00 560.00 640.00 720.00 800.00 880.00



STAGE 1 DISCITED MOTOR=0012199, TRIAXIAL CHS=1750 IN/MIN, 600 PSI, STRESS AT RUPT.

Figure 19

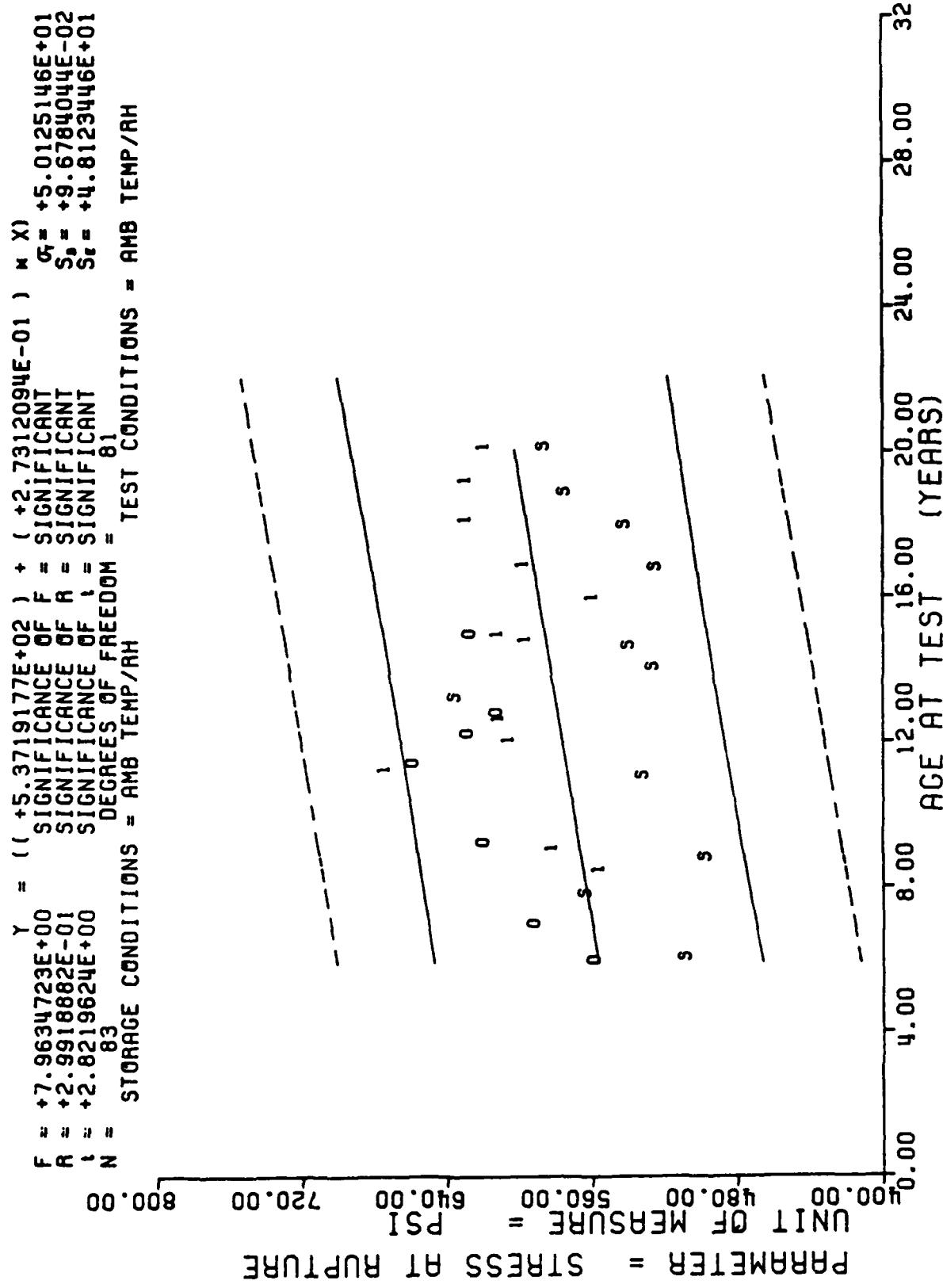


Figure 19A

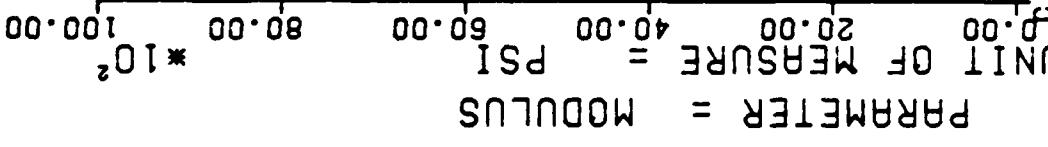
*** LINEAR REGRESSION ANALYSIS ***

*** ANALYSIS OF TIME SERIES ***

Age (months)	SPECSIMS MATERIAL	STANDARD DEVIATION	REGRESSION Y	
			MEAN Y	MAXIMUM Y
101.0	3	+5.5439990E+02	+1.2138417E+01	+5.6789990E+02
108.0	2	+5.8000000E+02	+7.0710678E+00	+5.8500000E+02
134.0	4	+6.7267480E+02	+1.7404708E+01	+6.9689990E+02
144.0	2	+6.0435473E+02	+1.9063322E+01	+6.1782983E+02
151.0	3	+6.0989990E+02	+8.8692548E+00	+6.1939990E+02
177.0	3	+5.9539990E+02	+9.6067201E+00	+6.0519995E+02
179.0	1	+6.1069995E+02	+0.0000000E+07	+6.1069995E+02
191.0	3	+5.5800976E+02	+1.0816872E+01	+5.7008984E+02
202.0	3	+5.9619628E+02	+5.5844651E+00	+6.0226977E+02
217.0	3	+6.2813305E+02	+3.5056925E+01	+6.6859985E+02
230.0	3	+6.2783325E+02	+2.0557519E+01	+6.4489990E+02
241.0	3	+6.1773974E+02	+9.8289121E+00	+6.2750000E+02
251.0	7	+6.3955517E+02	+3.0278197E+01	+6.6539990E+02

STAGE 1, DISC1LD MOTOR=0012199, TRIAXIAL CHS=1750 IN/MIN,600 PSI, STRESS AT RUPT.

$F = +1.0157907E-01$
 $R = +5.1633389E-02$
 $t = +3.1871471E-01$
 $N = 40$
 $y = ((+5.1901988E+03) + (+8.4013425E-01) * X)$
 $F = \text{SIGNIFICANT}$
 $R = \text{NOT SIGNIFICANT}$
 $t = \text{NOT SIGNIFICANT}$
 $N = \text{NOT SIGNIFICANT}$
 $\text{DEGREES OF FREEDOM} = 38$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$



STAGE 1 .DISSECTED MOTOR=0012199,TRIAXIAL CHS=1750 IN/MIN,600 PSI,MODULUS.

Figure 20

$\gamma = ((+7.9480071E+03) + (-1.3296515E+01) \times X)$
 $F = +2.7217889E+01$ $F = SIGNIFICANT$
 $R = -5.0150780E-01$ $R = SIGNIFICANT$
 $I = +5.2170767E+00$ $I = SIGNIFICANT$
 $N = 83$ DEGREES OF FREEDOM = 81
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = PSI
 $\times 10^2$

PARAMETER = MODULUS

DISSECTED TP-H1011, H.R. TRIAXIAL CHS=1750 IN/MIN. 600 PSI. MODULUS

Figure 20A

*** LUDWIG TRIAXIAL TEST ANALYSIS ***

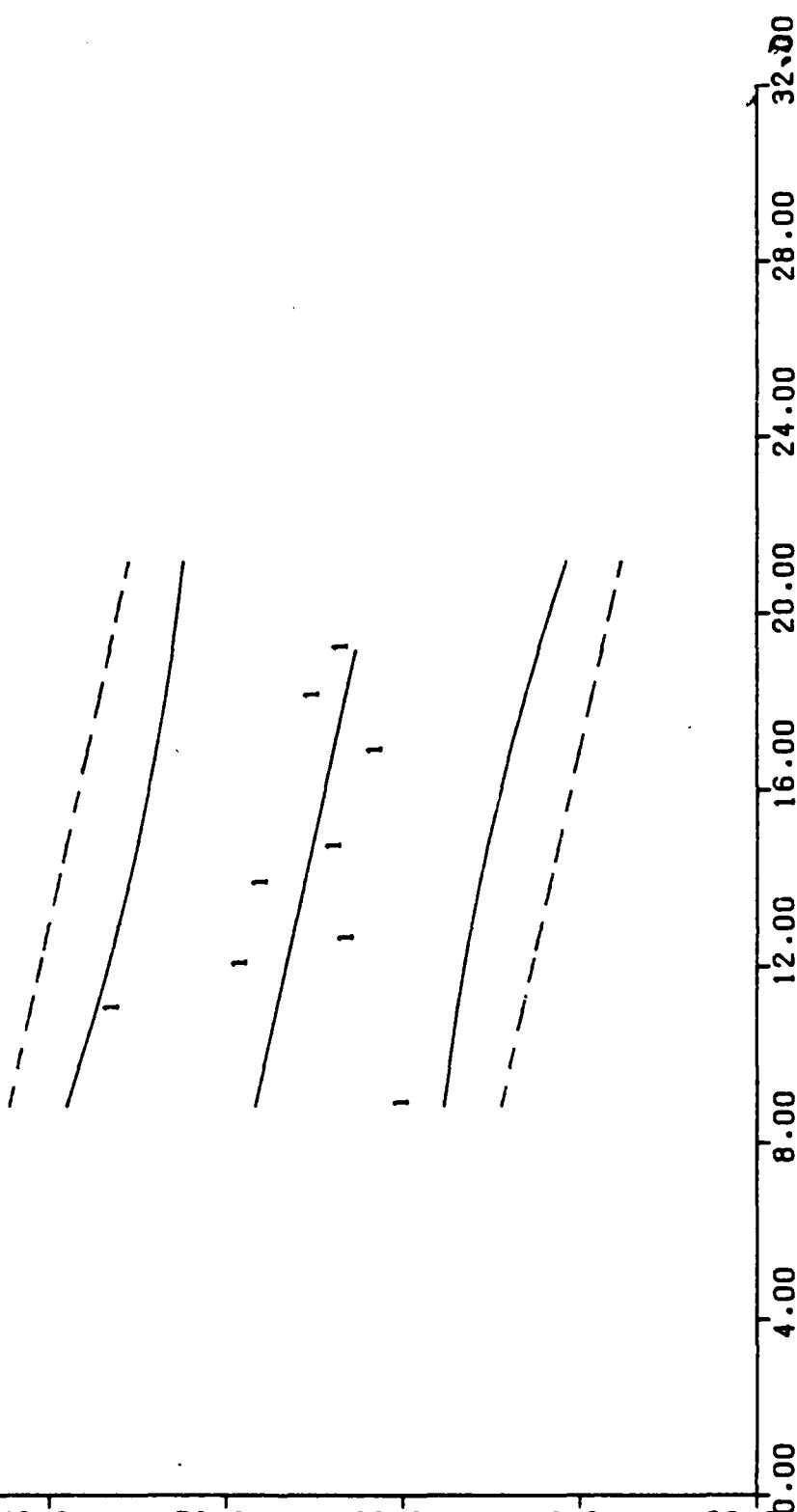
* * * ANALYSIS OF TEST 20115 * * *

(X, Y, Z)	STANDARD DEFINITION	MAXIMUM Y	MINIMUM Y	PROGRESSION Y
1.0 0.0	3 +5.3115320L+03	+3.9279426L+02	+6.1640000L+03	+5.3880000E+03
1.0 0.3	2 +6.1000000E+03	+1.4142135L+02	+6.2000000F+03	+5.2809296F+03
1.4 0.0	4 +5.4572500F+03	+1.4371335L+03	+7.5630000L+03	+5.3027734F+03
1.4 0.0	2 +6.2200000L+03	+4.5254333L+01	+5.2520000L+03	+5.1800000F+03
1.4 1.0	0 +4.1350040F+03	+5.3507421L+02	+4.7156000L+03	+3.5450000E+03
1.7 0.0	3 +5.3960000E+03	+7.2776319L+02	+6.0000000L+03	+4.5880000E+03
1.7 0.0	1 +4.9180000L+03	+0.0000000E+07	+4.9180000E+03	+5.3405820F+03
1.7 1.0	3 +3.9935332L+03	+2.1359281L+02	+4.2350000F+03	+3.8490000F+03
1.7 1.0	5 +5.0020000L+03	+3.2704576L+02	+5.3790000C+03	+5.2950000E+03
1.7 0.0	3 +6.3780040E+03	+2.3590044L+02	+6.3510000F+03	+5.9350000F+03
1.7 0.0	3 +5.6190000E+03	+5.6930283L+02	+6.0690000L+03	+5.0600000L+03
1.4 1.0	3 +4.7363520L+03	+1.4218239L+02	+4.3630000L+03	+4.5820000F+03
1.4 1.0	7 +5.0480554L+03	+3.6410411L+02	+6.3960000E+03	+5.2840000E+03

TEST 20115 CLO MULR=0012199, TRIAXIAL CHS-1750 IN/MIN,000 PSI, MODULUS.

$Y = ((+1.3265450E-03) + (-1.8222149E-06)) * X$
 $F = +2.8423755E+00$ SIGNIFICANCE OF F = NOT SIGNIFICANT
 $R = -3.3825495E-01$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $t = +1.6869346E+00$ SIGNIFICANCE OF t = NOT SIGNIFICANT
 $N = 24$ DEGREES OF FREEDOM = 22
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = COMPLIANCE
 UNIT OF MEASURE = INCHIN/LBS $* 10^{-2}$
 0.00 0.04 0.08 0.12 0.16 0.20



STAGE 1, DISCTED MOTOR=00012099, CREEP 10 LB LOAD, COMPLIANCE AT 10 SEC.

Figure 21

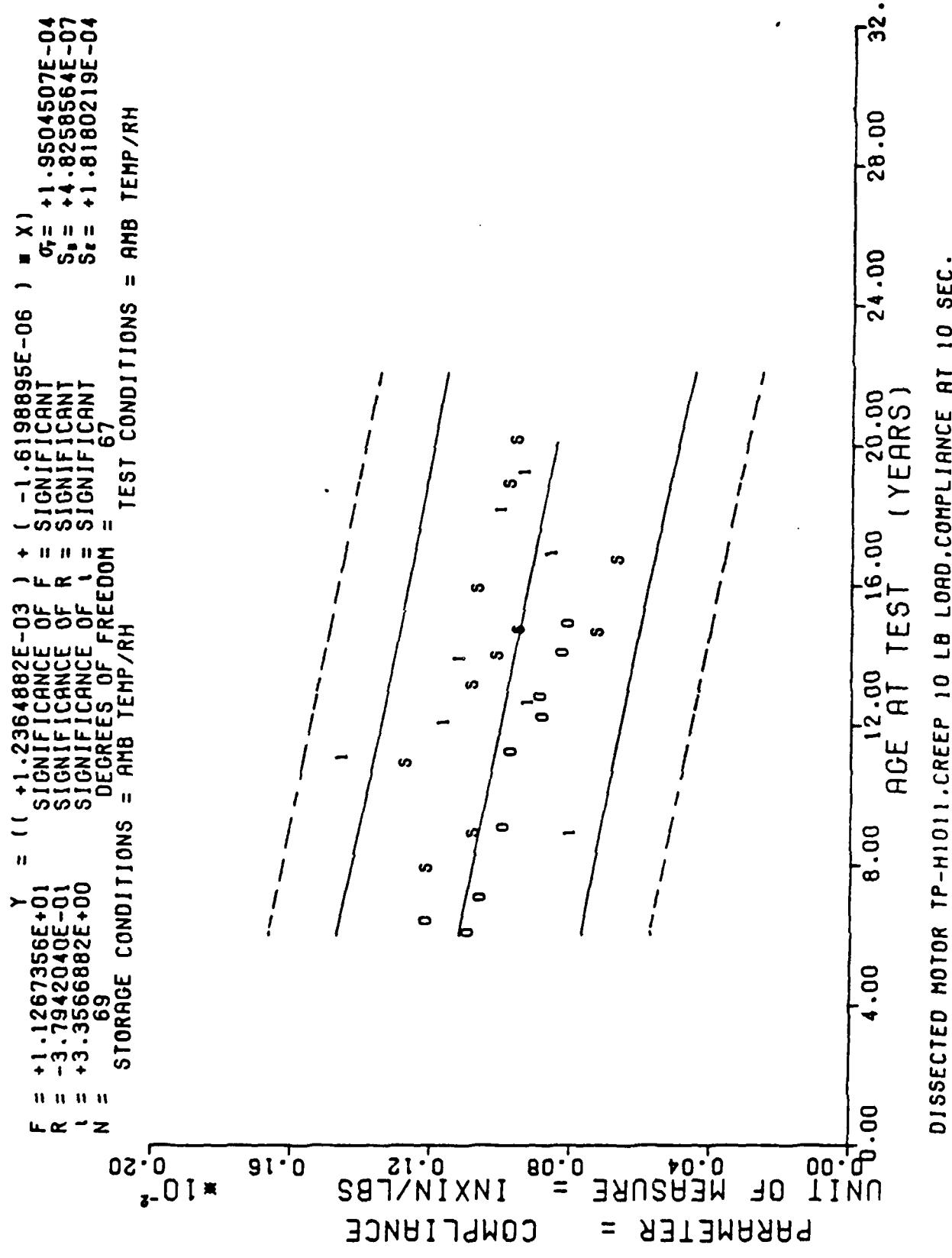


Figure 21A

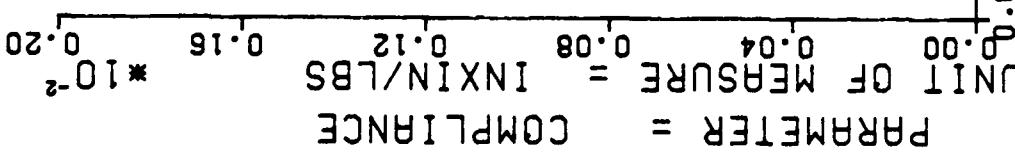
**** LINEAR REGRESSION ANALYSIS ****
 *** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	1	+7.8999996E-04	+0.000000E+07	+7.8999996E-04	+7.8999996E-04	+1.1333900E-03
132.0	2	+1.4449998E-03	+7.7734788E-05	+1.4999997E-03	+1.3899998E-03	+1.0860124E-03
144.0	2	+1.1549997E-03	+6.3638460E-05	+1.1999598E-03	+1.1099998E-03	+1.0641459E-03
151.0	4	+9.1499974E-04	+1.4387380E-04	+1.1299999E-03	+8.2999980E-04	+1.0513905E-03
166.0	3	+1.1099998E-03	+1.0816609E-04	+1.1999988E-03	+9.8999985E-04	+1.0240571E-03
176.0	3	+9.4333314E-04	+9.8658726E-05	+1.009997E-03	+8.2999980E-04	+1.0058351E-03
202.0	3	+8.4999972E-04	+3.6052453E-05	+8.7999994E-04	+8.0999988E-04	+9.5845758E-04
217.0	3	+9.9333305E-04	+1.2701651E-04	+1.1399998E-03	+9.1999978E-04	+9.3112420E-04
230.0	3	+9.2666642E-04	+1.7039168E-04	+1.0899999E-03	+7.4999999E-04	+9.0743554E-04

STAGL 1.DISCTED MOTOR=0012099.CREEP 10 LB LOAD,COMPLIANCE AT 10 SEC.

$F = +2.9714387E+00$
 $R = -3.4495433E-01$
 $t = +1.7237861E+00$
 $N = 24$
 STORAGE CONDITIONS = AMB TEMP/RH

$Y = ((+1.4678366E-03) + (-2.0113530E-06) * X)$
 SIGNIFICANCE OF F = NOT SIGNIFICANT
 SIGNIFICANCE OF R = NOT SIGNIFICANT
 SIGNIFICANCE OF t = NOT SIGNIFICANT
 DEGREES OF FREEDOM = 22
 TEST CONDITIONS = AMB TEMP/RH



STAGE 1. DISCITED MOTOR=0012199.CREEP 10 LB LOAD.COMPLIANCE AT 20 SEC.

Figure 22

$F = +1.6576129E+01$
 $R = -4.4534895E-01$
 $I = +4.0713793E+00$
 $N = 69$
 $\gamma = ((+1.498267E-03) + (-2.1518936E-06) \cdot X) /$
 $S_r = +2.2074488E-04$
 $S_s = +5.2854168E-07$
 $S_t = +1.9911499E-04$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF I = SIGNIFICANT
 DEGREES OF FREEDOM = 67
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

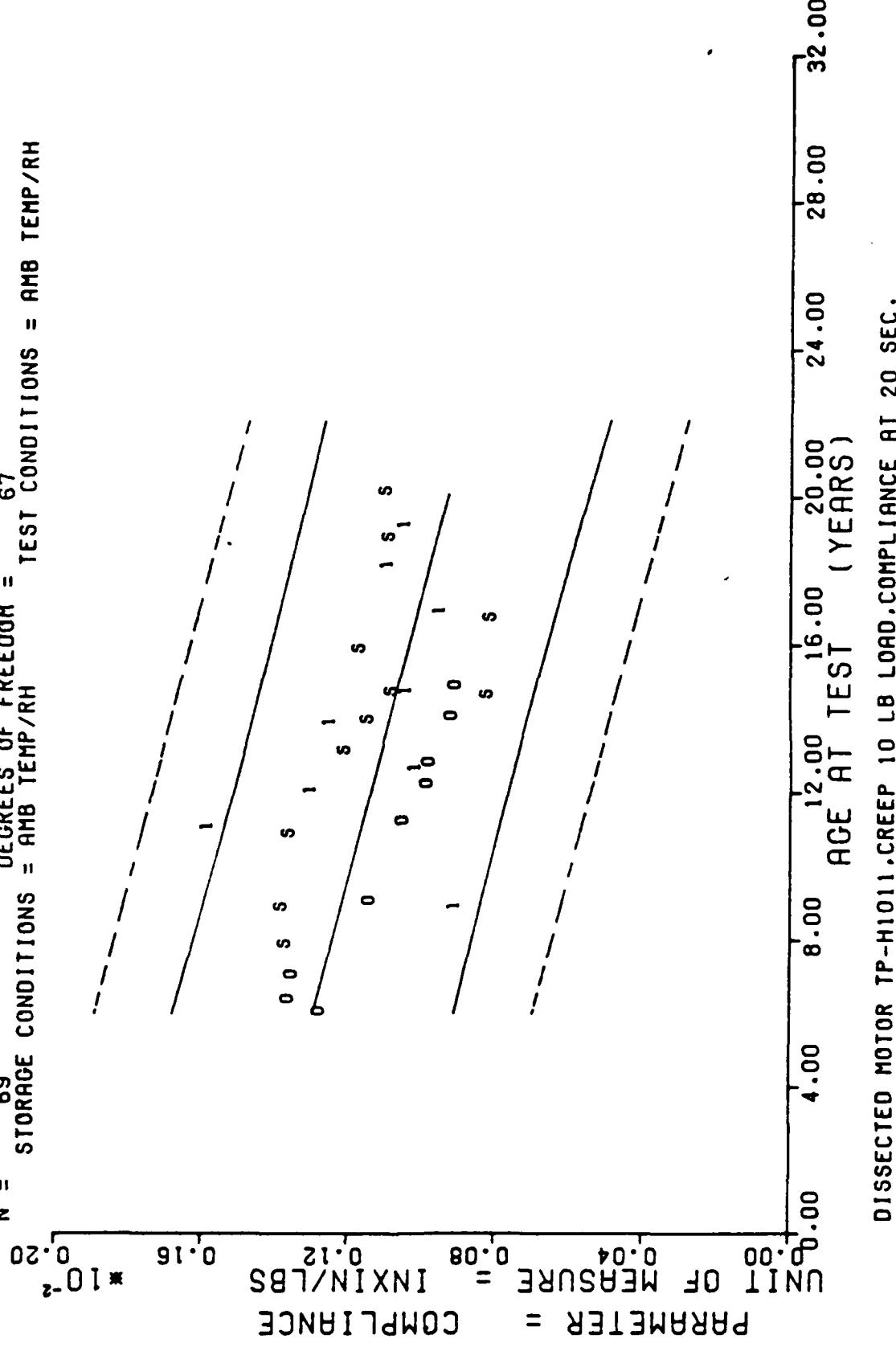


Figure 22A

*** LINEAR REGRESSION ANALYSIS ***

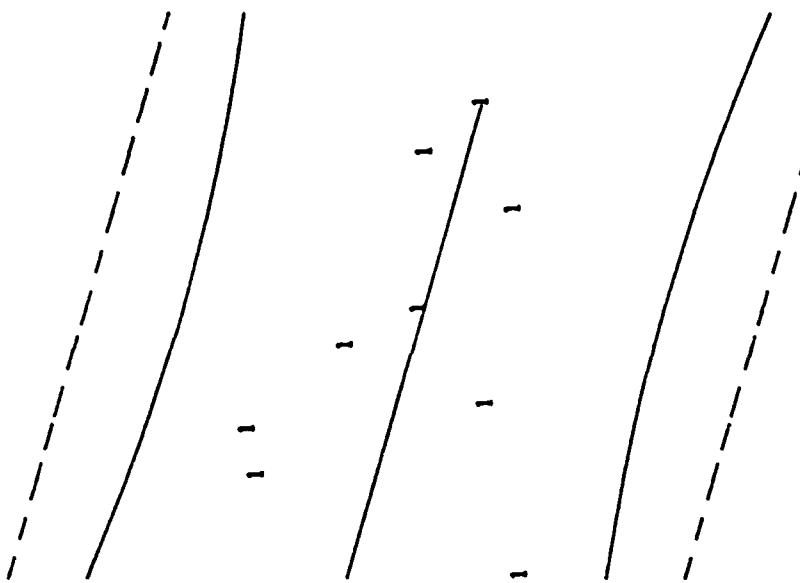
*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
1.06•0	1	+8.9999986E-04	+0.000000E+07	+8.9999986E-04	+8.9999986E-04	+1.2546330E-03
1.32•0	2	+1.5749998E-03	+7.7779895E-05	+1.6299998E-03	+1.5199999E-03	+1.2023379E-03
1.44•0	2	+1.2949998E-03	+7.7780806E-05	+1.3499998E-03	+1.2399998E-03	+1.1782017E-03
1.51•0	4	+1.0099997E-03	+1.5534918E-04	+1.2399998E-03	+8.9999986E-04	+1.1641222E-03
1.66•0	3	+1.2399998E-03	+1.0148818E-04	+1.3299998E-03	+1.1299999E-03	+1.1339520E-03
1.76•0	3	+1.0333331E-03	+9.8148814E-05	+1.0899999E-03	+9.1999978E-04	+1.1138385E-03
2.02•0	3	+9.4333314E-04	+4.5089774E-05	+9.8999985E-04	+8.9999986E-04	+1.0615431E-03
2.17•0	3	+1.0866664E-03	+1.3278991E-04	+1.2399998E-03	+1.0999997E-03	+1.0313729E-03
2.30•0	3	+1.0399997E-03	+2.0518266E-04	+1.2399998E-03	+8.2999980E-04	+1.0052253E-03

STAGE 1, DISCTED MOTOR=0012199, CREEP 10 LB LOAD, COMPLIANCE AT 20 SEC.

$\gamma = ((+2.0985691E-03) + (-2.3437214E-06) * \chi)$
 $F = +2.6681769E+00$ SIGNIFICANCE OF F = NOT SIGNIFICANT $\sigma_f = +2.5493392E-04$
 $R = -3.2888100E-01$ SIGNIFICANCE OF R = NOT SIGNIFICANT $S_r = +1.4348241E-06$
 $\iota = +1.6334555E+00$ SIGNIFICANCE OF I = NOT SIGNIFICANT $S_\iota = +2.4616313E-04$
 $N = 24$ DEGREES OF FREEDOM = 22
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = COMPLIANCE
 UNIT OF MEASURE = INCHIN/LBS
 0.07 0.11 0.15 0.19 0.23 $* 10^{-2}$
 0.00 4.00 8.00 12.00 16.00 20.00 24.00 28.00 32.00



STAGE 1. DISCTED MOTOR=0012199, CREEP 10 LB LOAD, COMPLIANCE AT 1000 SEC.

Figure 23

$F = +1.0864070E+01$ $\gamma = ((+2.1605719E-03) + (-2.7404138E-06) \equiv X)$
 $R = -3.7353193E-01$ $\sigma_f = +3.3516502E-04$
 $r = +3.2960690E+00$ $S_f = +8.3141884E-07$
 $N = 69$ $S_r = +3.1321647E-04$
 $Degrees of Freedom = 67$
 $Storage Conditions = AMB TEMP/RH$ TEST CONDITIONS = AMB TEMP/RH

PARAMETER = COMPLIANCE
 UNIT OF MEASURE = INCHIN/LBS
 0.04 0.09 0.14 0.19 0.24 *10⁻²
 0.00 4.00 8.00 12.00 16.00 20.00 24.00 28.00 32.00

DISSECTED MOTOR TP-H1011.CREEP 10 LB LOAD.COMPLIANCE AT 1000 SEC.

Figure 23A

* 444 L1 LOAD CREEP 1000 STC ANALYSIS * 44*

* 44* ANALYSIS OF 1000 STC RATES * 44*

STATION (X, Y, Z)	STRUCTURE NO. GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y		MINIMUM Y	PROGRESSION Y
				Y	Z		
1.000.0	1	+1.45939991E-03	+0.0000000E+0.0	+1.45959991E-03	+1.45999991E-03	+1.45999991E-03	+1.45999991E-03
1.000.0	2	+1.03460947E-03	+2.47404591E-04	+2.00953308E-03	+2.00953308E-03	+1.85999991E-03	+1.78919771E-03
1.000.0	3	+1.05499806E-03	+1.48525421E-04	+2.15999991E-03	+1.94999991E-03	+1.76107321E-03	+1.7446670E-03
1.000.0	4	+1.53499841E-03	+2.03513531E-04	+1.52099977E-03	+1.38900008E-03	+1.38900008E-03	+1.38900008E-03
1.000.0	5	+1.04333321E-03	+1.74736384E-04	+1.93595997E-03	+1.64999991E-03	+1.7095112E-03	+1.7095112E-03
1.000.0	6	+1.08333320E-03	+1.18044341E-05	+1.06999981E-03	+1.66999991E-03	+1.6860740E-03	+1.6860740E-03
1.000.0	7	+1.47006641E-03	+7.50523141E-05	+1.51996901E-03	+1.38999981E-03	+1.6251374E-03	+1.6251374E-03
1.000.0	8	+1.06999921E-03	+1.90938381E-04	+1.85959991E-03	+1.47999991E-03	+1.5899816E-03	+1.5899816E-03
1.000.0	9	+1.54266600E-03	+2.60200221E-04	+1.79999991E-03	+1.27999991E-03	+1.55951311E-03	+1.55951311E-03

TABLE 1.015G10 MULT=0012199, CREEP 10 L1 LOAD, CREEP LANCE AT 1000 STC.

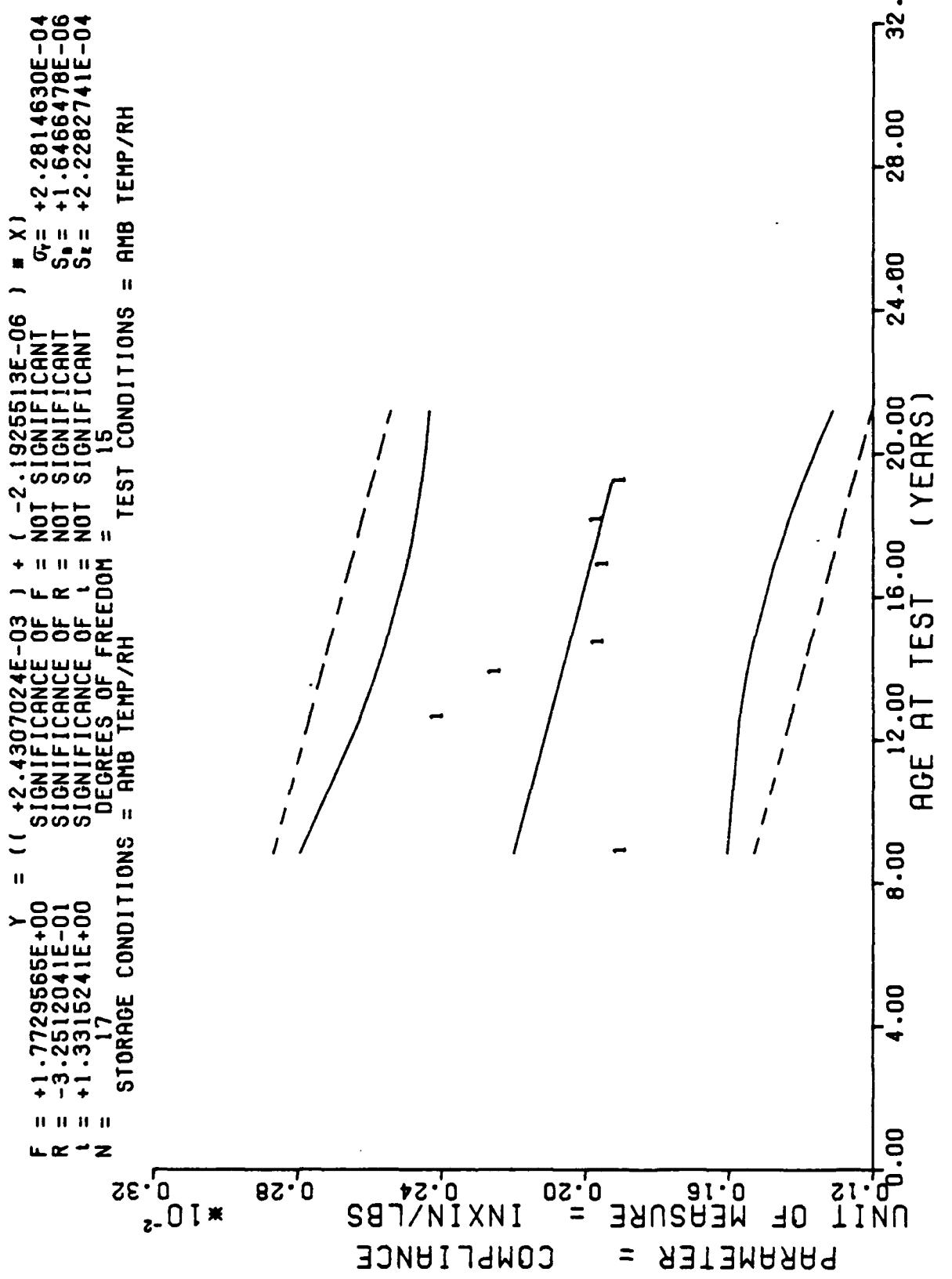
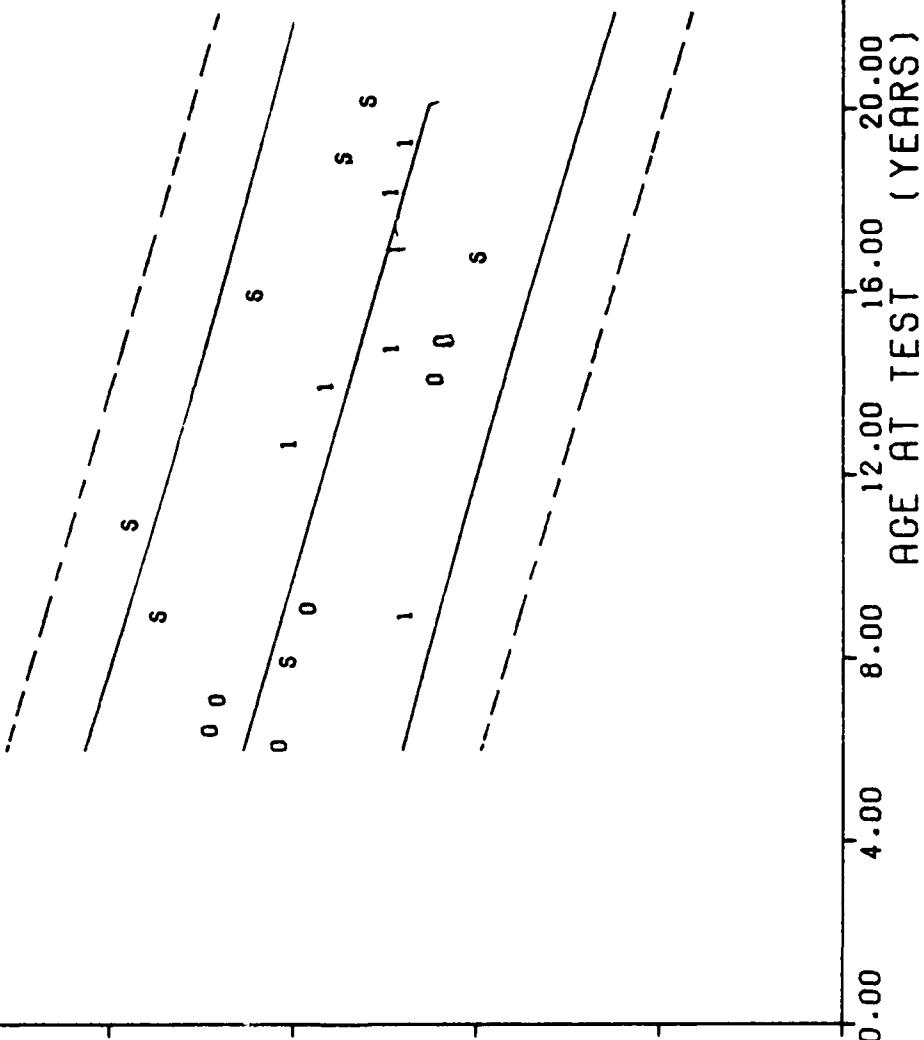


Figure 24

$Y = ((+2.9601604E-03) + (-4.7487540E-06) * X)$
 $F = +2.5562003E+01$ SIGNIFICANT OF F = SIGNIFICANT
 $R = -6.0188288E-01$ SIGNIFICANT OF R = SIGNIFICANT
 $I = +5.0558879E+00$ SIGNIFICANT OF I = SIGNIFICANT
 $N = 47$ DEGREES OF FREEDOM = 45
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = COMPLIANCE
 UNIT OF MEASURE = INXIN/LBS
 $* 10^{-2}$



DISSECTED MOTOR TP-H1011.CREEP 10 LB LOAD, COMPLIANCE AT 10.000 SEC.

Figure 24A

TABLE I. THE COMPUTED RESULTS AT 10° C.

| C₁ | C₂ | C₃ | C₄ | C₅ | C₆ | C₇ | C₈ | C₉ | C₁₀ | C₁₁ | C₁₂ | C₁₃ | C₁₄ | C₁₅ | C₁₆ | C₁₇ | C₁₈ | C₁₉ | C₂₀ | C₂₁ | C₂₂ | C₂₃ | C₂₄ | C₂₅ | C₂₆ | C₂₇ | C₂₈ | C₂₉ | C₃₀ | C₃₁ | C₃₂ | C₃₃ | C₃₄ | C₃₅ | C₃₆ | C₃₇ | C₃₈ | C₃₉ | C₄₀ | C₄₁ | C₄₂ | C₄₃ | C₄₄ | C₄₅ | C₄₆ | C₄₇ | C₄₈ | C₄₉ | C₅₀ | C₅₁ | C₅₂ | C₅₃ | C₅₄ | C₅₅ | C₅₆ | C₅₇ | C₅₈ | C₅₉ | C₆₀ | C₆₁ | C₆₂ | C₆₃ | C₆₄ | C₆₅ | C₆₆ | C₆₇ | C₆₈ | C₆₉ | C₇₀ | C₇₁ | C₇₂ | C₇₃ | C₇₄ | C₇₅ | C₇₆ | C₇₇ | C₇₈ | C₇₉ | C₈₀ | C₈₁ | C₈₂ | C₈₃ | C₈₄ | C₈₅ | C₈₆ | C₈₇ | C₈₈ | C₈₉ | C₉₀ | C₉₁ | C₉₂ | C₉₃ | C₉₄ | C₉₅ | C₉₆ | C₉₇ | C₉₈ | C₉₉ | C₁₀₀ | C₁₀₁ | C₁₀₂ | C₁₀₃ | C₁₀₄ | C₁₀₅ | C₁₀₆ | C₁₀₇ | C₁₀₈ | C₁₀₉ | C₁₁₀ | C₁₁₁ | C₁₁₂ | C₁₁₃ | C₁₁₄ | C₁₁₅ | C₁₁₆ | C₁₁₇ | C₁₁₈ | C₁₁₉ | C₁₂₀ | C₁₂₁ | C₁₂₂ | C₁₂₃ | C₁₂₄ | C₁₂₅ | C₁₂₆ | C₁₂₇ | C₁₂₈ | C₁₂₉ | C₁₃₀ | C₁₃₁ | C₁₃₂ | C₁₃₃ | C₁₃₄ | C₁₃₅ | C₁₃₆ | C₁₃₇ | C₁₃₈ | C₁₃₉ | C₁₄₀ | C₁₄₁ | C₁₄₂ | C₁₄₃ | C₁₄₄ | C₁₄₅ | C₁₄₆ | C₁₄₇ | C₁₄₈ | C₁₄₉ | C₁₅₀ | C₁₅₁ | C₁₅₂ | C₁₅₃ | C₁₅₄ | C₁₅₅ | C₁₅₆ | C₁₅₇ | C₁₅₈ | C₁₅₉ | C₁₆₀ | C₁₆₁ | C₁₆₂ | C₁₆₃ | C₁₆₄ | C₁₆₅ | C₁₆₆ | C₁₆₇ | C₁₆₈ | C₁₆₉ | C₁₇₀ | C₁₇₁ | C₁₇₂ | C₁₇₃ | C₁₇₄ | C₁₇₅ | C₁₇₆ | C₁₇₇ | C₁₇₈ | C₁₇₉ | C₁₈₀ | C₁₈₁ | C₁₈₂ | C₁₈₃ | C₁₈₄ | C₁₈₅ | C₁₈₆ | C₁₈₇ | C₁₈₈ | C₁₈₉ | C₁₉₀ | C₁₉₁ | C₁₉₂ | C₁₉₃ | C₁₉₄ | C₁₉₅ | C₁₉₆ | C₁₉₇ | C₁₉₈ | C₁₉₉ | C₂₀₀ | C₂₀₁ | C₂₀₂ | C₂₀₃ | C₂₀₄ | C₂₀₅ | C₂₀₆ | C₂₀₇ | C₂₀₈ | C₂₀₉ | C₂₁₀ | C₂₁₁ | C₂₁₂ | C₂₁₃ | C₂₁₄ | C₂₁₅ | C₂₁₆ | C₂₁₇ | C₂₁₈ | C₂₁₉ | C₂₂₀ | C₂₂₁ | C₂₂₂ | C₂₂₃ | C₂₂₄ | C₂₂₅ | C₂₂₆ | C₂₂₇ | C₂₂₈ | C₂₂₉ | C₂₃₀ | C₂₃₁ | C₂₃₂ | C₂₃₃ | C₂₃₄ | C₂₃₅ | C₂₃₆ | C₂₃₇ | C₂₃₈ | C₂₃₉ | C₂₄₀ | C₂₄₁ | C₂₄₂ | C₂₄₃ | C₂₄₄ | C₂₄₅ | C₂₄₆ | C₂₄₇ | C₂₄₈ | C₂₄₉ | C₂₅₀ | C₂₅₁ | C₂₅₂ | C₂₅₃ | C₂₅₄ | C₂₅₅ | C₂₅₆ | C₂₅₇ | C₂₅₈ | C₂₅₉ | C₂₆₀ | C₂₆₁ | C₂₆₂ | C₂₆₃ | C₂₆₄ | C₂₆₅ | C₂₆₆ | C₂₆₇ | C₂₆₈ | C₂₆₉ | C₂₇₀ | C₂₇₁ | C₂₇₂ | C₂₇₃ | C₂₇₄ | C₂₇₅ | C₂₇₆ | C₂₇₇ | C₂₇₈ | C₂₇₉ | C₂₈₀ | C₂₈₁ | C₂₈₂ | C₂₈₃ | C₂₈₄ | C₂₈₅ | C₂₈₆ | C₂₈₇ | C₂₈₈ | C₂₈₉ | C₂₉₀ | C₂₉₁ | C₂₉₂ | C₂₉₃ | C₂₉₄ | C₂₉₅ | C₂₉₆ | C₂₉₇ | C₂₉₈ | C₂₉₉ | C₃₀₀ | C₃₀₁ | C₃₀₂ | C₃₀₃ | C₃₀₄ | C₃₀₅ | C₃₀₆ | C₃₀₇ | C₃₀₈ | C₃₀₉ | C₃₁₀ | C₃₁₁ | C₃₁₂ | C₃₁₃ | C₃₁₄ | C₃₁₅ | C₃₁₆ | C₃₁₇ | C₃₁₈ | C₃₁₉ | C₃₂₀ | C₃₂₁ | C₃₂₂ | C₃₂₃ | C₃₂₄ | C₃₂₅ | C₃₂₆ | C₃₂₇ | C₃₂₈ | C₃₂₉ | C₃₃₀ | C₃₃₁ | C₃₃₂ | C₃₃₃ | C₃₃₄ | C₃₃₅ | C₃₃₆ | C₃₃₇ | C₃₃₈ | C₃₃₉ | C₃₄₀ | C₃₄₁ | C₃₄₂ | C₃₄₃ | C₃₄₄ | C₃₄₅ | C₃₄₆ | C₃₄₇ | C₃₄₈ | C₃₄₉ | C₃₅₀ | C₃₅₁ | C₃₅₂ | C₃₅₃ | C₃₅₄ | C₃₅₅ | C₃₅₆ | C₃₅₇ | C₃₅₈ | C₃₅₉ | C₃₆₀ | C₃₆₁ | C₃₆₂ | C₃₆₃ | C₃₆₄ | C₃₆₅ | C₃₆₆ | C₃₆₇ | C₃₆₈ | C₃₆₉ | C₃₇₀ | C₃₇₁ | C₃₇₂ | C₃₇₃ | C₃₇₄ | C₃₇₅ | C₃₇₆ | C₃₇₇ | C₃₇₈ | C₃₇₉ | C₃₈₀ | C₃₈₁ | C₃₈₂ | C₃₈₃ | C₃₈₄ | C₃₈₅ | C₃₈₆ | C₃₈₇ | C₃₈₈ | C₃₈₉ | C₃₉₀ | C₃₉₁ | C₃₉₂ | C₃₉₃ | C₃₉₄ | C₃₉₅ | C₃₉₆ | C₃₉₇ | C₃₉₈ | C₃₉₉ | C₄₀₀ | C₄₀₁ | C₄₀₂ | C₄₀₃ | C₄₀₄ | C₄₀₅ | C₄₀₆ | C₄₀₇ | C₄₀₈ | C₄₀₉ | C₄₁₀ | C₄₁₁ | C₄₁₂ | C₄₁₃ | C₄₁₄ | C₄₁₅ | C₄₁₆ | C₄₁₇ | C₄₁₈ | C₄₁₉ | C₄₂₀ | C₄₂₁ | C₄₂₂ | C₄₂₃ | C₄₂₄ | C₄₂₅ | C₄₂₆ | C₄₂₇ | C₄₂₈ | C₄₂₉ | C₄₃₀ | C₄₃₁ | C₄₃₂ | C₄₃₃ | C₄₃₄ | C₄₃₅ | C₄₃₆ | C₄₃₇ | C₄₃₈ | C₄₃₉ | C₄₄₀ | C₄₄₁ | C₄₄₂ | C₄₄₃ | C₄₄₄ | C₄₄₅ | C₄₄₆ | C₄₄₇ | C₄₄₈ | C₄₄₉ | C₄₅₀ | C₄₅₁ | C₄₅₂ | C₄₅₃ | C₄₅₄ | C₄₅₅ | C₄₅₆ | C₄₅₇ | C₄₅₈ | C₄₅₉ | C₄₆₀ | C₄₆₁ | C₄₆₂ | C₄₆₃ | C₄₆₄ | C₄₆₅ | C₄₆₆ | C₄₆₇ | C₄₆₈ | C₄₆₉ | C₄₇₀ | C₄₇₁ | C₄₇₂ | C₄₇₃ | C₄₇₄ | C₄₇₅ | C₄₇₆ | C₄₇₇ | C₄₇₈ | C₄₇₉ | C₄₈₀ | C₄₈₁ | C₄₈₂ | C₄₈₃ | C₄₈₄ | C₄₈₅ | C₄₈₆ | C₄₈₇ | C₄₈₈ | C₄₈₉ | C₄₉₀ | C₄₉₁ | C₄₉₂ | C₄₉₃ | C₄₉₄ | C₄₉₅ | C₄₉₆ | C₄₉₇ | C₄₉₈ | C₄₉₉ | C₅₀₀ | C₅₀₁ | C₅₀₂ | C₅₀₃ | C₅₀₄ | C₅₀₅ | C₅₀₆ | C₅₀₇ | C₅₀₈ | C₅₀₉ | C₅₁₀ | C₅₁₁ | C₅₁₂ | C₅₁₃ | C₅₁₄ | C₅₁₅ | C₅₁₆ | C₅₁₇ | C₅₁₈ | C₅₁₉ | C₅₂₀ | C₅₂₁ | C₅₂₂ | C₅₂₃ | C₅₂₄ | C₅₂₅ | C₅₂₆ | C₅₂₇ | C₅₂₈ | C₅₂₉ | C₅₃₀ | C₅₃₁ | C₅₃₂ | C₅₃₃ | C₅₃₄ | C₅₃₅ | C₅₃₆ | C₅₃₇ | C₅₃₈ | C₅₃₉ | C₅₄₀ | C₅₄₁ | C₅₄₂ | C₅₄₃ | C₅₄₄ | C₅₄₅ | C₅₄₆ | C₅₄₇ | C₅₄₈ | C₅₄₉ | C₅₅₀ | C₅₅₁ | C₅₅₂ | C₅₅₃ | C₅₅₄ | C₅₅₅ | C₅₅₆ | C₅₅₇ | C₅₅₈ | C₅₅₉ | C₅₆₀ | C₅₆₁ | C₅₆₂ | C₅₆₃ | C₅₆₄ | C₅₆₅ | C₅₆₆ | C₅₆₇ | C₅₆₈ | C₅₆₉ | C₅₇₀ | C₅₇₁ | C₅₇₂ | C₅₇₃ | C₅₇₄ | C₅₇₅ | C₅₇₆ | C₅₇₇ | C₅₇₈ | C₅₇₉ | C₅₈₀ | C₅₈₁ | C₅₈₂ | C₅₈₃ | C₅₈₄ | C₅₈₅ | C₅₈₆ | C₅₈₇ | C₅₈₈ | C₅₈₉ | C₅₉₀ | C₅₉₁ | C₅₉₂ | C₅₉₃ | C₅₉₄ | C₅₉₅ | C₅₉₆ | C₅₉₇ | C₅₉₈ | C₅₉₉ | C₆₀₀ | C₆₀₁ | C₆₀₂ | C₆₀₃ | C₆₀₄ | C₆₀₅ | C₆₀₆ | C₆₀₇ | C₆₀₈ | C₆₀₉ | C₆₁₀ | C₆₁₁ | C₆₁₂ | C₆₁₃ | C₆₁₄ | C₆₁₅ | C₆₁₆ | C₆₁₇ | C₆₁₈ | C₆₁₉ | C₆₂₀ | C₆₂₁ | C₆₂₂ | C₆₂₃ | C₆₂₄ | C₆₂₅ | C₆₂₆ | C₆₂₇ | C₆₂₈ | C₆₂₉ | C₆₃₀ | C₆₃₁ | C₆₃₂ | C₆₃₃ | C₆₃₄ | C₆₃₅ | C₆₃₆ | C₆₃₇ | C₆₃₈ | C₆₃₉ | C₆₄₀ | C₆₄₁ | C₆₄₂ | C₆₄₃ | C₆₄₄ | C₆₄₅ | C₆₄₆ | C₆₄₇ | C₆₄₈ | C₆₄₉ | C₆₅₀ | C₆₅₁ | C₆₅₂ | C₆₅₃ | C₆₅₄ | C₆₅₅ | C₆₅₆ | C₆₅₇ | C₆₅₈ | C₆₅₉ | C₆₆₀ | C₆₆₁ | C₆₆₂ | C₆₆₃ | C₆₆₄ | C₆₆₅ | C₆₆₆ | C₆₆₇ |
<th rowspan
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |

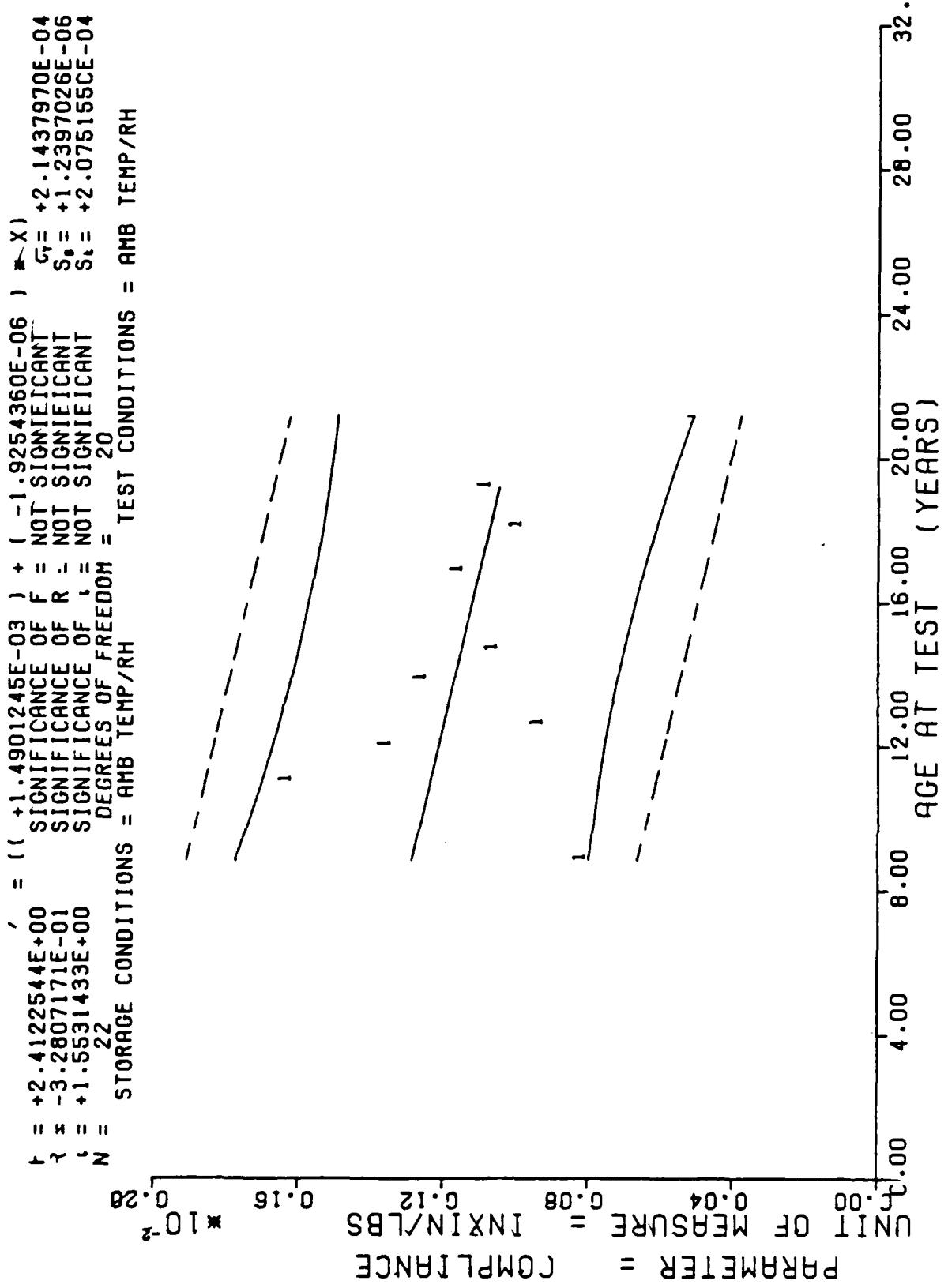
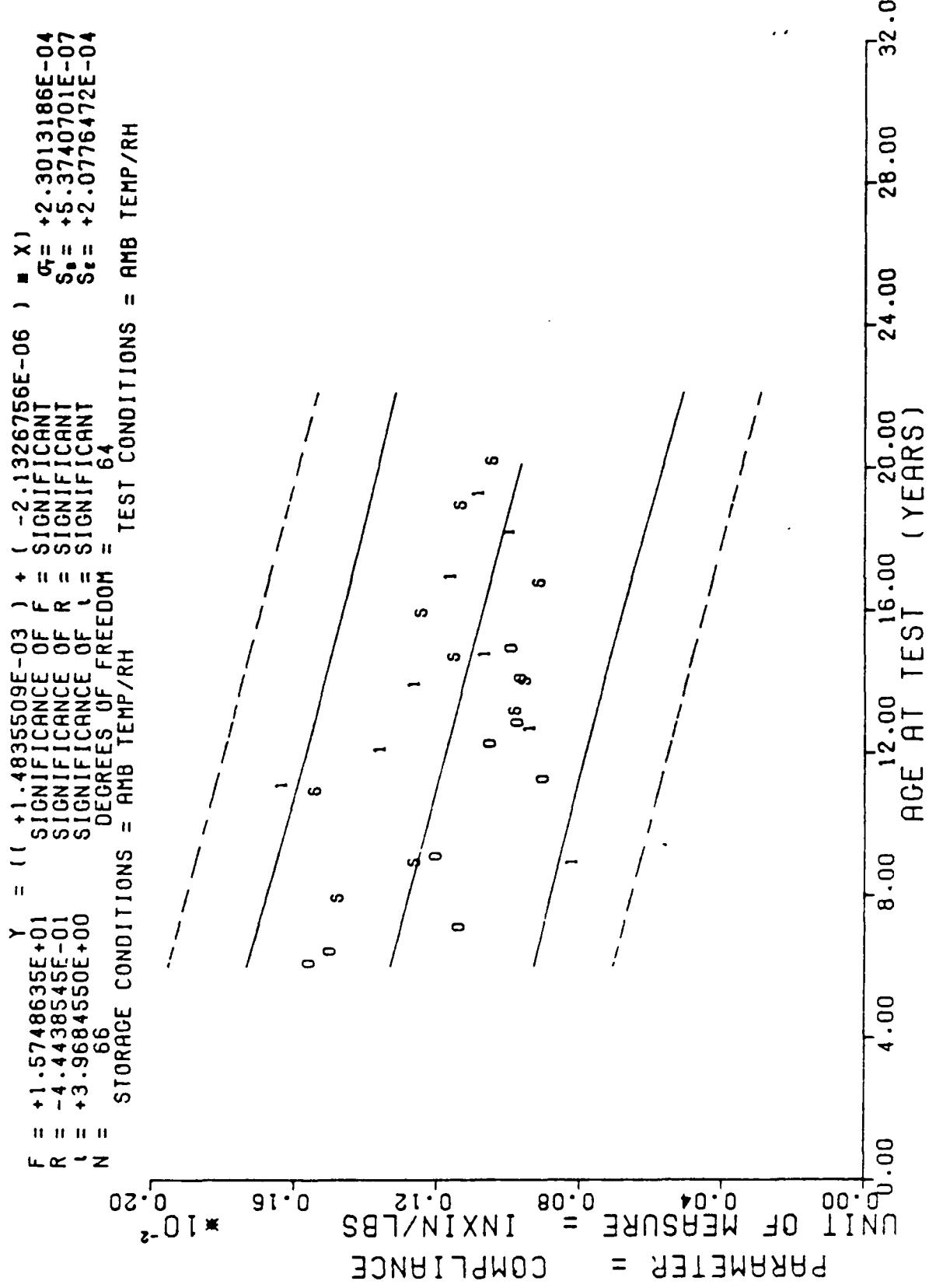


Figure 25

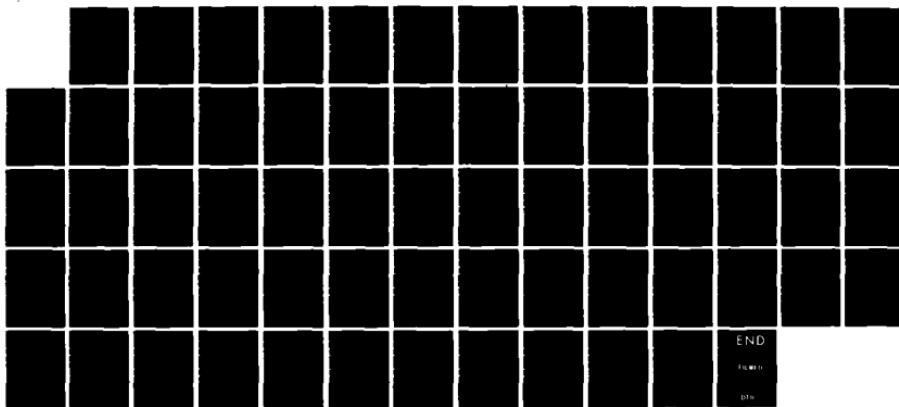


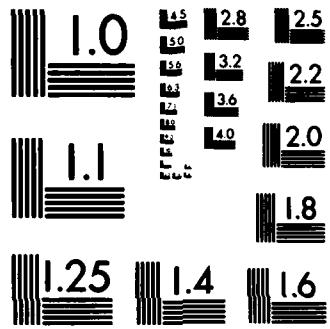
DISSECTED MOTOR TP-H1011.CREEP 12 LB LOAD, COMPLIANCE AT 10 SEC.

Figure 25A

AD-A153 206 SURVEILLANCE REPORT STAGE I DISSECTED MOTORS/
PROPELLANTS MOTOR NUMBER 00. (U) OGDEN AIR LOGISTICS
CENTER HILL AFB UT PROPELLANT ANALYSIS LA.
UNCLASSIFIED J A THOMPSON MAR 85 MANPA-503(85) 272

F/G 21/8.2 NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD		MINIMUM Y	REGRESSION Y
			DEVIATION	DEVIATION		
106.0	1	+8.0999988E-04	+0.000000E+07	+8.0999988E-04	+8.0999988E-04	+1.2860281E-03
132.0	2	+1.6249998E-03	+4.9497517E-05	+1.6599998E-03	+1.5899999E-03	+1.2359668E-03
144.0	2	+1.3499998E-03	+1.8384802E-04	+1.4799998E-03	+1.2199999E-03	+1.2128616E-03
151.0	2	+9.2999986E-04	+7.0702867E-05	+9.7999977E-04	+8.7999994E-04	+1.1993835E-03
166.0	3	+1.2533331E-03	+9.2373851E-05	+1.3599998E-03	+1.1999998E-03	+1.1705020E-03
176.0	3	+1.0566664E-03	+2.5158932E-05	+1.0799998E-03	+1.0299999E-03	+1.1512476E-03
202.0	3	+1.1533331E-03	+3.2141070E-05	+1.1899999E-03	+1.1299999E-03	+1.1011862E-03
217.0	3	+5.8999985E-04	+3.6050328E-05	+1.0199998E-03	+9.4999978E-04	+1.0723047E-03
230.0	3	+1.0766664E-03	+5.6859570E-05	+1.1399998E-03	+1.0299999E-03	+1.0472740E-03

STAGE 1. DISCTED MOTOR=0012199. CREEP 12 LB LOAD.COMPLIANCE AT 10 SEC.

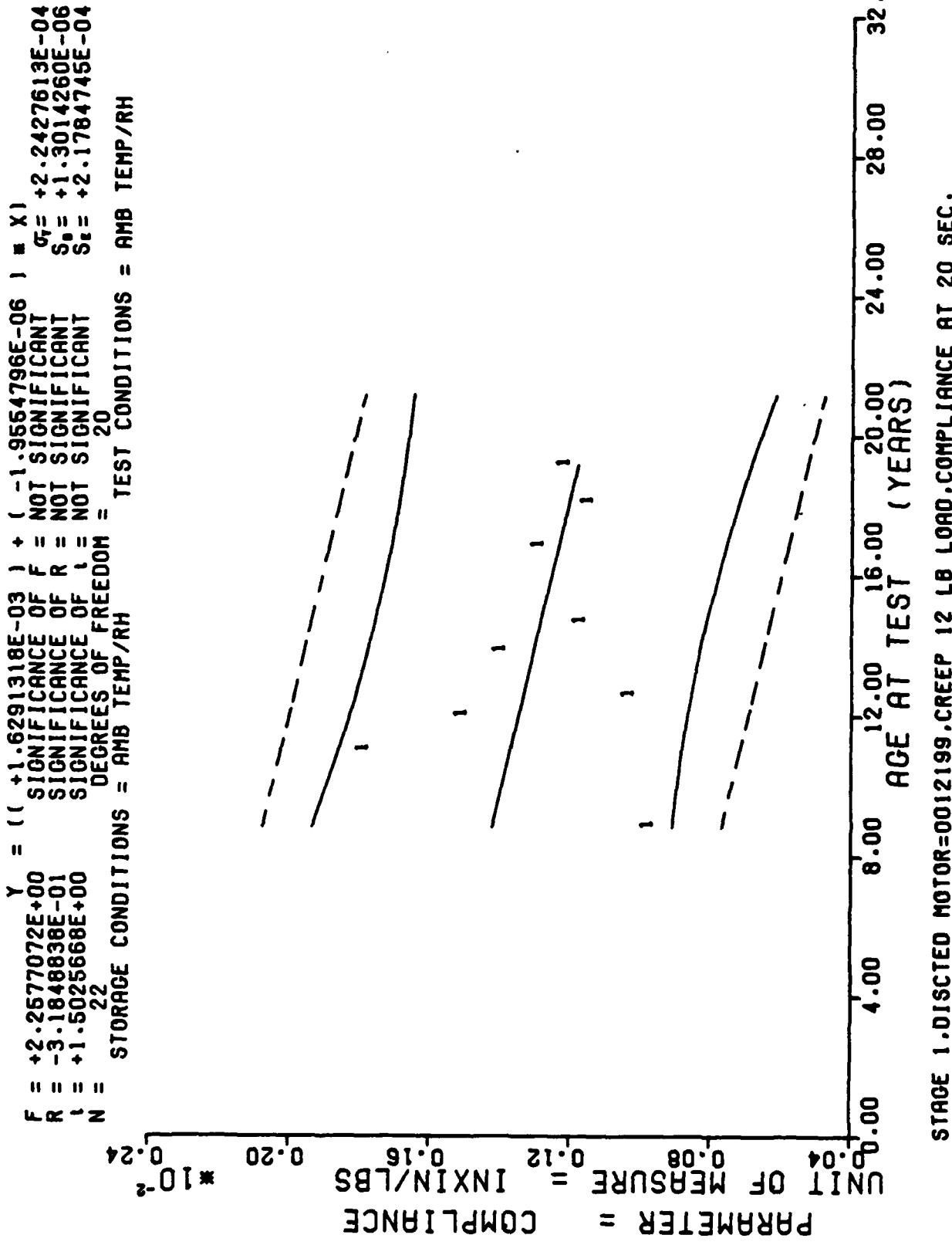
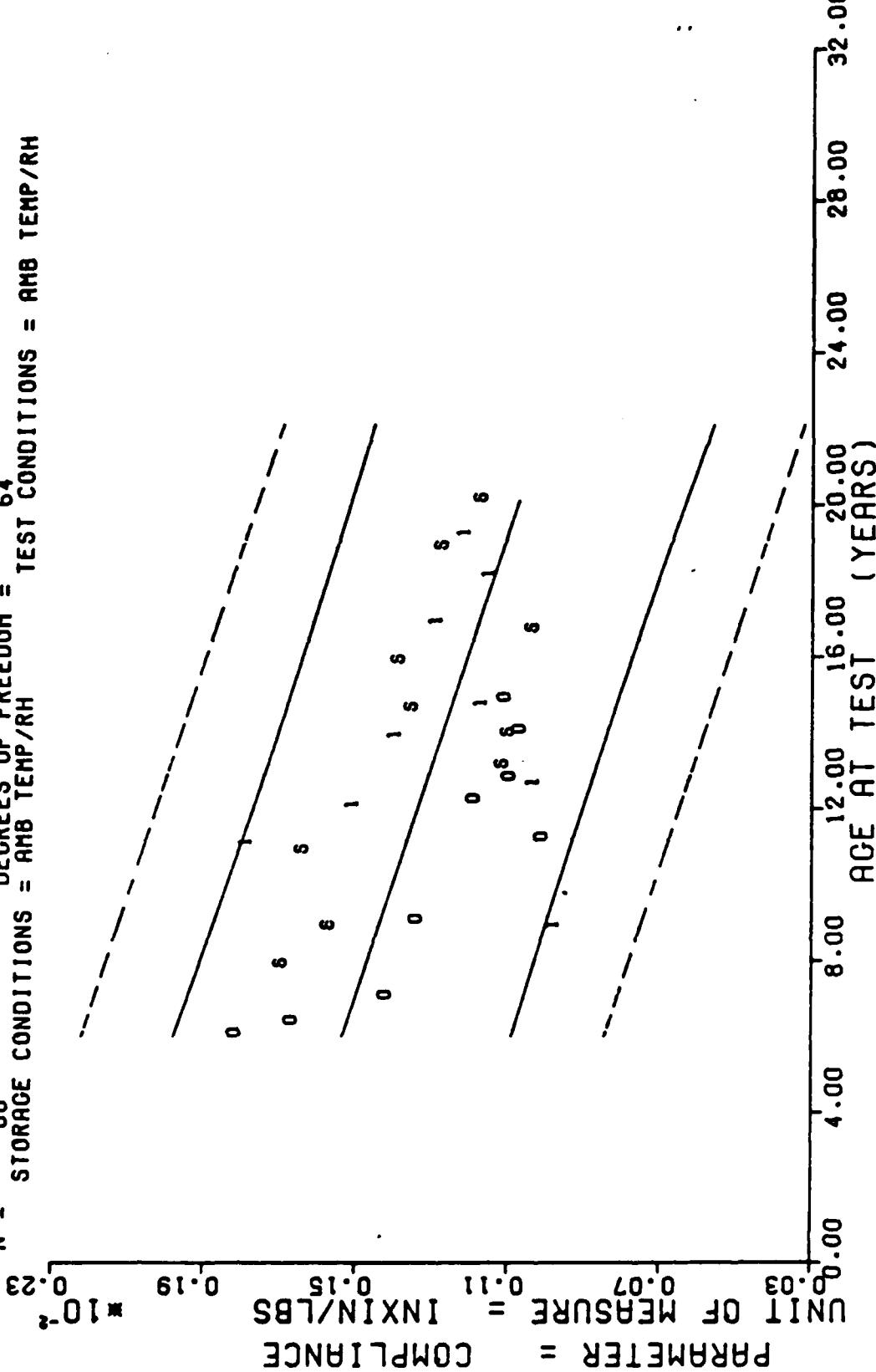


Figure 26

$F = +2.0890509E+01$
 $R = -4.9607226E-01$
 $r^2 = +4.5706137E+00$
 $N = 66$
 STORAGE CONDITIONS = AMB TEMP/RH
 $\text{DEGREES OF FREEDOM} = 64$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$
 $\gamma = ((+1.7293819E-03) + (-2.711158E-06) * X)$
 $\text{SIGNIFICANCE OF } F = \text{SIGNIFICANT}$
 $\text{SIGNIFICANCE OF } R = \text{SIGNIFICANT}$
 $\text{SIGNIFICANCE OF } r^2 = \text{SIGNIFICANT}$
 $S_0 = +2.6206855E-04$
 $S_0 = +5.9316231E-07$
 $S_0 = +2.2932006E-04$



DISSECTED MOTOR TP-H1011.CREEP 12 LB LOAD.COMPLIANCE AT 20 SEC.

Figure 26A

*** * LOAD ANALYSIS , THERMAL ANALYSIS ***

*** * ANALYSIS OF PLATE SIZES ***

Node (x,y,z)	Element Number	Mean Y	Deviation	Maximum Y	Minimum Y	PERMISSION Y
100.0	1	+9.9999993E-04	+0.0000000L+07	+9.6999993L-04	+9.6999993E-04	+1.4218500L-03
151.0	2	+1.77955999E-03	+4.2437450L-05	+1.80999993L-03	+1.74909998E-03	+1.3710083E-03
164.0	4	+1.45999997E-03	+1.9793675E-04	+1.63999999E-03	+1.45999998E-03	+1.3475427E-03
181.0	2	+1.0249998E-03	+7.7779595E-05	+1.07999998E-03	+9.09999993L-04	+1.3338543E-03
183.0	3	+1.5395989E-03	+9.3416171E-05	+1.4999997E-03	+1.32999998E-03	+1.3045221E-03
176.0	5	+1.1633331E-03	+3.0544797E-05	+1.13999999E-03	+1.12999999E-03	+1.2849674E-03
203.0	5	+1.28333351E-03	+1.5257015E-05	+1.29959981E-03	+1.2699998E-03	+1.2341248E-03
217.0	3	+1.1433332E-03	+7.0644756E-05	+1.2135536E-03	+1.0799998E-03	+1.2047926E-03
219.0	3	+1.20999929E-03	+6.2442926E-05	+1.27999999E-03	+1.15999999E-03	+1.1793714E-03

STRUCTURE, MATT=1.012137, CHPD 12 Lb. LOAD, COUPLE FORCE AT 20 SEC.

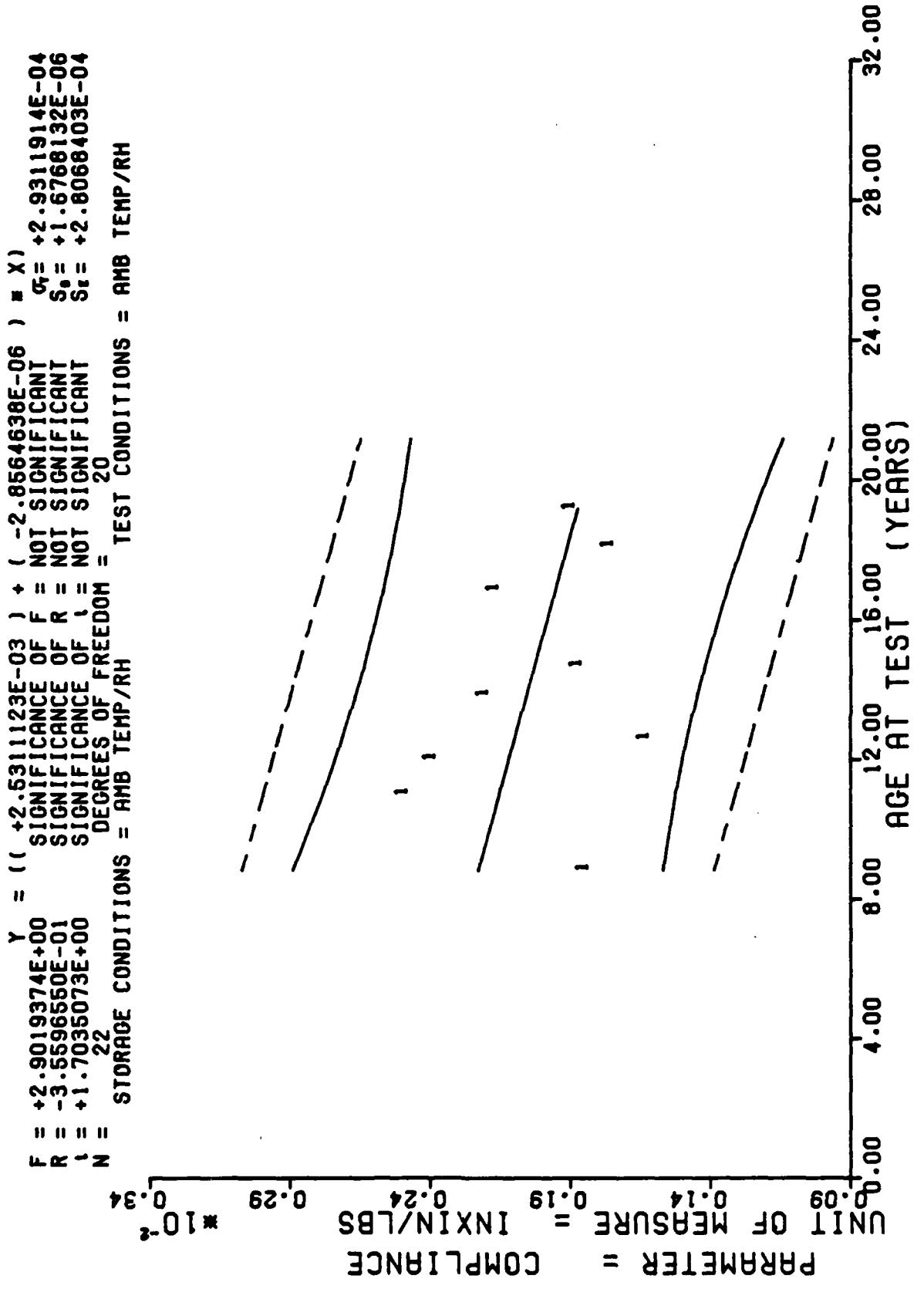


Figure 27

$F = +1.7936759E+01$
 $R = -4.6787797E-01$
 $t^1 = +4.2351812E+00$
 $N = 66$
 $Y = ((+2.9176798E-03) + (-4.7190508E-06) ■ X)$
 $F = \text{SIGNIFICANCE OF } F$
 $R = \text{SIGNIFICANCE OF } R$
 $t^1 = \text{SIGNIFICANCE OF } t^1$
 $\text{DEGREES OF FREEDOM} = 64$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

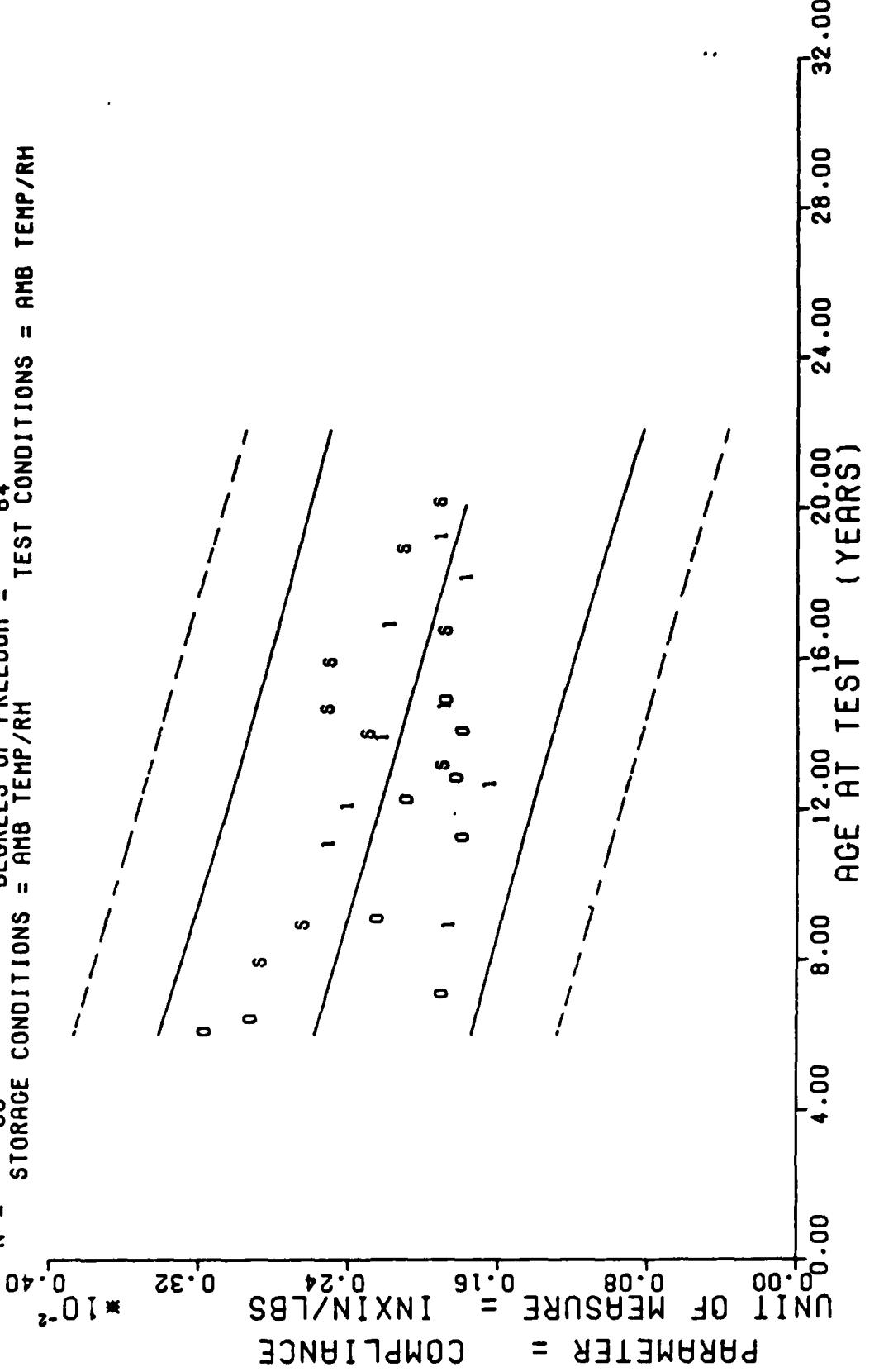


Figure 27A

**** LINEAR RELIABILITY ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

A.S. (REL.)	SPECIFICATIONS PER GROUP	STANDARD			MAXIMUM Y	MINIMUM Y	PROGRESSION Y
		MEAN Y	VARIATION	COVARIANCE			
1.00 • 0	1	+1.45999993E-03	+0.00000001E+07	+1.03395598E-03	+1.8399998E-03	+2.2283270E-03	
1.00 • 0	2	+2.4849595E-03	+2.0163550E-04	+2.05e99.99E-03	+2.2999928E-03	+2.1540500E-03	
1.00 • 0	3	+2.3649997E-03	+2.0577413E-04	+2.05795993E-03	+2.18999999E-03	+2.1197614E-03	
1.00 • 0	2	+1.02499993E-03	+1.034151832E-04	+1.01905981E-03	+1.52999997E-03	+2.0997861E-03	
1.00 • 0	3	+2.1929685E-03	+1.03955096E-04	+2.03599593E-03	+2.10999997E-03	+2.0569392E-03	
1.00 • 0	3	+1.3066659E-03	+0.0082464E-05	+1.01999999E-03	+1.76999999E-03	+2.0283746E-03	
1.00 • 0	3	+2.1035319E-03	+2.05325002E-05	+2.01399999E-03	+2.13999999E-03	+1.9541066E-03	
1.00 • 0	3	+1.07035325E-03	+5.0395783E-05	+1.07999999E-03	+1.68999998E-03	+1.9112597E-03	
1.00 • 0	3	+1.0395985E-03	+1.04935370E-04	+2.00599498E-03	+1.77999998E-03	+1.8741255E-03	

TABLE 1. DISCRETE MEDIUM=0012109, CREFL.P 12 LB LOAD, COMPLIANCE AT 1000 SEC.

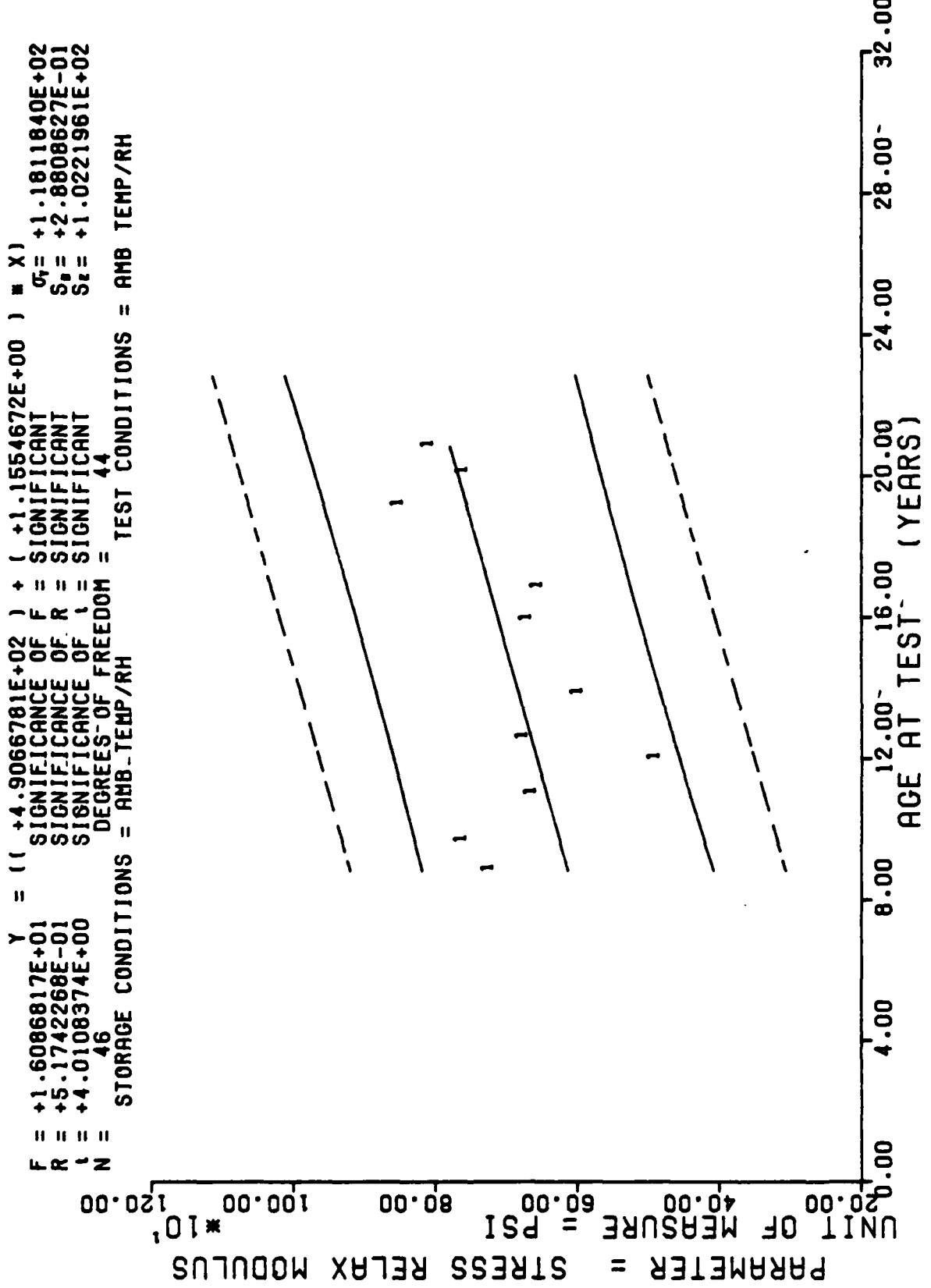
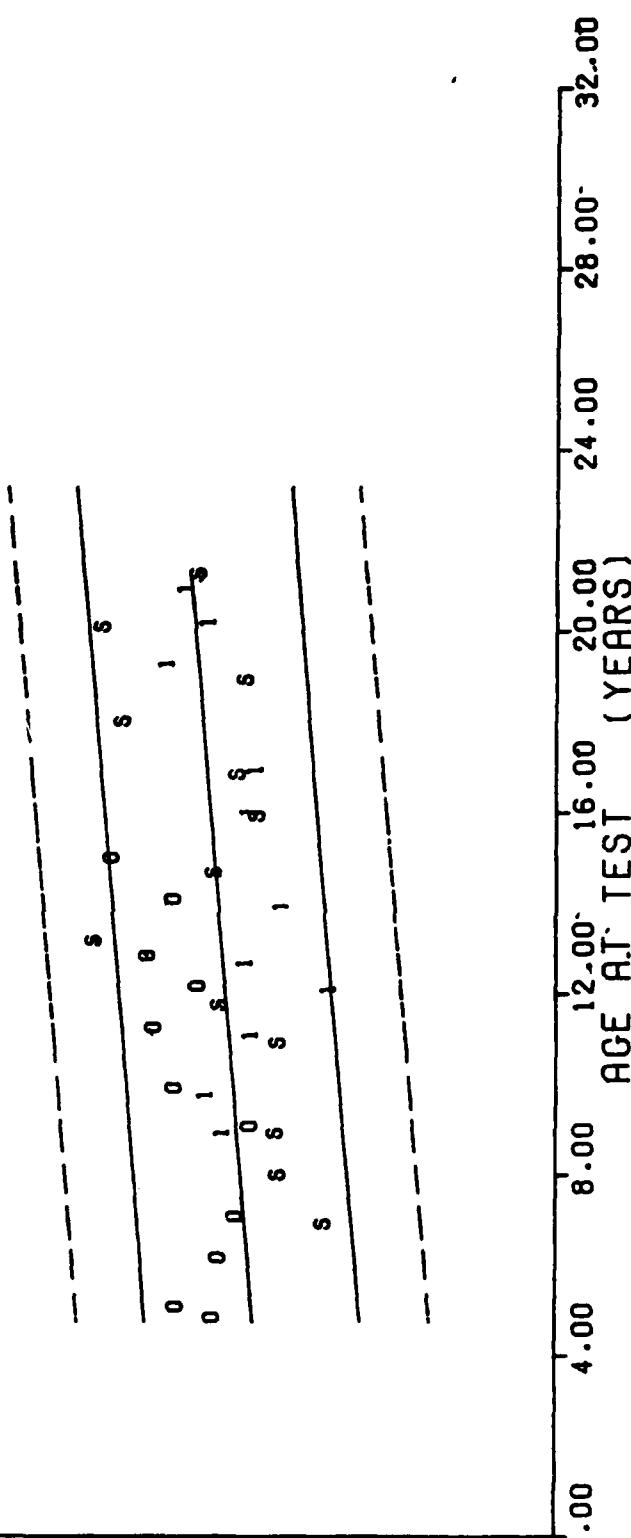


Figure 28

$E = +1.2805469E+01$
 $R = +3.1408793E-01$
 $L = +3.5784730E+00$
 $N = 119$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF L = SIGNIFICANT
 DEGREES OF FREEDOM = 117
 STORAGE CONDITIONS = AMB. TEMP/RH.

TEST CONDITIONS = AMB. TEMP/RH.

PARAMETER = STRESS RELAX MODULUS
 UNIT OF MEASURE = PSI
 0.00 40.00 80.00 120.00 * 160.00 200.00
 20.00 4.00 8.00 12.00 TEST (YEARS)



TP-H1011 DISSECTED MTRS. STRESS RELAXATION MODULUS. 3 PERCENT STRAIN. 10 SEC

Figure 28A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	3	+7.200000E+02	+5.1961524E+01	+7.500000E+02	+6.600000E+02	+6.1314721E+02
116.0	3	+7.5866650E+02	+1.5044378E+01	+7.7300000E+02	+7.4300000E+02	+6.2470190E+02
132.0	3	+6.6000000E+02	+1.6999999E+01	+6.7700000E+02	+6.4300000E+02	+6.4318945E+02
144.0	4	+4.8650000E+02	+3.7278233E+01	+5.2000000E+02	+4.4000000E+02	+6.5705493E+02
151.0	3	+6.7233325E+02	+3.2331615E+01	+7.0700000E+02	+6.4300000E+02	+6.6514331E+02
166.0	3	+5.9433325E+02	+3.5571524E+01	+6.3300000E+02	+5.6300000E+02	+6.8247534E+02
161.0	3	+6.6700000E+02	+2.6457513E+01	+6.9700000E+02	+6.4700000E+02	+7.1136206E+02
202.0	3	+6.5100000E+02	+7.2111025E+00	+6.5700000E+02	+6.4300000E+02	+7.2407202E+02
230.0	3	+8.4766650E+02	+1.2858201E+01	+8.5700000E+02	+8.3300000E+02	+7.5642504E+02
241.0	6	+7.5666650E+02	+8.0955955E+01	+8.7300000E+02	+6.4300000E+02	+7.6913525E+02
250.0	12	+8.0500000E+02	+1.0683632E+02	+9.9000000E+02	+6.8300000E+02	+7.7953442E+02

STAGE 1,DISC1D MOTOR=0012199,STRESS RELAXATION MODULUS,3 X STRAIN AT 10 SEC.

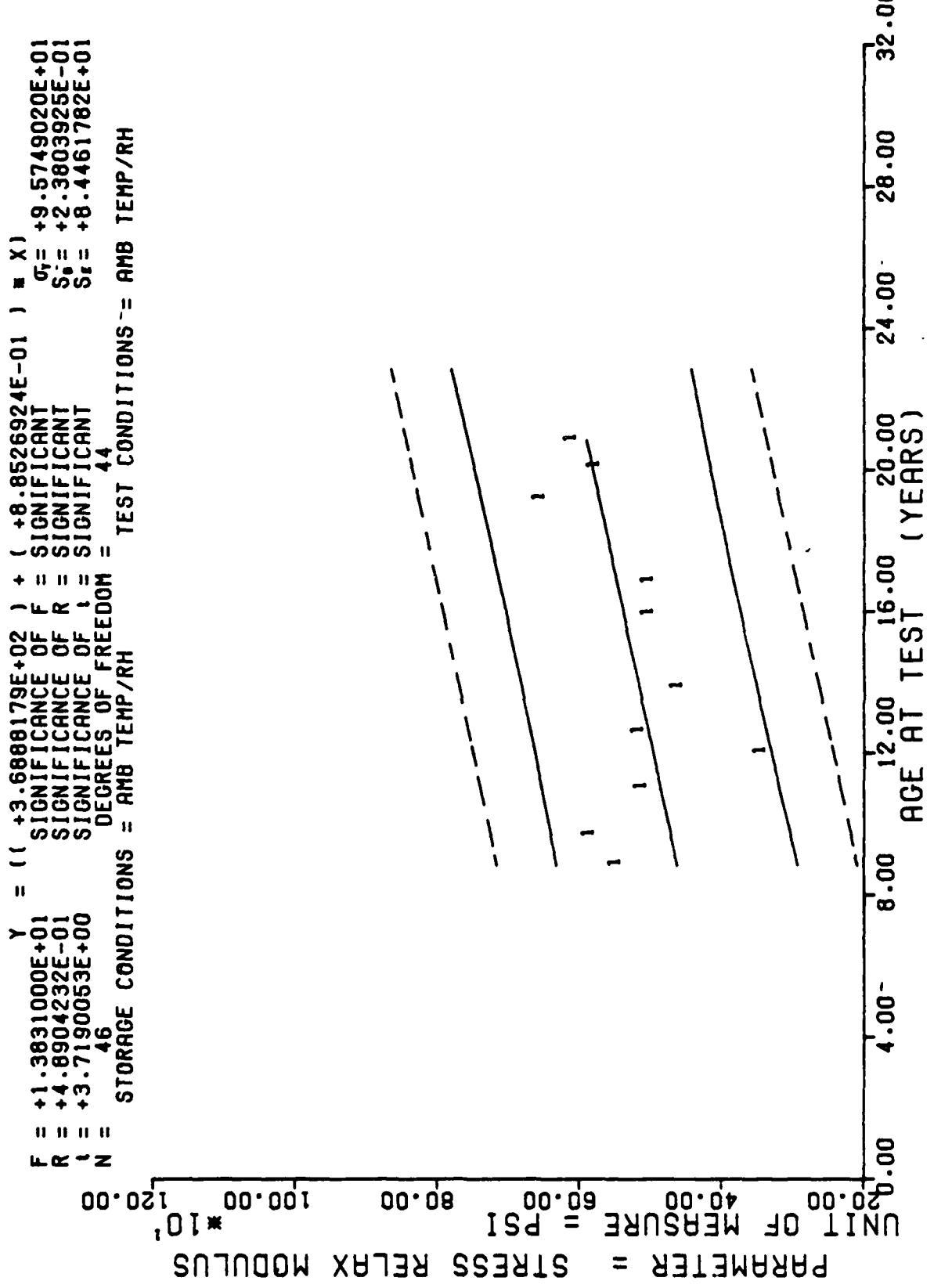
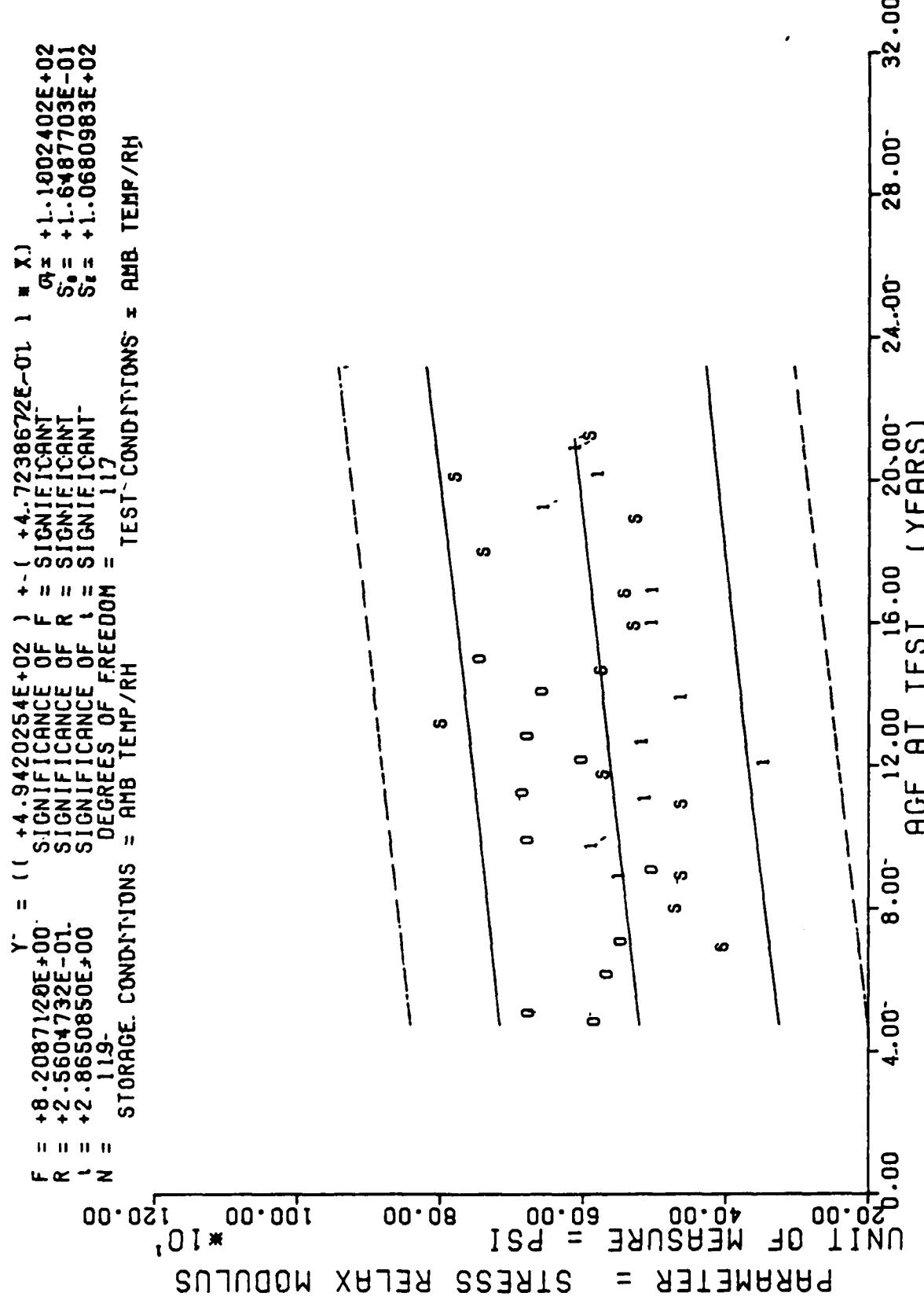


Figure 29

$F = +8.2087120E+00$ $Y = ((+4.9420254E+02) + (-4.7238672E-01) 1 \times X_1)$
 $R = +2.5604732E-01$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = +2.8650850E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $t = +2.8650850E+00$ SIGNIFICANCE OF t = SIGNIFICANT
 $N = 119-$ DEGREES OF FREEDOM = 117
 $N =$ STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



TP-H1011 DISSECTED-MTRS. STRESS RELAXATION MODULUS, 3 PERCENT STRAIN, 50-SEC

*** LINEAR REGRESSION ANALYSIS ***

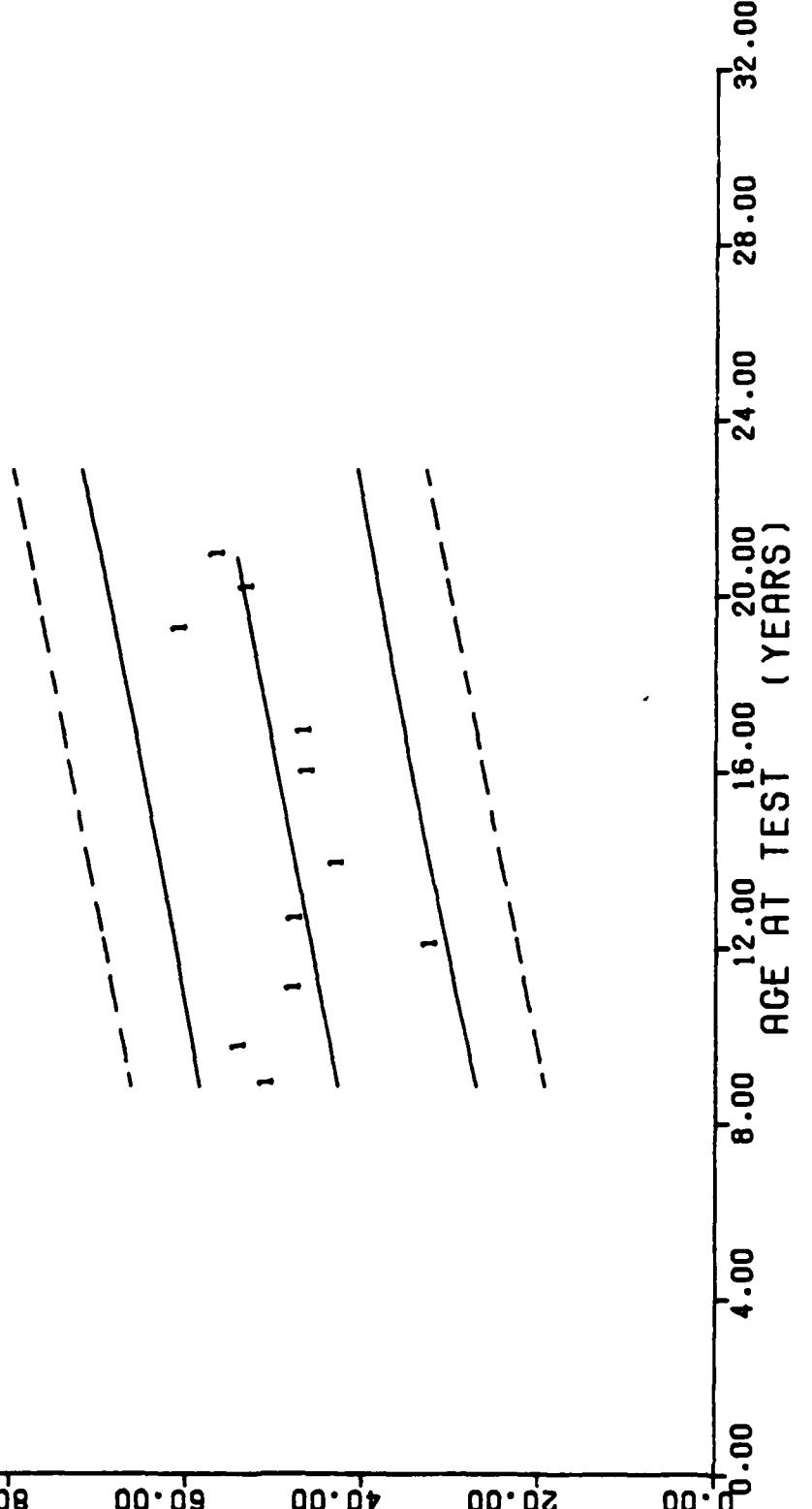
*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	3	+5.440000E+02	+3.8105117E+01	+5.6000000E+02	+5.0000000E+02	+4.6272021E+02
116.0	3	+5.8200000E+02	+2.0074859E+01	+6.0300000E+02	+5.6300000E+02	+4.7157299E+02
132.0	3	+5.0766650E+02	+1.5011106E+01	+5.2300000E+02	+4.9300000E+02	+4.8573730E+02
144.0	4	+3.4100000E+02	+1.8018509E+01	+3.6000000E+02	+3.1700000E+02	+4.9636035E+02
151.0	3	+5.1233325E+02	+2.6576932E+01	+5.4000000E+02	+4.8700000E+02	+5.0255737E+02
166.0	3	+4.5766650E+02	+2.7300793E+01	+4.8700000E+02	+4.3300000E+02	+5.1583642E+02
191.0	3	+4.9900000E+02	+2.0297783E+01	+5.1700000E+02	+4.7700000E+02	+5.3796801E+02
202.0	3	+4.9866650E+02	+5.1316014E+00	+5.0300000E+02	+4.9300000E+02	+5.4770605E+02
230.0	3	+6.5100000E+02	+1.8243287E+01	+6.6300000E+02	+6.3000000E+02	+5.7249365E+02
241.0	6	+5.7500000E+02	+7.0350550E+01	+6.7000000E+02	+4.8000000E+02	+5.8223144E+02
250.0	12	+6.0666650E+02	+8.5760059E+01	+7.6000000E+02	+5.0000000E+02	+5.9019897E+02

STAGE 1, DISCTED MOTDR=0012199, STRESS RELAXATION MODULUS.3 % STRAIN AT 50 SEC.

$F = +1.3282933E+01$
 $R = +4.8154222E-01$
 $L = +3.6445759E+00$
 $N = 46$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF L = SIGNIFICANT
 DEGREES OF FREEDOM = 44
 STORAGE CONDITIONS = AMB TEMP/RH

PARAMETER = STRESS RELAX MODULUS
 UNIT OF MEASURE = PSI
 0.00 20.00 40.00 60.00 80.00 *10
 100.00



STAGE 1.DISCETED MOTOR=0012199,STRESS RELAXATION MODULUS.3 % STRAIN AT 100 SEC.

Figure 30

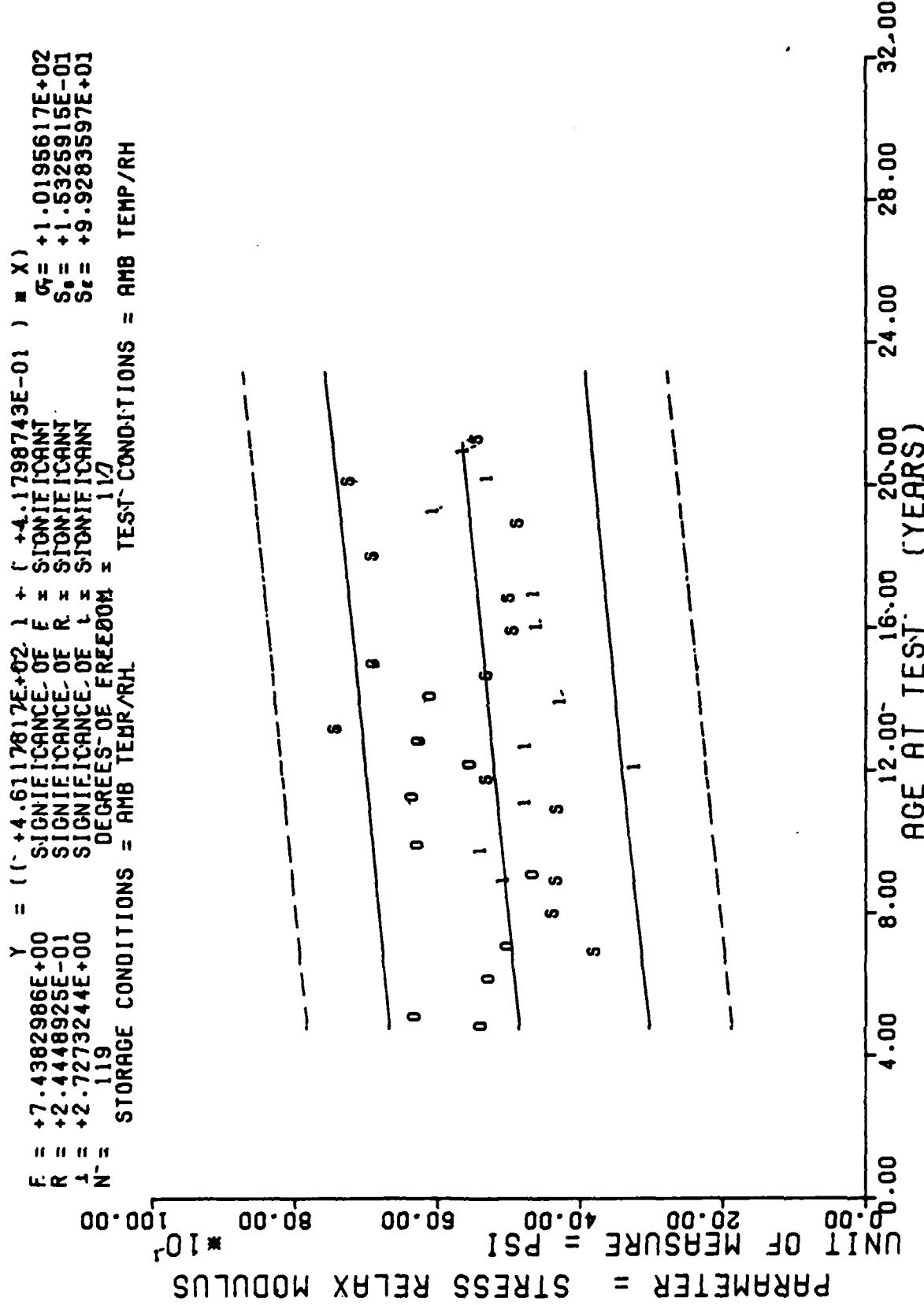


Figure 30A

*** LINEAR REGRESSION ANALYSIS ***

*** ANALYSIS OF TIME SERIES ***

AGE (MILLNS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
1.00•.0	3	+5.030000E+02	+3.4641016E+01	+5.230000E+02	+4.630000E+02	+4.2819140E+02
1.10•.0	3	+5.350000E+02	+2.0074859E+01	+5.560000E+02	+5.160000E+02	+4.3622070E+02
1.32•.0	3	+4.7233325E+02	+1.3650396E+01	+4.870000E+02	+4.600000E+02	+4.4906738E+02
1.44•.0	4	+3.1825000E+02	+2.0451161E+01	+3.430000E+02	+2.930000E+02	+4.5870263E+02
1.51•.0	3	+4.7133325E+02	+2.5026652E+01	+4.970000E+02	+4.470000E+02	+4.6432299E+02
1.60•.0	3	+4.2333325E+02	+2.5166114E+01	+4.500000E+02	+4.000000E+02	+4.7636694E+02
1.91•.0	3	+4.5666650E+02	+1.8230011E+01	+4.730000E+02	+4.370000E+02	+4.9644018E+02
2.02•.0	3	+4.6133325E+02	+5.1316014E+00	+4.670000E+02	+4.570000E+02	+5.0527246E+02
2.30•.0	3	+6.0233325E+02	+1.7473789E+01	+6.170000E+02	+5.830000E+02	+5.2775439E+02
2.41•.0	6	+5.2666650E+02	+6.5071243E+01	+6.130000E+02	+4.370000E+02	+5.3658666E+02
2.50•.0	12	+5.6016650E+02	+8.1358726E+01	+6.970000E+02	+4.430000E+02	+5.4381298E+02

STAGE 1. DISCTED MOTOR=0012199. STRESS RELAXATION MODULUS.3 X STRAIN AT 100 SEC.

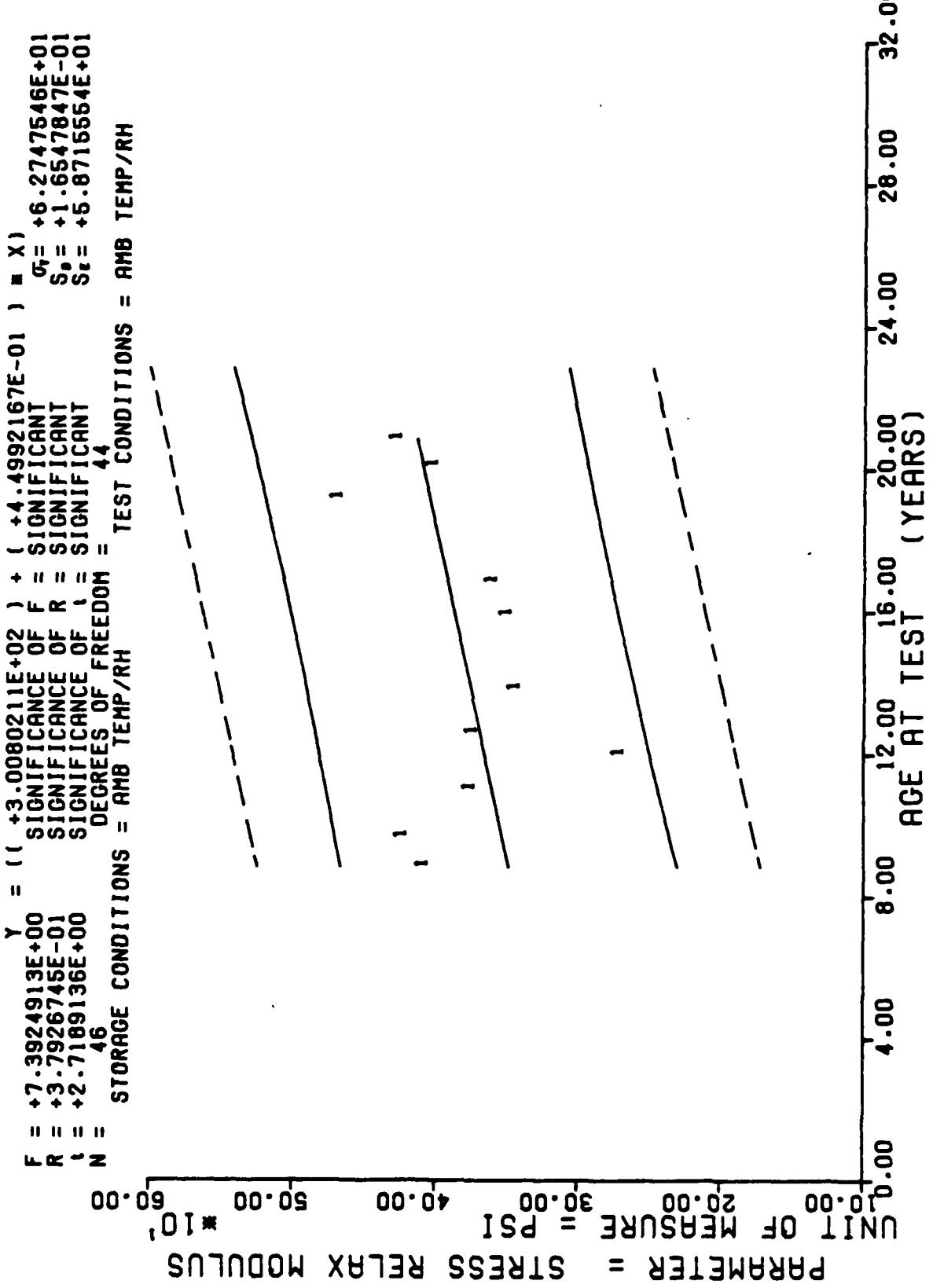


Figure 31

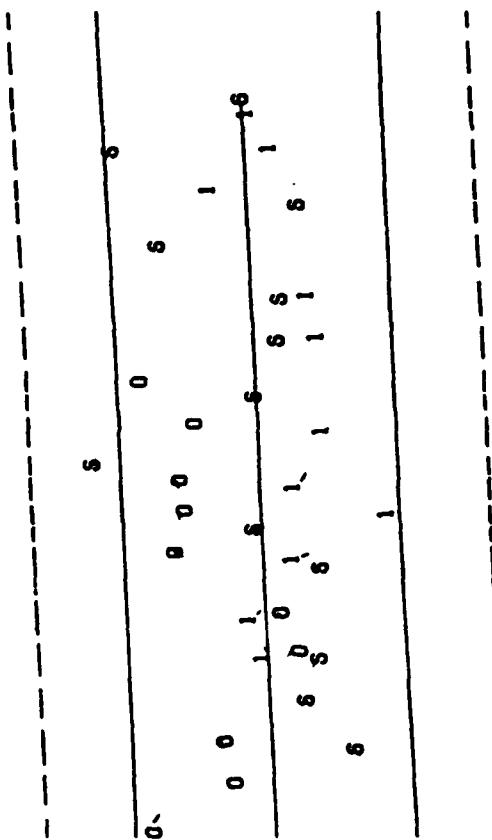
$F = +2.4487372E+00$
 $R = +1.4501191E-01$
 $t = +1.5648441E+00$
 $N = 116$
 STORAGE CONDITIONS = AMB. TEMP/RH

$\gamma = ((+3.8240604E+02) + (+2.1255564E-01) \cdot X) / (+8.4776366E+01)$
 SIGNIFICANCE OF F = NOT SIGNIFICANT
 SIGNIFICANCE OF R = NOT SIGNIFICANT
 SIGNIFICANCE OF t = NOT SIGNIFICANT
 DEGREES OF FREEDOM = 114

TEST CONDITIONS = AMB. TEMP/RH

UNIT OF MEASURE = PSI
 PARAMETER = STRESS RELAX MODULUS

Age at Test (Years)	Stress Relax Modulus
0.00	100.00
4.00	80.00
8.00	12.00
12.00	16.00
16.00	20.00
20.00	24.00
24.00	28.00
28.00	32.00



TP-H1011 DISSECTED-MTRS, STRESS-RELAXATION MODULUS, 3 PERCENT STRAIN, 1000 SEC

Figure 31A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	3	+4.060000E+02	+3.464101E+01	+4.260000E+02	+3.660000E+02	+3.4849365E+02
116.0	3	+4.2066650E+02	+1.361371E+01	+4.360000E+02	+4.100000E+02	+3.5299291E+02
132.0	3	+3.73333325E+02	+1.2342339E+01	+3.8700000E+02	+3.6300000E+02	+3.6019165E+02
144.0	4	+2.6500000E+02	+2.3888630E+01	+3.0300000E+02	+2.470000E+02	+3.6559082E+02
151.0	3	+3.7200000E+02	+1.8520259E+01	+3.9000000E+02	+3.5300000E+02	+3.6874023F+02
166.0	3	+3.42333325E+02	+1.6623276E+01	+3.6000000E+02	+3.2700000E+02	+3.7548901E+02
191.0	3	+3.4800000E+02	+1.1532562E+01	+3.6000000E+02	+3.3700000E+02	+3.8673706E+02
202.0	3	+3.5866650E+02	+5.1316014E+00	+3.6300000E+02	+3.5300000E+02	+3.9168627E+02
230.0	3	+4.6666650E+02	+2.0550750E+01	+4.800000E+02	+4.4300000E+02	+4.0428393E+02
241.0	6	+4.0016650E+02	+4.3462244E+01	+4.5300000E+02	+3.3700000F+02	+4.0923315E+02
250.0	12	+4.2525000E+02	+6.6449057E+01	+5.5300000E+02	+3.3700000E+02	+4.1328247E+02

STAGE 1. DISCTED MOTUR=0012199. STRESS RELAXATION MODULUS.3 X STRAIN AT 1000 SEC.

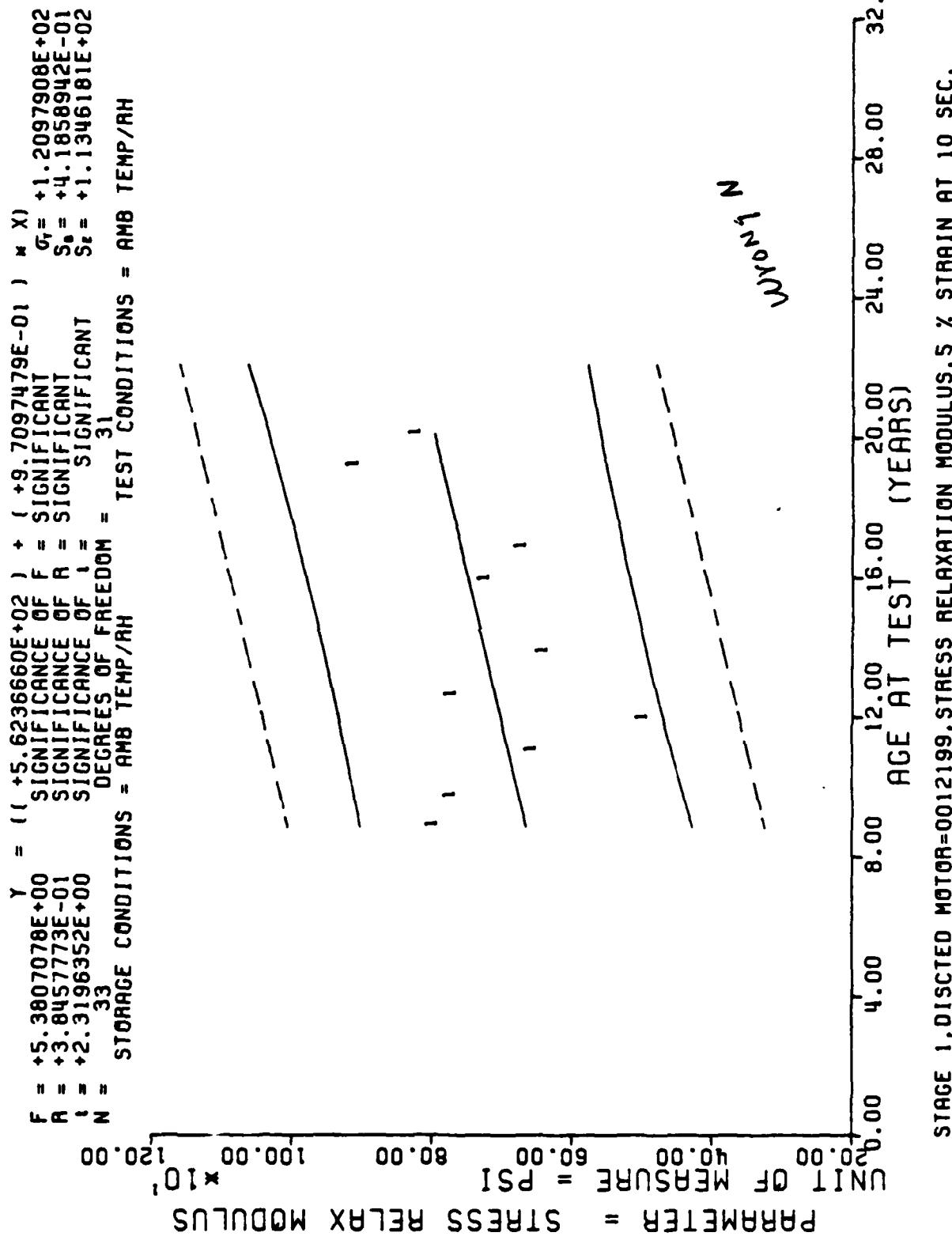


Figure 32

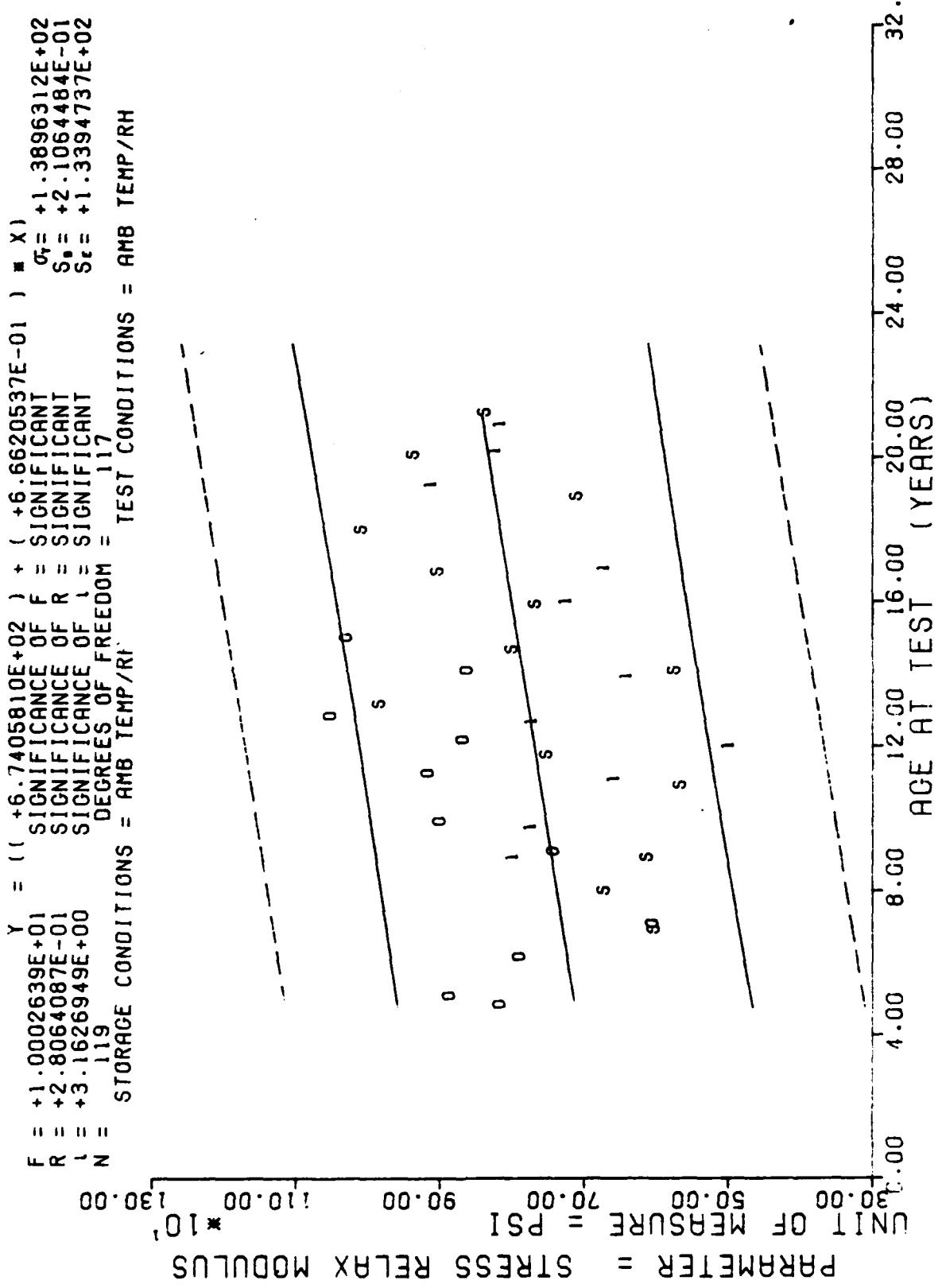


Figure 32A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
1.00• 0	3	+7.9400000E+02	+9.4636145E+01	+9.0000000E+02	+7.1800000E+02	+6.6384643E+02
116• 0	3	+7.6866650E+02	+6.4291005E+00	+7.7600000E+02	+7.6400000E+02	+6.7392626E+02
132• 0	3	+6.5333325E+02	+5.5473717E+01	+7.0000000E+02	+5.9200000E+02	+6.9005444E+02
143• 0	3	+4.9466650E+02	+3.4312291E+01	+5.2600000E+02	+4.5800000E+02	+7.0114233E+02
151• 0	3	+7.6800000E+02	+9.9999999E+00	+7.7800000E+02	+7.5800000E+02	+7.0920654E+02
166• 0	3	+6.3666650E+02	+4.5003703E+01	+6.7200000E+02	+5.8600000E+02	+7.2432641E+02
191• 0	3	+7.2000000E+02	+1.2489995E+01	+7.3000000E+02	+7.0600000E+02	+7.4952661E+02
202• 0	3	+6.6800000E+02	+1.3114877E+01	+6.8200000E+02	+6.5600000E+02	+7.6061450E+02
230• 0	3	+9.0733325E+02	+3.8279672E+01	+9.5000000E+02	+8.7600000E+02	+7.8883862E+02
241• 0	6	+8.1933325E+02	+9.9032654E+01	+9.7800000E+02	+7.1000000E+02	+7.9992675E+02
250• 0	10	+8.1259985E+02	+8.2430037E+01	+9.7200000E+02	+6.9200000E+02	+8.0899877E+02

STAGE 1, DISCTED MOTOR=0012199, STRESS RELAXATION MODULUS,5 X STRAIN AT 10 SEC.

$\gamma = (1 + 4.0045843E+02) + (1 + 6.9786691E-01) \cdot X$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF L = SIGNIFICANT
 DEGREES OF FREEDOM = 41
 N = 43
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = STRESS RELAX MODULUS
 INIT OF MEASURE = PSI
 20.00 40.00 60.00 80.00 100.00 *10
 120.00

STAGE 1, DISCTED MOTOR=0012199, STRESS RELAXATION MODULUS, S : STRAIN AT 50 SEC.

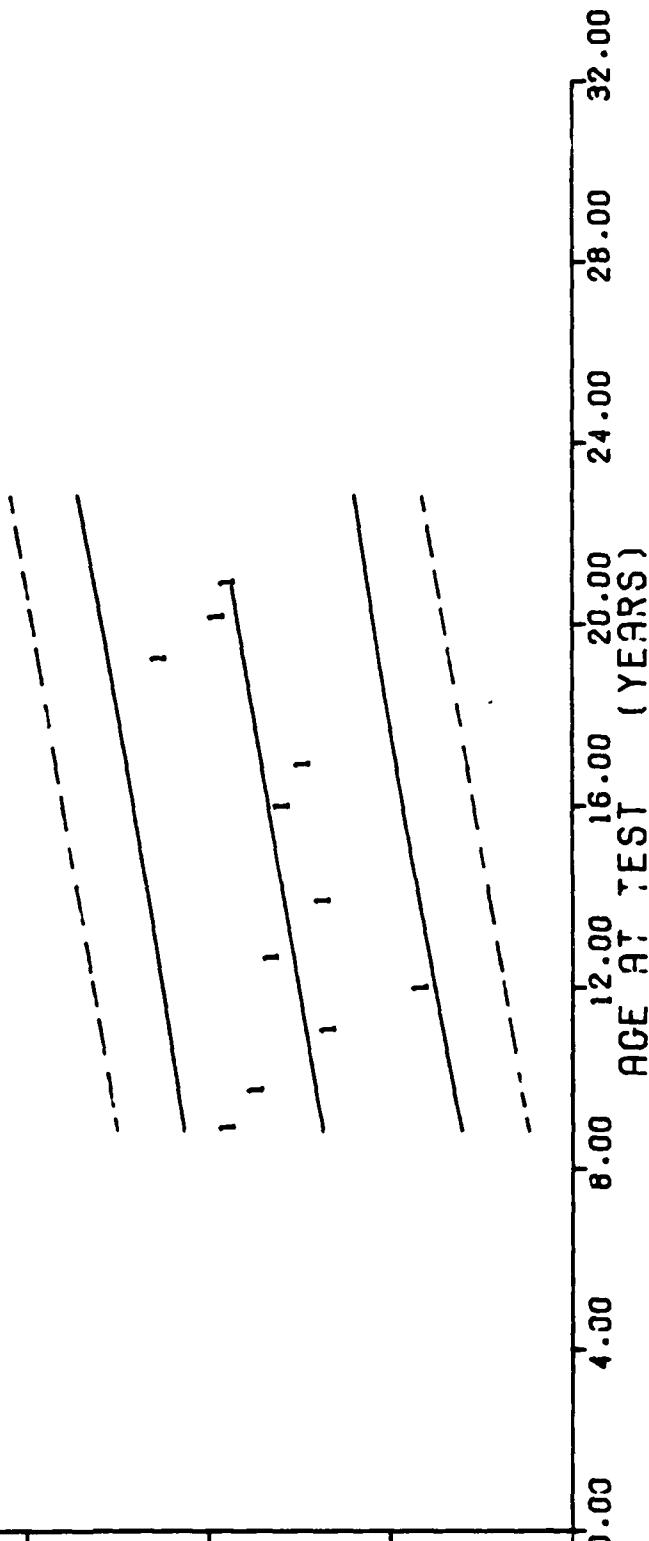
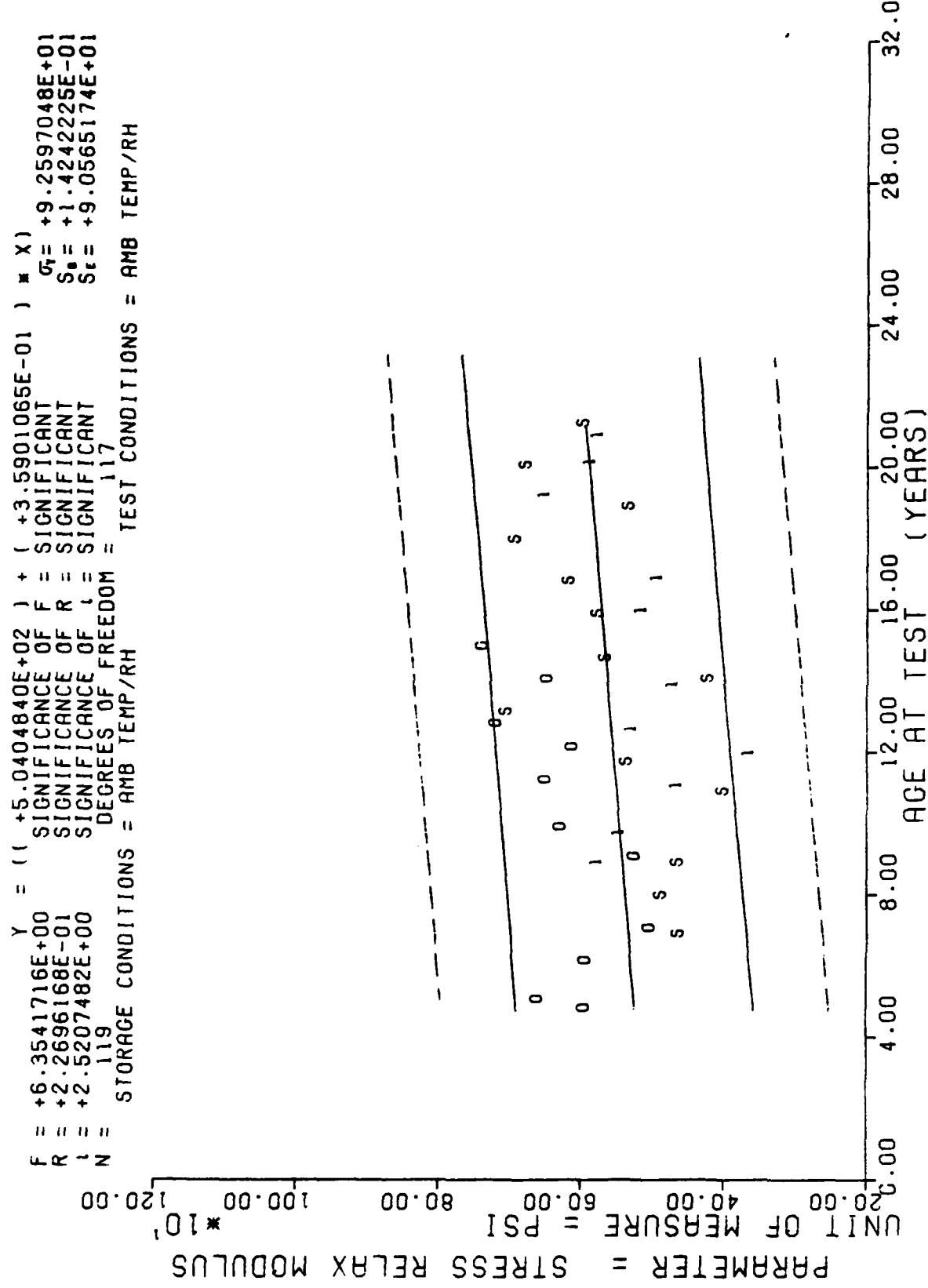


Figure 33



TP-H1011 DISSECTED MTRS. STRESS RELAXATION MODULUS. 5 PERCENT STRAIN, 50 SEC

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	3	+5.7333325E+02	+6.7121779E+01	+6.4800000E+02	+5.1800000E+02	+4.7443212E+02
116.0	3	+5.4200000E+02	+1.2489995E+01	+5.5600000E+02	+5.3200000E+02	+4.8141088E+02
132.0	3	+4.6200000E+02	+4.1327956E+01	+4.9600000E+02	+4.1600000E+02	+4.9257666E+02
143.0	3	+3.6066650E+02	+2.3180451E+01	+3.8200000E+02	+3.3600000E+02	+5.0025317E+02
151.0	3	+5.2533325E+02	+8.0829037E+00	+5.3400000E+02	+5.1800000E+02	+5.0583618E+02
166.0	3	+4.6800000E+02	+2.6457513E+01	+4.8800000E+02	+4.3800000E+02	+5.1630419E+02
191.0	3	+5.1266650E+02	+5.7735026E+00	+5.1600000E+02	+5.0600000E+02	+5.3375097E+02
202.0	3	+4.9000000E+02	+5.9999999E+00	+4.9600000E+02	+4.8400000E+02	+5.4142749E+02
230.0	3	+6.4800000E+02	+1.4422205E+01	+6.6400000E+02	+6.3600000E+02	+5.6096777E+02
241.0	6	+5.8433325E+02	+8.9901427E+01	+7.3200000E+02	+4.9000000E+02	+5.6864428E+02
250.0	10	+5.7300000E+02	+6.1255385E+01	+6.8600000E+02	+4.9000000E+02	+5.7492504E+02

STAGE 1. DISCTED MOTOR=0012199. STRESS RELAXATION MODULUS,5 X STRAIN AT 50 SEC.

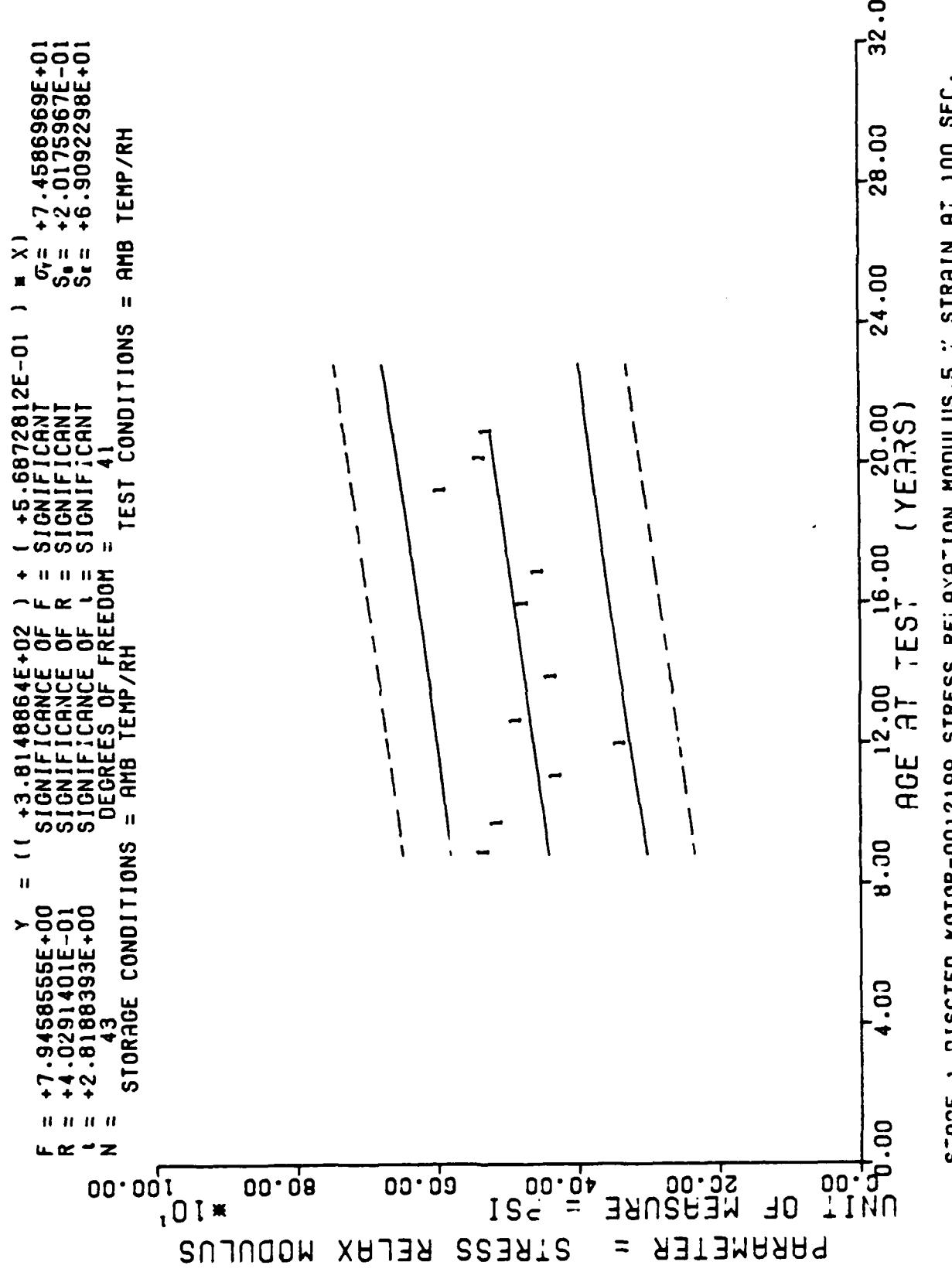
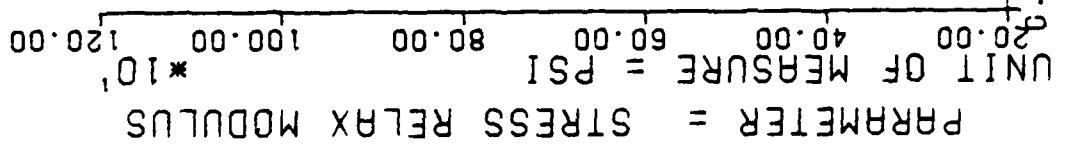


Figure 34

$F = +4.6442171E+00$
 $R = +1.9539368E-01$
 $I = +2.1550445E+00$
 $N = 119$
 Y = $((+4.7323451E+02) + (+2.8278445E-01) * X)$
 F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF I = SIGNIFICANT
 DEGREES OF FREEDOM = 117
 STORAGE CONDITIONS = AMB TEMP/RH



TP-H1011 DISSECTED MIRS, STRESS RELAXATION MODULUS, 5 PERCENT STRAIN, 100 SEC

Figure 4A

***** LINEAR REGRESSION ANALYSIS *****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	3	+5.2866650E+02	+6.2139627E+01	+5.9800000E+02	+4.7800000E+02	+4.4177368E+02
116.0	3	+5.1066650E+02	+1.1547005E+01	+5.2400000E+02	+5.0400000E+02	+4.4746093E+02
132.0	3	+4.2600000E+02	+3.7469987E+01	+4.5600000E+02	+3.8400000E+02	+4.5656054E+02
143.0	3	+3.3466650E+02	+2.1197484E+01	+3.5400000E+02	+3.1200000E+02	+4.6281665E+02
151.0	3	+4.8200000E+02	+7.2111025E+00	+4.9000000E+02	+4.7600000E+02	+4.6736645E+02
166.0	3	+4.3266650E+02	+2.5006665E+01	+4.5000000E+02	+4.0400000E+02	+4.7589746E+02
191.0	3	+4.7200000E+02	+3.4641016E+00	+4.7400000E+02	+4.6800000E+02	+4.9011547E+02
202.0	3	+4.5066650E+02	+6.1101009E+00	+4.5600000E+02	+4.4400000E+02	+4.9637158E+02
230.0	3	+5.8866650E+02	+1.5143755E+01	+6.0600000E+02	+5.7800000E+02	+5.1229589E+02
241.0	6	+5.3266650E+02	+8.2060140E+01	+6.6800000E+02	+4.4600000E+02	+5.1855200E+02
250.0	10	+5.2259985E+02	+5.7237190E+01	+6.2400000E+02	+4.4200000E+02	+5.2367065E+02

STAGE 1, DISCTED MOTOR=0012199, STRESS RELAXATION MODULUS,5 X STRAIN AT 100 SEC.

$F = +4.1480012E+00$
 $R = +3.0310993E-01$
 $S = +2.0366642E+00$
 $t = 43$
 $N = 43$
 $\gamma = (1 + 3.2221324E+02) + (3.1643825E-01) \cdot X_1$
 $F = \text{SIGNIFICANT}$
 $R = \text{SIGNIFICANT}$
 $S = \text{SIGNIFICANT}$
 $t = \text{SIGNIFICANT}$
 $D = \text{DEGREES OF FREEDOM} = 41$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$

PARAMETER = STRESS RELAX MODULUS

UNIT OF MEASURE = PSI

290.00 270.00 350.00 430.00 510.00 590.00

STAGE 1. RISCTEC MOTOR=0012199, STRESS RELAXATION MODULUS, % STRAIN AT 1000 SEC.

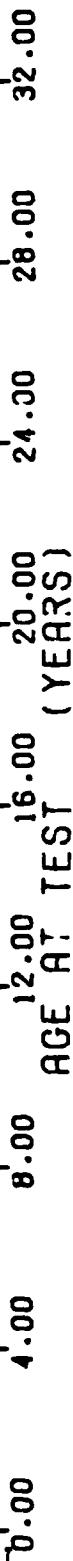


Figure 35

$\gamma = 11 \cdot 3752075E+00$
 $F = 1 \cdot 3752075E+00$
 $R = +1 \cdot 0917617E-01$
 $S = +1 \cdot 1726924E+00$
 $N = 116$
 $D = 114$
 $S = \text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $F = \text{SIGNIFICANCE OF F} = \text{NOT SIGNIFICANT}$
 $R = \text{SIGNIFICANCE OF R} = \text{NOT SIGNIFICANT}$
 $S = \text{SIGNIFICANCE OF S} = \text{NOT SIGNIFICANT}$
 $D = \text{DEGREES OF FREEDOM} = 114$
 $X = 1 \cdot 2872389E-01$
 $G = 6 \cdot 6893089E+01$
 $S_0 = +1 \cdot 0976782E-01$
 $S_1 = +6 \cdot 6784230E+01$

TEST CONDITIONS = AMB TEMP/RH

$\text{PARAMETER} = \text{STRESS RELAX MODULUS}$
 $\text{UNIT OF MEASURE} = \text{PSI}$
 $29.00 \quad 39.00 \quad 49.00 \quad 59.00 \quad 69.00$

TP-H1011 DISSECTED MTRS. STRESS RELAXATION MODULUS. 5 PERCENT STRAIN. 1000 SEC

Figure 35A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

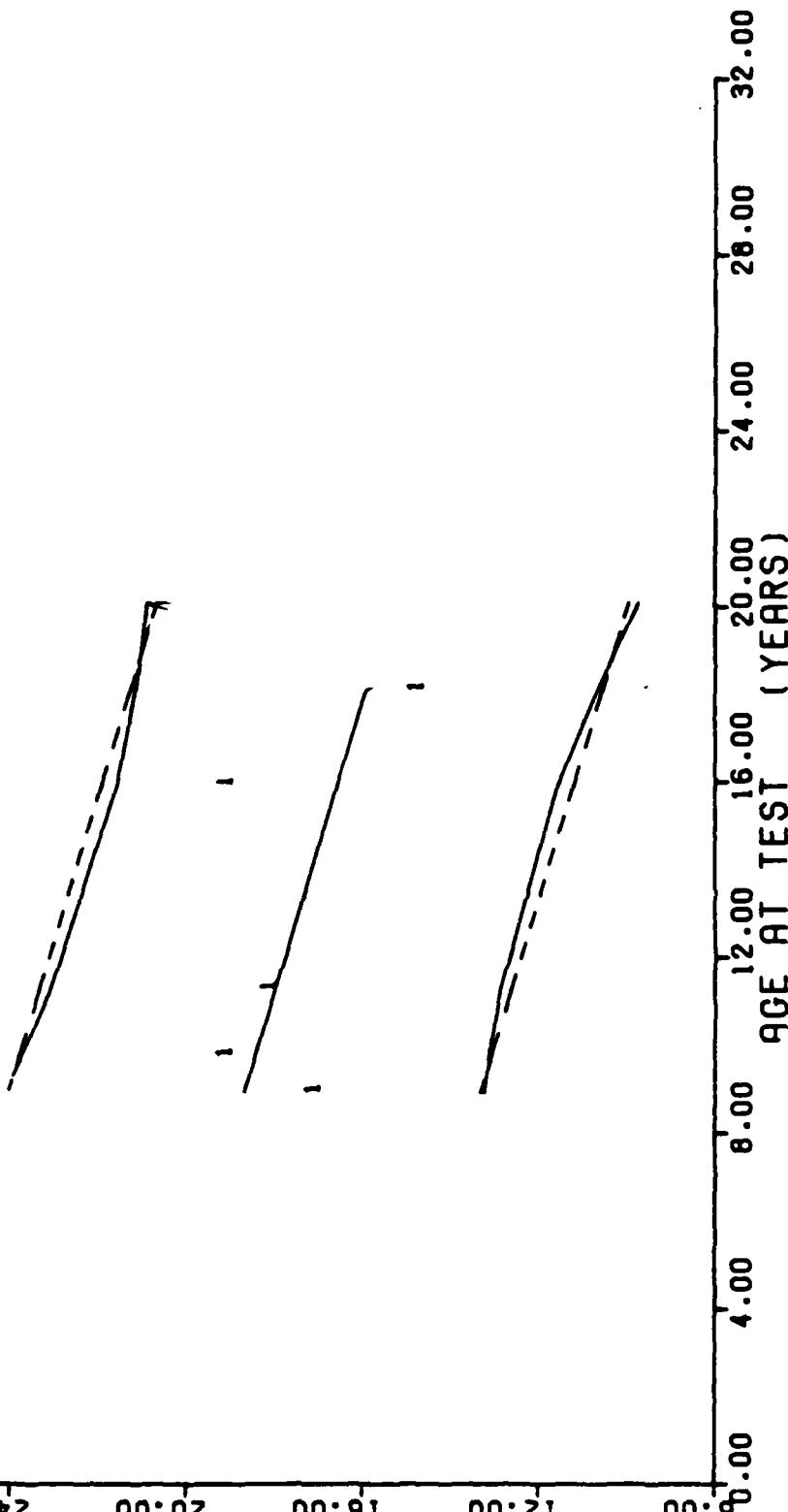
AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	3	+4.2333325E+02	+5.0649119E+01	+4.7800000E+02	+3.7800000E+02	+3.5575561E+02
116.0	3	+4.0266650E+02	+1.3316656E+01	+4.1800000E+02	+3.9400000E+02	+3.5891992E+02
132.0	3	+3.3733325E+02	+2.5716402E+01	+3.5600000E+02	+3.0800000E+02	+3.6398291E+02
143.0	3	+2.7200000E+02	+1.9078784E+01	+2.9000000E+02	+2.5200000E+02	+3.6746386E+02
151.0	3	+3.7733325E+02	+7.0237691E+00	+3.8400000E+02	+3.7000000E+02	+3.6999536E+02
166.0	3	+3.5000000E+02	+1.9078784E+01	+3.6200000E+02	+3.2800000E+02	+3.7474194E+02
191.0	3	+3.7000000E+02	+3.4641016E+00	+3.7400000E+02	+3.6600000E+02	+3.8265263E+02
202.0	3	+3.4933325E+02	+1.1547005E+00	+3.5000000E+02	+3.4800000E+02	+3.8613354E+02
230.0	3	+4.7066650E+02	+8.3266639E+00	+4.8000000E+02	+4.6400000E+02	+3.9499389E+02
241.0	6	+4.0500000E+02	+5.7267791E+01	+5.0200000E+02	+3.4600000E+02	+3.9847485E+02
250.0	10	+3.9800000E+02	+4.4899888E+01	+4.7400000E+02	+3.3000000E+02	+4.0132275E+02

STAGE 1, DISCTED MATOR=0012199, STRESS RELAXATION MODULUS X STRAIN AT 1000 SEC.

$F = +3.3168119E+00$
 $r = -5.6700601E-01$
 $s = +1.8212116E+00$
 $N = 9$
 STORAGE CONDITIONS = AMB TEMP/RH
 $f = ((+2.1375756E+01) + (-2.5135436E-02) * X)$
 $r = (SIGNIFICANCE \text{ OF } F = NOT \text{ SIGNIFICANT})$
 $s = (SIGNIFICANCE \text{ OF } R = NOT \text{ SIGNIFICANT})$
 $N = (SIGNIFICANCE \text{ OF } S = NOT \text{ SIGNIFICANT})$
 $Degrees \text{ of } Freedom = 7$
 TEST CONDITIONS = AMB TEMP/RH

STORAGE CONDITIONS = AMB TEMP/RH DEGREES OF FREEDOM = TEST CONDITIONS = AMB TEMP/RH

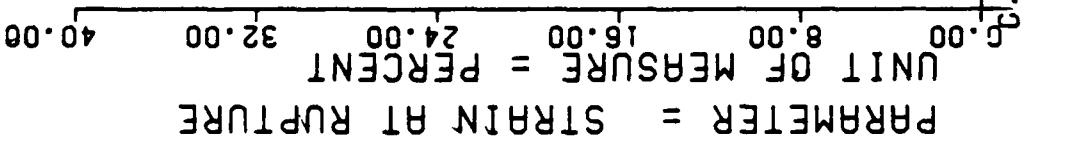
PARAMETER = STRAIN AT RUPTURE



SOURCE 1: OSSCID MIR=0012199,CONTIANI STRAIN,SIRAIN G-1 INIT 4 0.01 FEVER 4A HRS.

Figure 36

$f = +7.2438067E+01$ $f' = ((+2.7766417E+01) + (-5.8466116E-02)) \cdot X$
 $\sigma_f = +4.5386348E+00$
 $r = -8.2496388E-01$ SIGNIFICANCE OF $F = \text{SIGNIFICANT}$
 $R = +8.5110556E+00$ SIGNIFICANCE OF $R = \text{SIGNIFICANT}$
 $\nu = 36$ SIGNIFICANCE OF $\nu = \text{SIGNIFICANT}$
 $D = 34$ DEGREES OF FREEDOM = 34
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



STAGE 1.DSSCTD MTR COMBINED, CONSTANT STRAIN, STRAIN 0.1 INIT & 0.01 EVERY 48 HRS.

Figure 36A

*** LINEAR ELASTICITY ANALYSIS ***

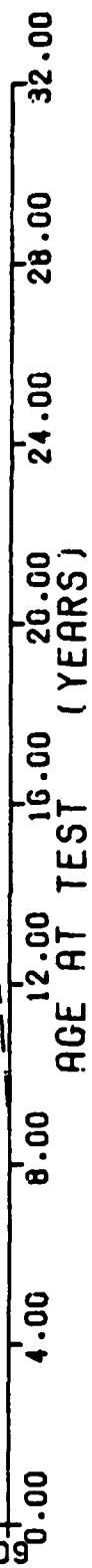
** ANALYSIS OF TIE STATUS **

ANALYSIS (NUMBER)	SET UP NUMBER	PLAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	PENALTY Y
1.01•0	1	+1.700000E+01	+0.000000E+07	+1.700000E+01	+1.700000E+01	+1.86862E4E+01
1.11•0	1	+1.900000E+01	+0.000000E+07	+1.900000E+01	+1.900000E+01	+1.84344E+01
1.25•0	2	+1.900000E+01	+1.42139E+00	+1.900000E+01	+1.700000E+01	+1.79E24E7F+01
1.41•0	4	+1.900000E+01	+0.303000E+07	+1.900000E+01	+1.900000E+01	+1.65744E74E+01
-1.17•0	3	+1.400000E+01	+5.7715020E-01	+1.500000E+01	+1.400000E+01	+1.59213E+01

DATA 1.003370 HTR=0012199, CONSTANT STRAIN, STRAIN 0.1 INIT & 0.01 EVERY 48 HRS.

$F = +6.8924941E-01$ $\gamma = ((+6.6405700E+01) + (+6.18995352E-03)) \equiv \chi$
 $R = +7.8386476E-02$ SIGNIFICANCE OF $F = \text{NOT SIGNIFICANT}$ $\sigma_r = +2.3494828E+00$
 $I = +8.2840172E-01$ SIGNIFICANCE OF $R = \text{NOT SIGNIFICANT}$ $S_o = +7.4716591E-03$
 $N = 113$ DEGREES OF FREEDOM = 111 SIGNIFICANCE OF $I = \text{NOT SIGNIFICANT}$ $S_i = +2.3527806E+00$
STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

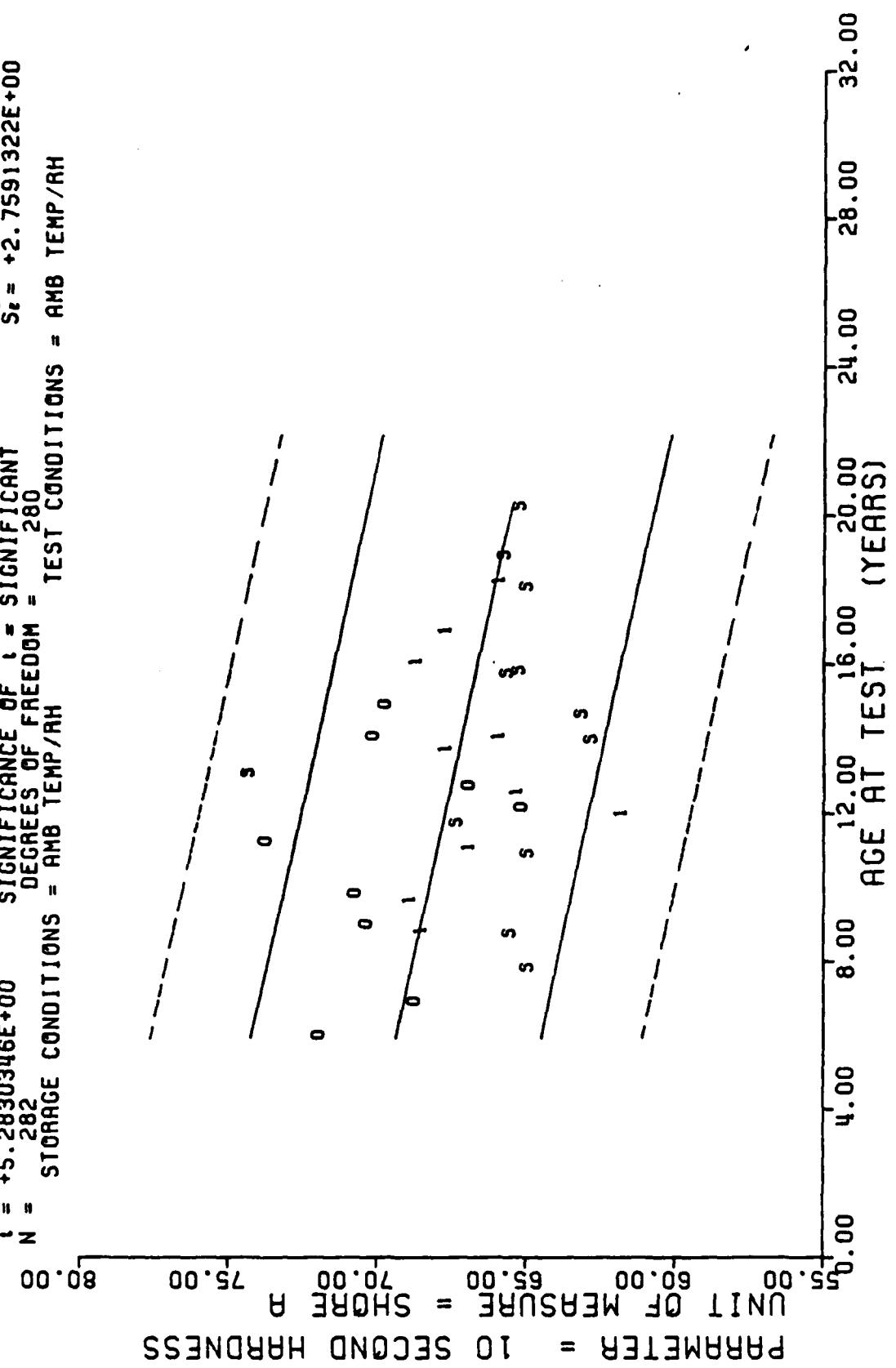
PARAMETER = 10 SECOND HARDNESS
UNIT OF MEASURE = SHORE A
60.00 64.00 68.00 72.00 76.00 80.00



STAGE 1. DISSECTED MOTOR=1100012199, SHORE-A HARDNESS, 10 SECOND.

Figure 37

$F = +2.7910455E+01$
 $R = -3.0107260E-01$
 $I^2 = +5.2830346E+00$
 $N = 282$
 Y = $((+7.0971554E+01) + (-2.2473799E-02) \times X)$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF I^2 = SIGNIFICANT
 DEGREES OF FREEDOM = 280
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



*** LINEAR REGRESSION ANALYSIS ***

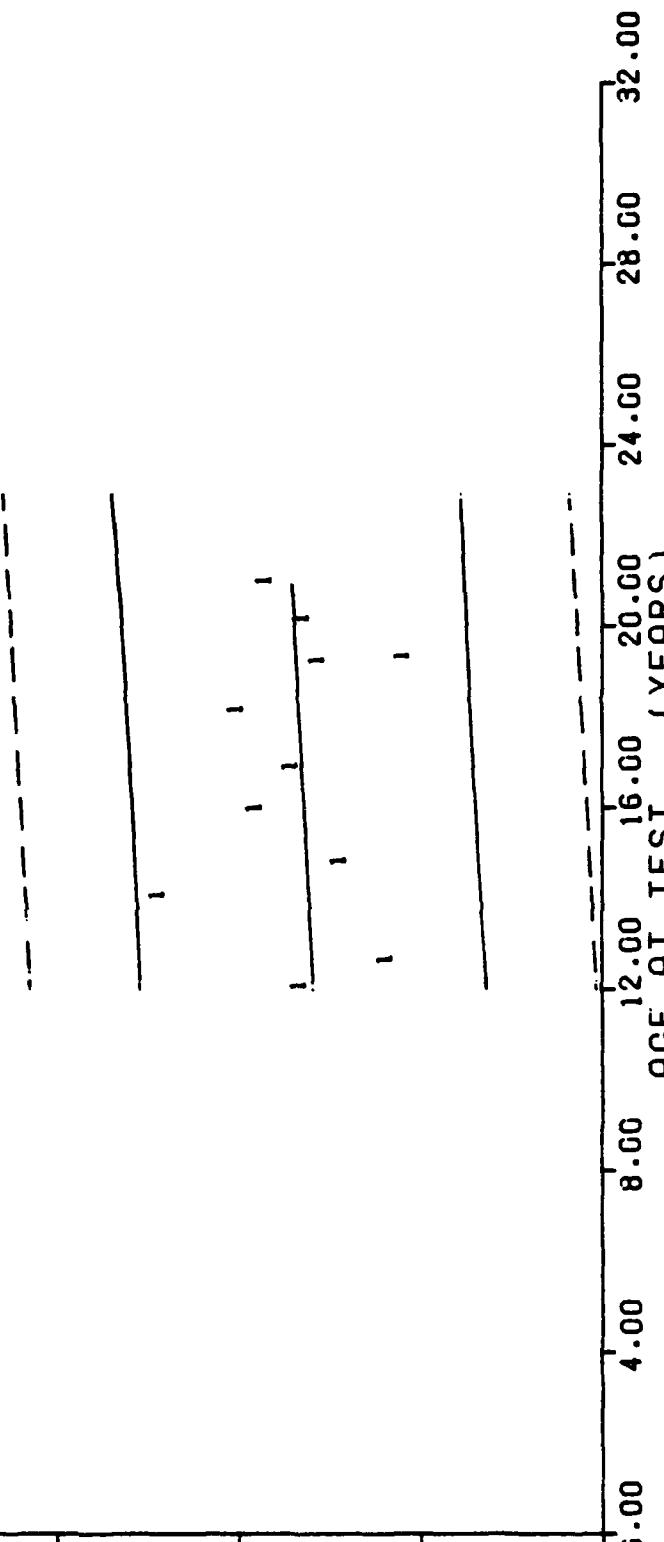
*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
1.05•.0	5	+6.8399993E+01	+1.5165750E+00	+7.0000000E+01	+6.7000000E+01	+6.7055587E+01
1.15•.0	5	+6.8799987E+01	+1.0954451E+00	+7.0000000E+01	+6.7000000E+01	+6.7117492E+01
1.22•.0	5	+6.6799987E+01	+2.2803508E+00	+6.9000000E+01	+6.4000000E+01	+6.7222717E+01
1.43•.0	3	+6.1666056E+01	+1.5275252E+00	+6.3000000E+01	+6.0000000E+01	+6.7290802E+01
1.50•.0	5	+6.5199996E+01	+4.4721359E-01	+6.6000000E+01	+6.5000000E+01	+6.7334121E+01
1.64•.0	10	+6.7599990E+01	+1.1737877E+00	+7.3000030E+01	+6.6000000E+01	+6.7420776E+01
1.68•.0	10	+6.5799988E+01	+1.2222725E+00	+6.8000000E+01	+6.4000000E+01	+6.7445541E+01
1.92•.0	50	+6.85799988E+01	+2.3307176E+00	+7.1000000E+01	+6.0000000E+01	+6.7594085E+01
2.02•.0	10	+6.7599990E+01	+1.1737877E+00	+7.0000000E+01	+6.6000000E+01	+6.7655975E+01
2.18•.0	10	+6.5799988E+01	+1.2292725E+00	+6.8000000E+01	+6.4000000F+01	+6.7755004E+01

STAGE 1. DISSECTED MOTOR=(1)0012199. SHORE-A HARDNESS. 10 SECOND.

$y = (+1.1404793E+00) + (+8.8461831E-04) \times x$
 $F = +7.1433890E-01$ SIGNIFICANCE OF F = NOT SIGNIFICANT
 $R = +8.0324904E-02$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $t = +8.4518572E-01$ SIGNIFICANCE OF t = NOT SIGNIFICANT
 $N = 112$ DEGREES OF FREEDOM = 110
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = COHESIVE ENERGY
 UNIT OF MEASURE = PSI
 0.60 0.80 1.60 2.40 3.20 4.00

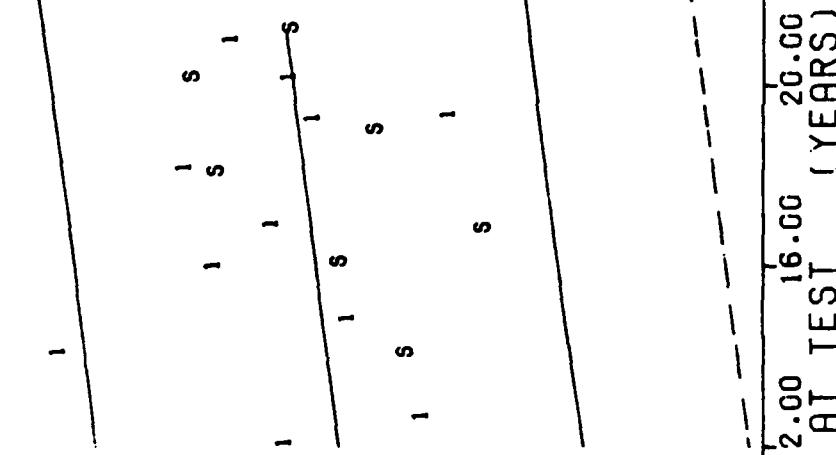


STAGE 1 DISSECTED MOTOR=0012199, YEAR ENERGY, CHS=0.1 IN/MIN.T/TEMP=77 DEG.

Figure 38

$F = +2.8554585E+00$
 $R = +1.2328947E-01$
 $t = +1.6898102E+00$
 $N = 187$
 $Y = ((+9.7432715E-01) + (+1.355C116E-03) * X)$
 $F = \text{NOT SIGNIFICANT}$
 $R = \text{NOT SIGNIFICANT}$
 $t = \text{NOT SIGNIFICANT}$
 $N = \text{NOT SIGNIFICANT}$
 $\text{DEGREES OF FREEDOM} = 185$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

$\text{PARAMETER} = \text{COHESIVE ENERGY}$
 $\text{UNIT OF MEASURE} = \text{PSI}$
 0.00 0.50 1.00 1.50 2.00 2.50



STAGE 1. DISSECTED MOTORS=110012199 4 (SYSTEM-012, TEAR ENERGY, CHS=0.1 AT 77 DEG

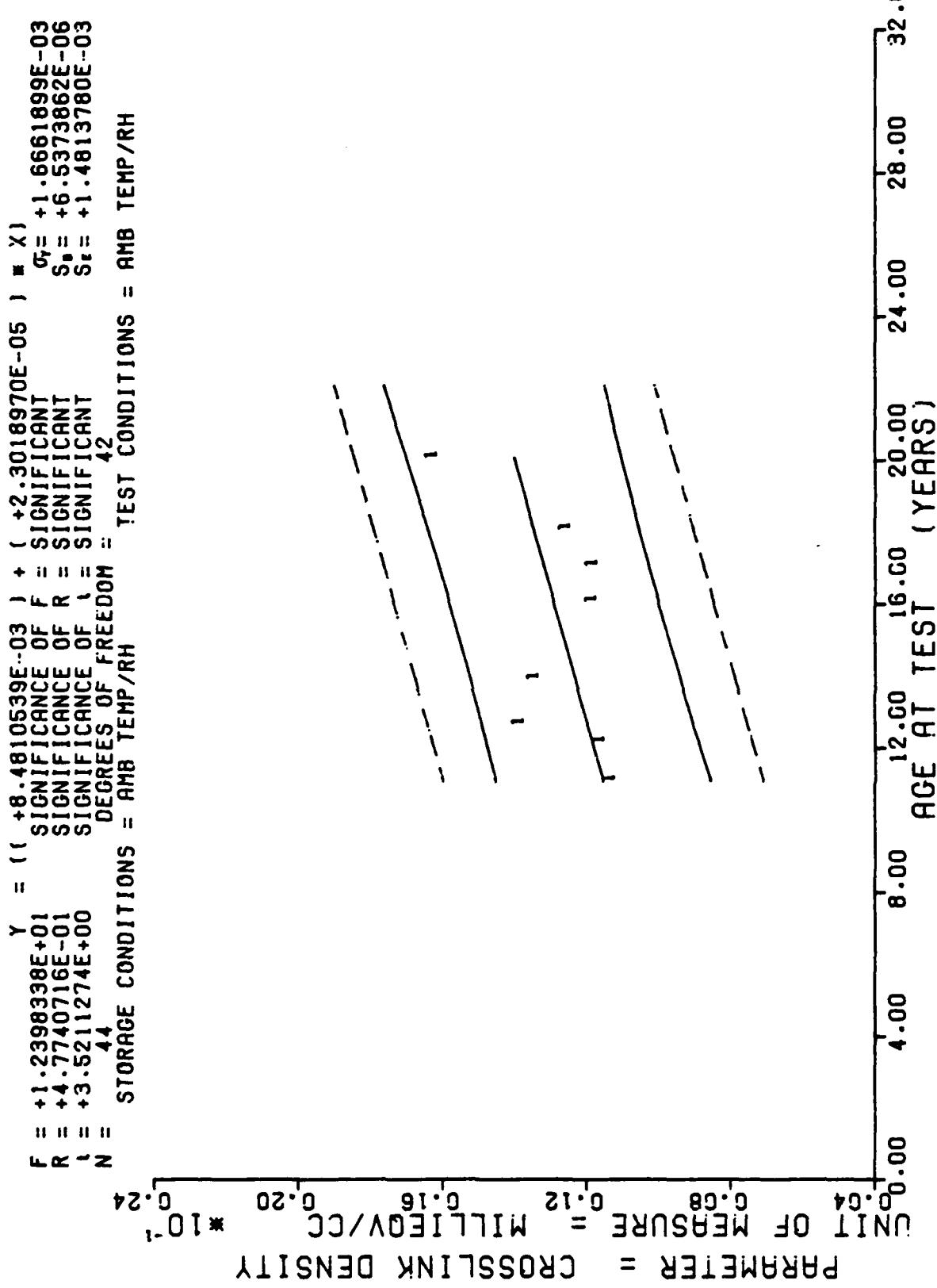
Figure 38A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIANS PER GROUP	MEAN Y	STANDARD DEVIATION		MAXIMUM Y	MINIMUM Y	REGRESSION Y
			STANDARD DEVIATION	STANDARD DEVIATION			
144.0	8	+1.3054866E+00	+2.4540969E-01	+1.6974992E+00	+9.1229999E-01	+1.2678642E+00	
151.0	17	+9.2757010E-01	+3.4659752E-01	+1.5503992E+00	+5.1189994E-01	+1.2740564E+00	
163.0	11	+1.9317884E+00	+4.6594024E-01	+2.5883598E+00	+1.2885999E+00	+1.2890949E+00	
177.0	8	+1.1311111E+00	+3.3515019E-01	+1.6190596E+00	+7.6609998E-01	+1.2970561E+00	
191.0	6	+1.5033864E+00	+3.2887333E-01	+2.0490999E+00	+9.9919998E-01	+1.3094406E+00	
202.0	10	+1.3446292E+00	+2.7193437E-01	+1.7876996E+00	+9.6319997E-01	+1.3191719E+00	
217.0	8	+1.5829744E+00	+3.1690500E-01	+2.1384992E+00	+1.1258993E+00	+1.3324413E+00	
230.0	9	+1.2281208E+00	+1.4474297E-01	+1.4004993E+00	+9.6739995E-01	+1.3439407E+00	
231.0	8	+8.5437452E-01	+4.7410577E-02	+9.3389999E-01	+8.0999994E-01	+1.3448257E+00	
241.0	9	+1.2973098E+00	+1.5053359E-01	+1.5008993E+00	+1.1089992E+00	+1.3536720E+00	
251.0	16	+1.4568910E+00	+2.9180035L-01	+1.9438592E+00	+1.1238994E+00	+1.3625183E+00	

STAGE 1. DISSECTED MOTOR=0012199, YEAR ENERGY, CIS=0.1 IN/MIN,T/TEMP=77 DEG.

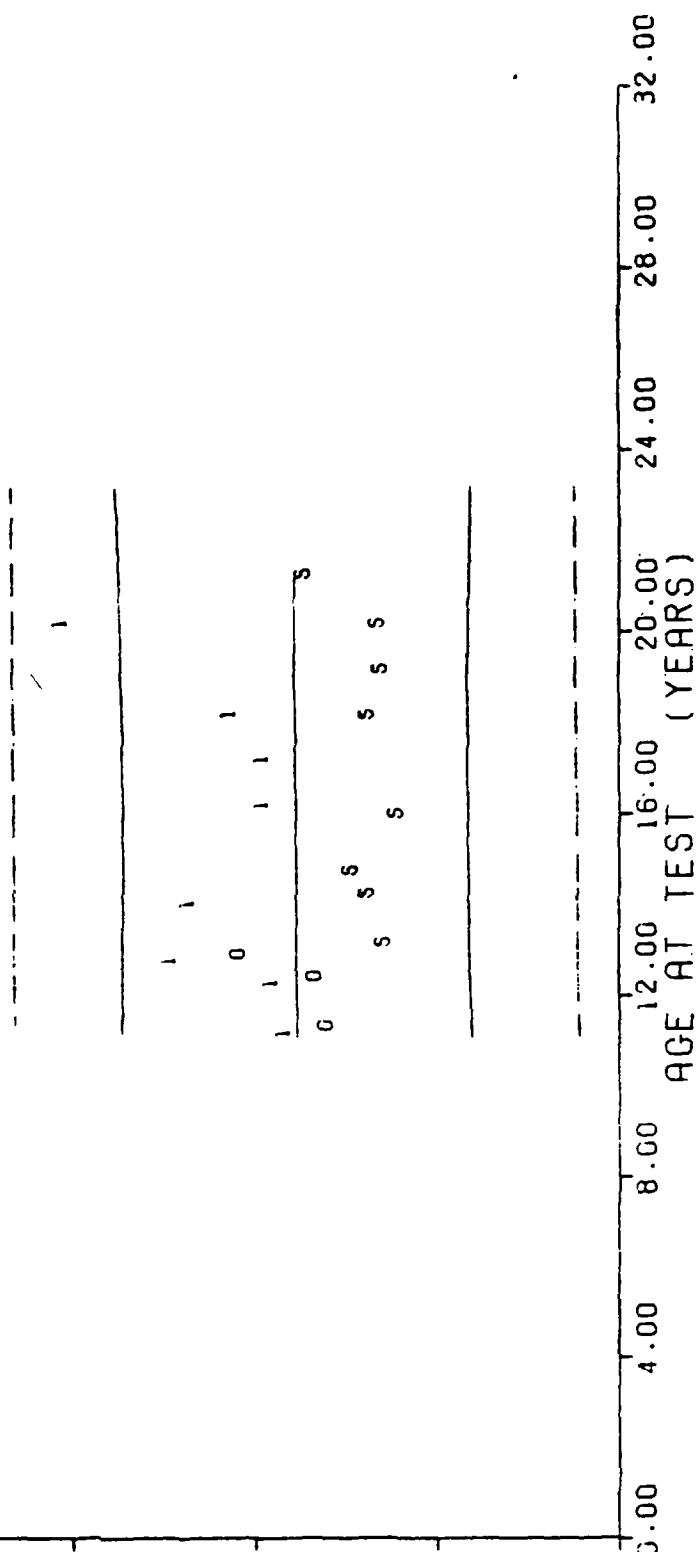


DISSECTED MTR, STAGE 1, TP-H1011, SOL GEL, CROSSLINK DENSITY, MOTOR=0012199.

Figure 39

$F = +1.4898971E-02$
 $R = +1.2588668E-02$
 $I = +1.2206134E-01$
 $N = 96$
 $Y = ((+1.0994496E-02) + (+7.2035647E-07) * X)$
 $S = NOT SIGNIFICANT$
 $S = NOT SIGNIFICANT$
 $S = NOT SIGNIFICANT$
 $S = NOT SIGNIFICANT$
 $DGREES OF FREEDOM = 94$
 $STORAGE CONDITIONS = AMB TEMP/RH$

PARAMETER = CROSSLINK DENSITY
 $C_{INIT} \text{ OF MEASURE} = \text{ MILLIEGKV/CC}$
 0.04
 0.08
 0.12
 0.16
 0.20
 $* 10^{-3}$



DISSECTED MTR. STAGE 1. TP-H1011. SOL GEL. CROSSLINK DENSITY

Figure 39A

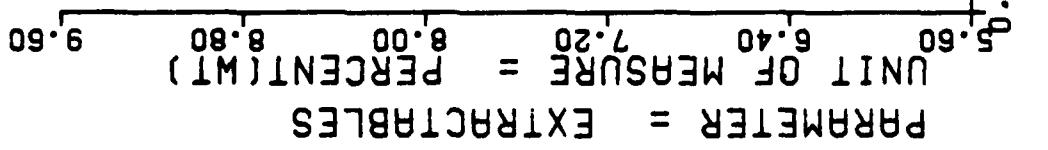
*** LIFFAP INF GEL POSITION ANALYSIS ***

*** ANALYSIS OF TIME STEPS ***

Age (days)	Inf Gel Top	STANDARD			MAXIMUM Y	MINIMUM Y	PLATEAU Y
		MEAN Y	DEVIATION	Y			
1.53•0	4	+1.1268490E-02	+3.3474339E-04	+1.1635397E-02	+1.0865997E-02	+1.1542573E-02	
1.49•0	4	+1.1549944E-02	+0.5070192E-04	+1.2386996E-02	+1.0865997E-02	+1.1841822E-02	
1.52•0	4	+1.3792496E-02	+7.4063018E-04	+1.4402690E-02	+1.2901990E-02	+1.1970933E-02	
1.67•0	0	+1.3390321E-02	+5.5357095E-04	+1.4407999E-02	+1.2906986E-02	+1.2325219E-02	
1.82•0	0	+1.1778324E-02	+6.3328713E-04	+1.2628998E-02	+1.1050999E-02	+1.2923713E-02	
2.05•0	8	+1.1750556E-02	+5.0922950E-04	+1.2629397E-02	+1.1050607E-02	+1.3199940E-02	
2.17•0	0	+1.2492854E-02	+8.4855124E-04	+1.3279799E-02	+1.1251598E-02	+1.3476170E-02	
2.41•0	0	+1.6193576E-02	+3.8753037E-04	+1.6725398E-02	+1.5627298E-02	+1.4028623E-02	

DISTRIBUTED FTR, STAGE 1, TP-H1011, SOL GEL, CROSSLINK DENSITY, MOTOR=0012199.

$y = ((+5.8586992E+00) + (+6.6973202E-03) * x)$
 $F = +1.6678520E+01$ SIGNIFICANT
 $R = +5.3313744E-01$ SIGNIFICANT
 $s_r = +4.0839344E+00$ SIGNIFICANT
 $N = 44$ DEGREES OF FREEDOM = 42
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

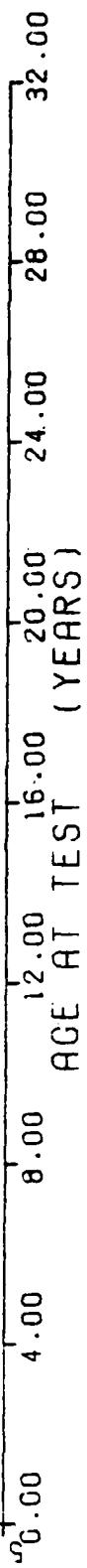


DISSECTED MTR, STAGE 1. TP-H1011. SOL GEL. PERCENT EXTRACTABLES. MOTOR=0012199.

Figure 40

$\gamma = +2 \cdot 6450012E+01$
 $R_s = +4 \cdot 6860780E-01$
 $t = +5 \cdot 1429575E+00$
 $N = 96$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF t = SIGNIFICANT
 DEGREES OF FREEDOM = 94
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = PERCENT (WT)
 PARAMETER = EXTRACTABLES



DISSECTED MTR STAGE I, TP-H1011, SOL GEL, PERCENT EXTRACTABLES

Figure 40A

**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (YEARS)	JOINTS PER CENT	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
17.3 .0	4	+7.2634968E+00	+1.9579601E-02	+7.3009996L+00	+7.2599992E+00	+6.7494421E+00
146 .0	4	+7.0024948E+00	+9.1140311E-02	+7.1279603E+00	+6.9340994E+00	+6.8365077E+00
152 .0	4	+6.2747459E+00	+2.7616375E-02	+6.3045593E+00	+6.2509994E+00	+6.8766918E+00
167 .0	6	+6.7723283E+00	+5.1643936E-02	+6.8399961E+00	+6.6919994E+00	+6.9771509E+00
173 .0	6	+6.8493270E+00	+7.7372235E-02	+6.9779951E+00	+6.7629995E+00	+7.1512813E+00
185 .0	6	+7.477949E+00	+1.7643032E-01	+7.7169930E+00	+7.3159999E+00	+7.2316493E+00
217 .0	6	+7.502645E+00	+1.5661292L-01	+7.771993E+00	+7.3489999E+00	+7.3120174E+00
241 .0	6	+7.394937E+00	+4.7917542E-01	+8.174992F+00	+6.9009990E+00	+7.4727525E+00

DISTRIBUTED MTR, STAGE 1, TP-11011, SOL GLI, PERCENT EXTRACTABLES, MOTOR=0012199.

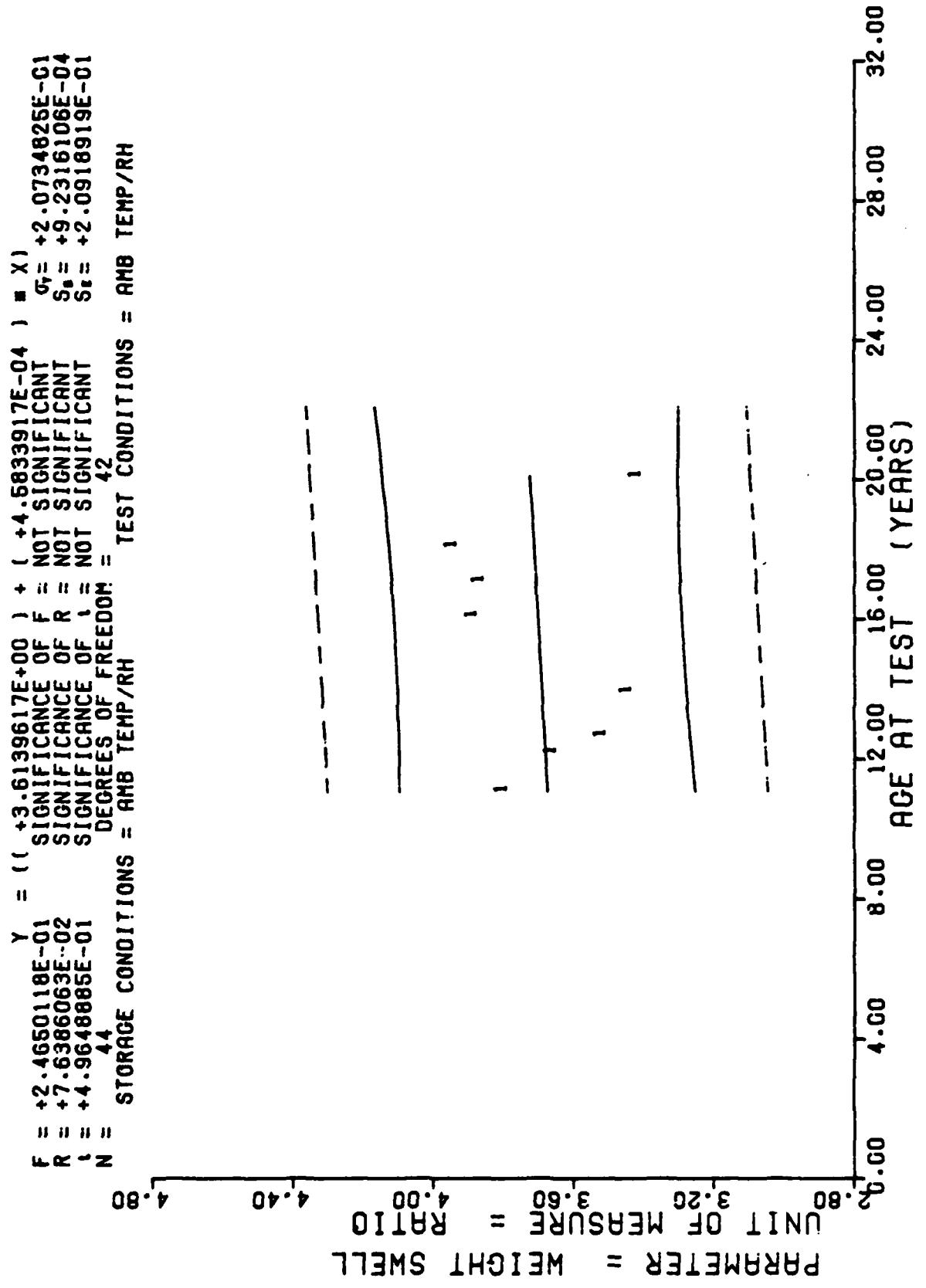


Figure 41

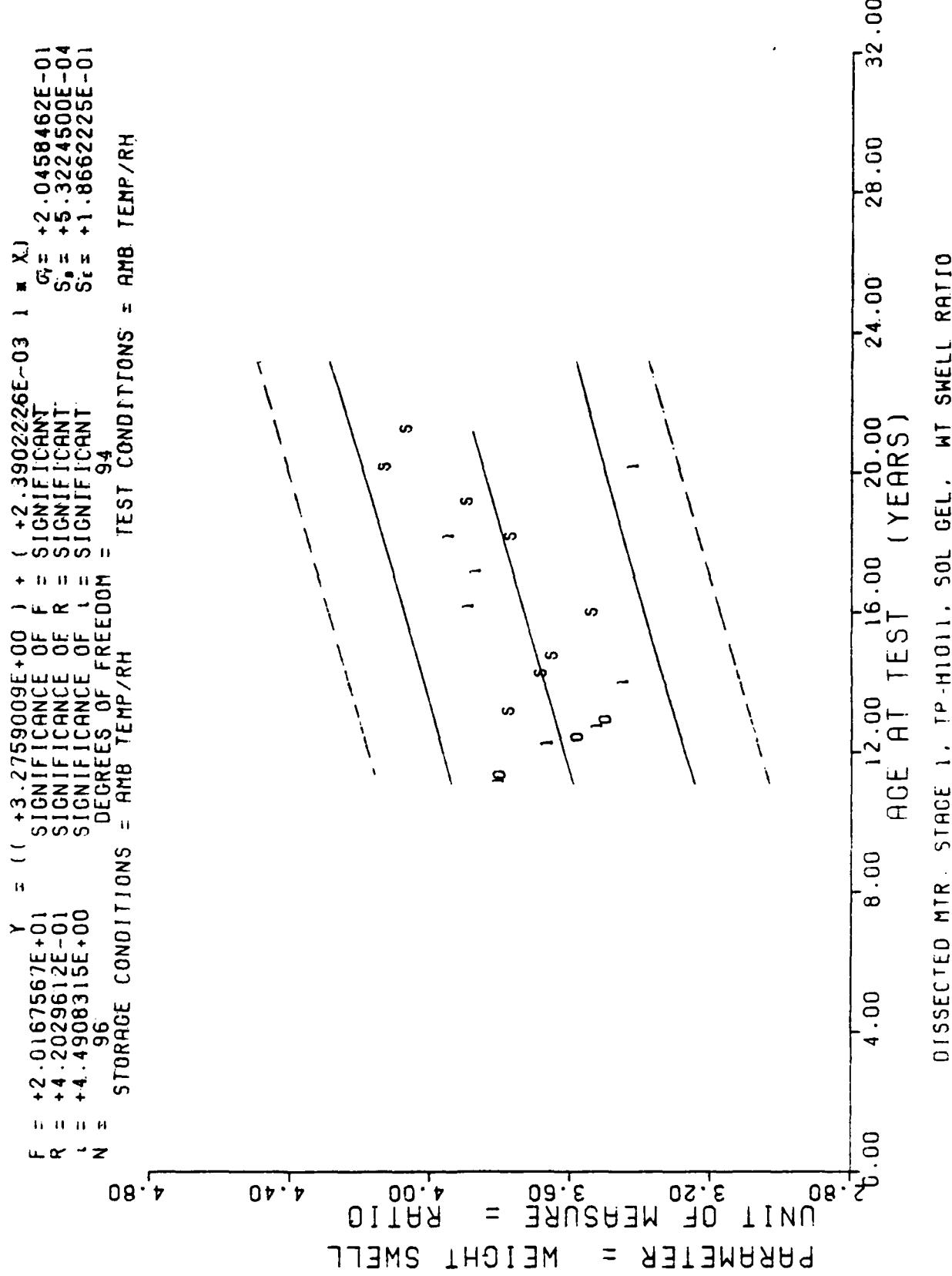


Figure 41A

*** LINEAR REGRESSION ANALYSIS ***

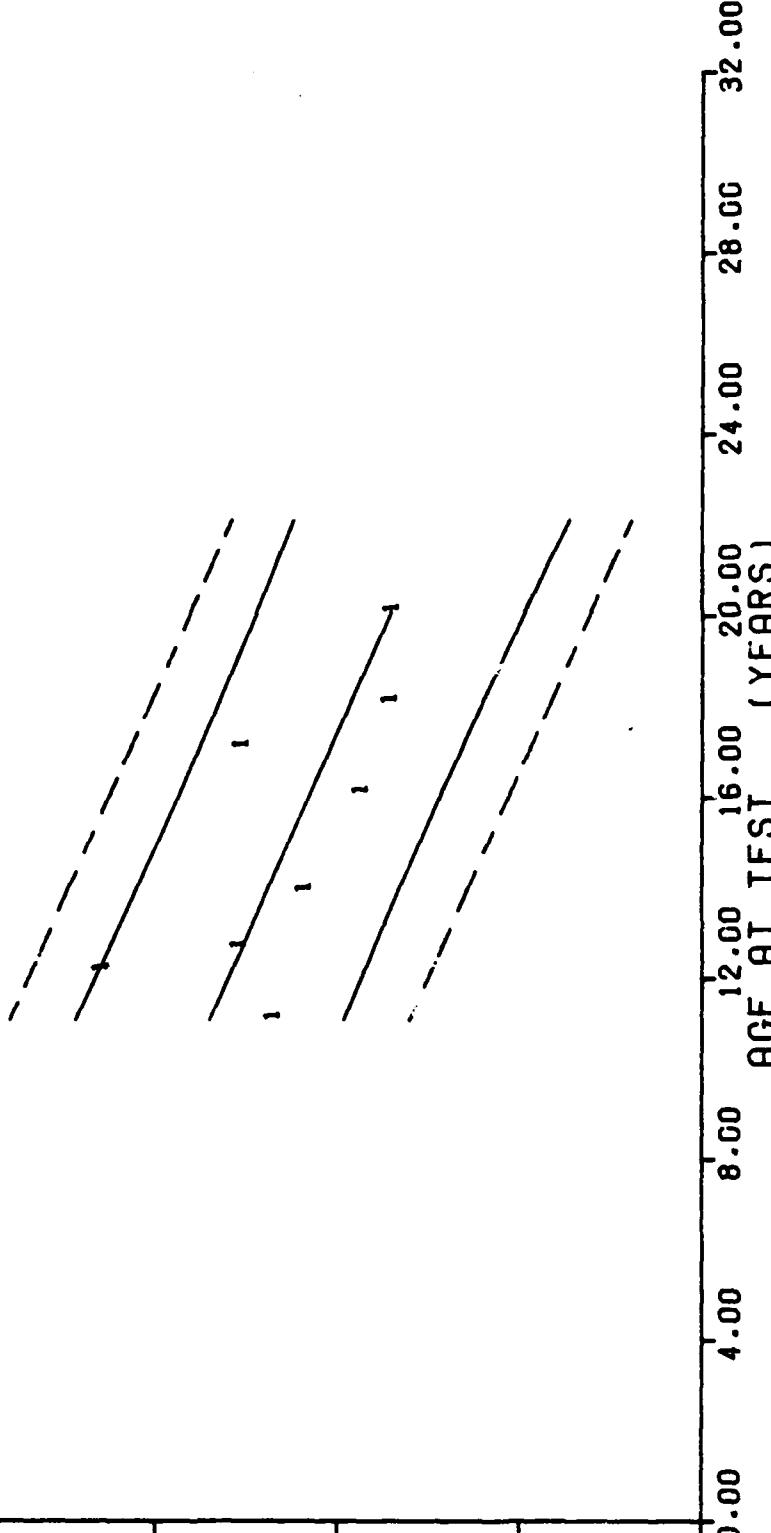
*** ANALYSIS OF TIME SERIES ***

A _{df} (deg. freedom)	SIGNALS W ₁ , W ₂ , GROUP	MEAN Y	STANDARD DEVIATION	MINIMUM Y		REGRESSION Y
				MAXIMUM Y	MINIMUM Y	
1.310	4	+3.7952489E+00	+1.9550496E-02	+3.6123598E+00	+3.7782993E+00	+3.6749200E+00
1.460	4	+3.6556491E+00	+1.3345124E-02	+3.671796E+00	+3.6299991E+00	+3.6808786E+00
1.620	4	+3.5143241E+00	+1.457364E-02	+3.5322599E+00	+3.4986991E+00	+3.6836290E+00
1.670	0	+3.4415149E+00	+4.1119079E-02	+3.4979991E+00	+3.3872995E+00	+3.6905040E+00
1.930	0	+3.3813648E+00	+1.1694731E-02	+3.6948693E+00	+3.8645992E+00	+3.7024211E+00
2.010	8	+3.622207E+00	+1.8234965E-02	+3.8157994E+00	+3.8403997F+00	+3.7079210F+00
-1.170	0	+3.9387733E+00	+2.0736030E-02	+3.9690591E+00	+3.8087998E+00	+3.7124208E+00
2.410	0	+3.4123313E+00	+2.6673100E-02	+3.4664593E+00	+3.3948993E+00	+3.7244215E+00

DISLECTED MTR, STAGE 1, T_p-H1011, SOL GEL, WT SWELL RATIO MOTOR=0012199.

$y = (1 + 1.7985522e+01) + (-1.8421165e-04) \ln(x)$
 $F = +3.2591998e+01$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = -6.6101204e-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $s_e = +5.7089402e+00$ SIGNIFICANCE OF s_e = SIGNIFICANT
 $N = 44$ DEGREES OF FREEDOM = 42
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = GRAMS/CC
 PARAMETER = DENSITY

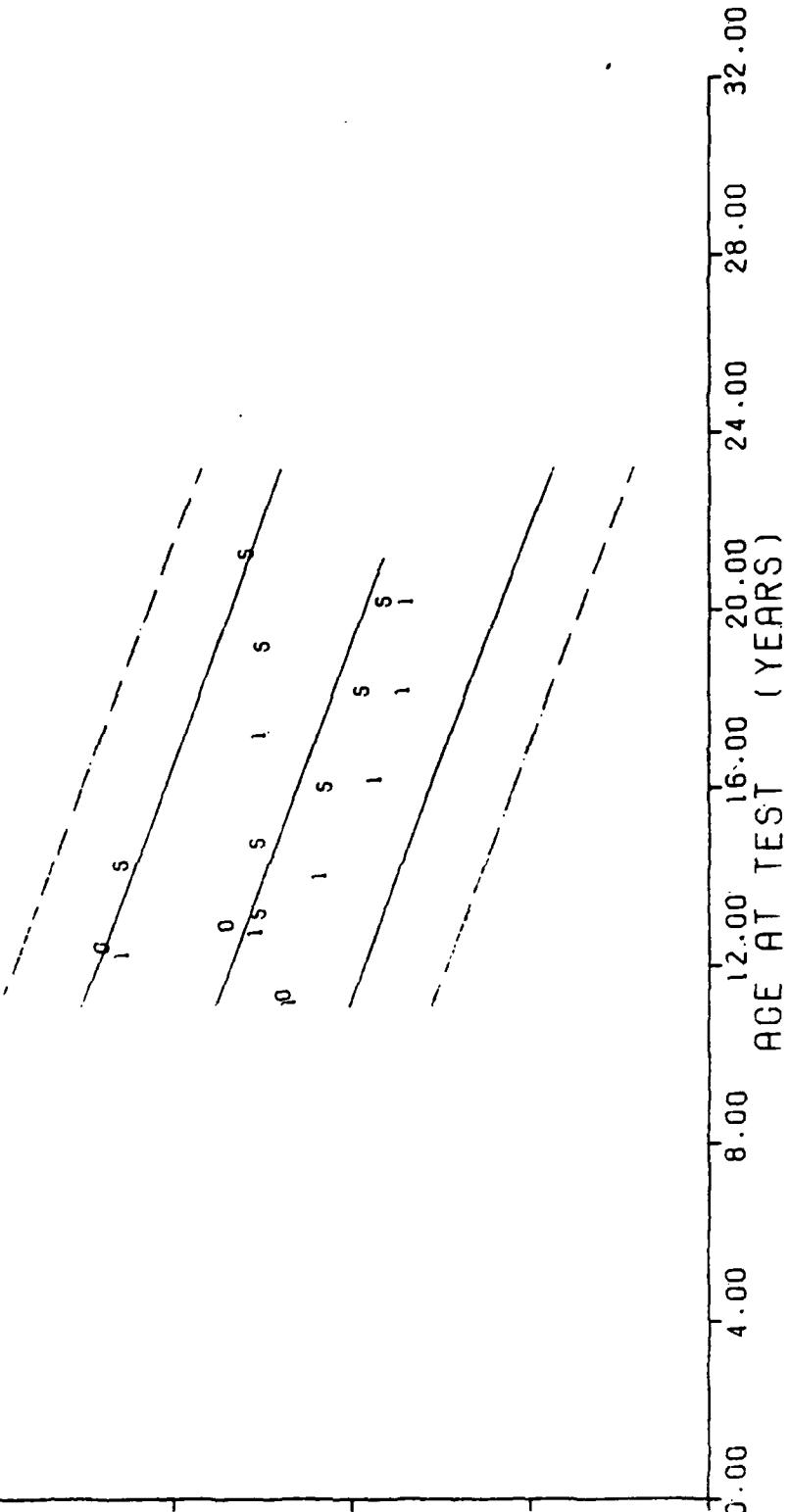


STAGE 1, DISSECTED MTRS, SOL GEL, DENSITY, MOTOR=0012199.

Figure 42

$F = +4.5262453E+01$ $y = 11 +1.7960472E+00$ $1 + (-1.5536187E-04)$ x_1
 $R = -5.7010129E-01$ SIGNIFICANCE OF F = SIGNIFICANT
 $s_r = +6.7277376E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $t = 96$ SIGNIFICANCE OF L = SIGNIFICANT
 $N = 96$ DEGREES OF FREEDOM = 94
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = GRAMS/CC
 PARAMETER = DENSITY



STAGE 1, DISSECTED MTRS=(0)0012099, (1)0012199, (S)STM-012. SOL GEL DENSITY.

Figure 42A

*** LIQUID ANALYSIS OF 14 ANALYSIS ***

*** ANALYSIS OF LIQUID SAMPLES ***

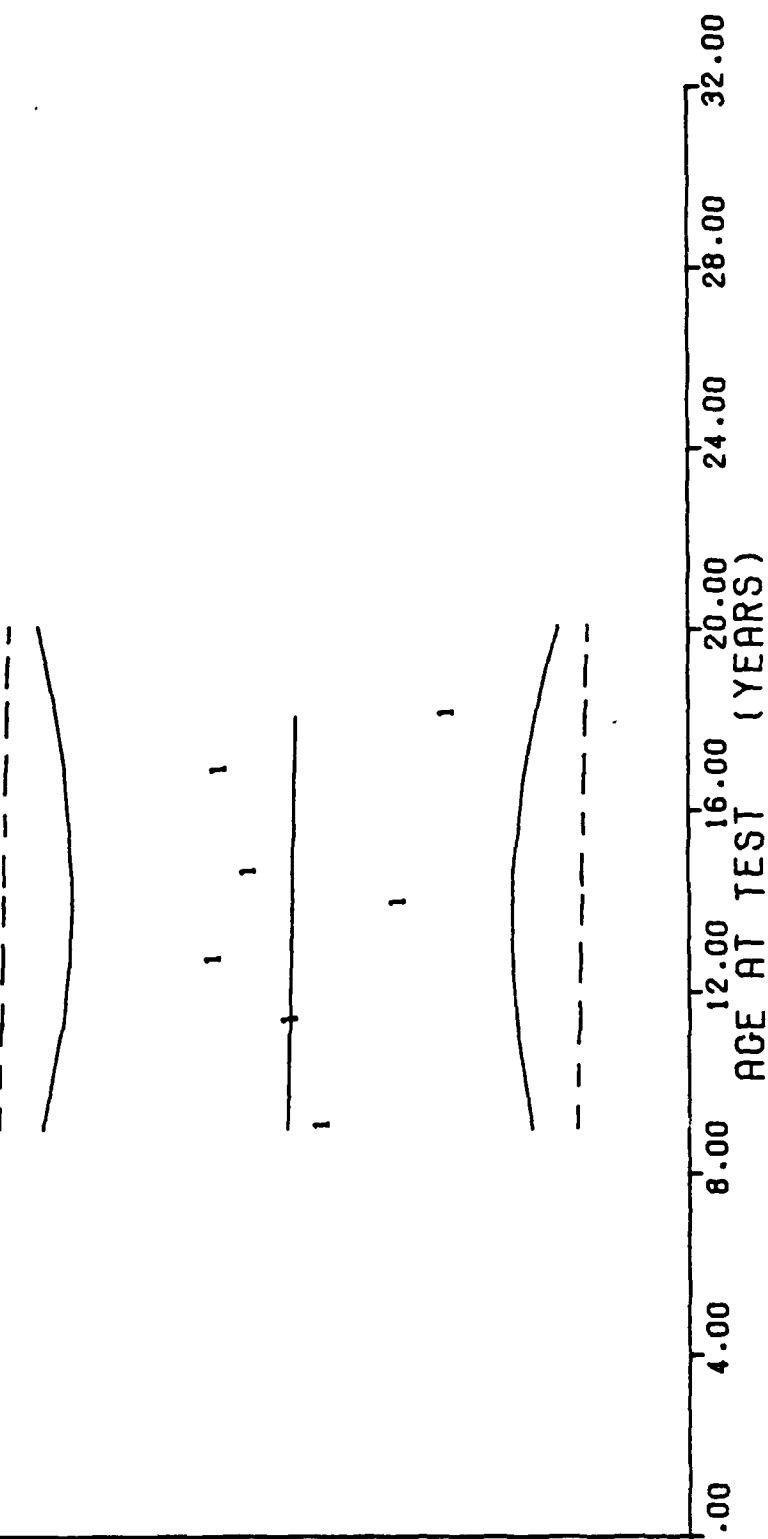
ANALYSIS	MEAN Y	MAXIMUM Y	MINIMUM Y	REGRESSION Y
1-5-0	4	+1.7065243E+00	+1.7069592E+00	+1.7058996E+00
1-6-0	4	+1.7853746E+00	+1.425350L-03	+1.7301395E+00
1-7-0	4	+1.7703237E+00	+1.0130530L-03	+1.7704992E+00
1-8-0	6	+1.7630653E+00	+1.2636602L-03	+1.760595L+00
1-9-0	6	+1.75e9160E+00	+1.2320593L-03	+1.750995E+00
1-0-0	6	+1.75e9160E+00	+1.7562999E+00	+1.7629985E+00
1-1-0	3	+1.7700366E+00	+1.1100144L-03	+1.7727594E+00
1-2-0	6	+1.7537488E+00	+2.4352323L-03	+1.7559995E+00
1-3-0	6	+1.7534329E+00	+2.1692241E-03	+1.7513999E+00

STAN. 1. • SELECTED ATTS. SOL GEL. DENSITY. Molar=091219.

$Y = ((+1.5450797E+03) + (-8.7754528E-03) * X) \quad * X)$
 $F = +9.1673333E-03 \quad$ SIGNIFICANCE OF F = NOT SIGNIFICANT $\sigma_F = +1.0270864E+01$
 $R = -2.4714009E-02 \quad$ SIGNIFICANCE OF R = NOT SIGNIFICANT $S_R = +9.1653282E-02$
 $L = +9.5746192E-02 \quad$ SIGNIFICANCE OF L = NOT SIGNIFICANT $S_L = +1.0604463E+01$
 $N = 17 \quad$ DEGREES OF FREEDOM = 15
 $N = 17 \quad$ STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = CAL/GRAM

PARAMETER = HEAT OF EXPLOSION



STAGE 1. DISSECTED MOTOR=0012199. HEAT RELEASED AT IGNITION.

Figure 43

$F = +1.5910074E+01$
 $R = +4.5189682E-01$
 $t^1 = +3.9887434E+00$
 $N = 64$
 $Y = ((+1.5245202E+03) + (+1.5460811E-01) ■ X)$
 $F = \text{SIGNIFICANCE OF } F$
 $R = \text{SIGNIFICANCE OF } R$
 $t^1 = \text{SIGNIFICANCE OF } t^1$
 $\text{DEGREES OF FREEDOM} = 62$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $\sigma_f = +1.5681608E+01$
 $s_b = +3.8761108E-02$
 $s_e = +1.4101460E+01$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

UNIT OF MEASURE = CAL/GRAM
 PARAMETER = HEAT OF EXPLOSION

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STAGE 1 DISSECTED MOTORS. HEAT OF EXPLOSION

Figure 43A

*** LINEAR REGRESSION ANALYSIS ***

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
108.0	1	+1.5396999E+03	+0.0000000E+07	+1.5396999E+03	+1.5396999E+03	+1.5441318E+03
136.0	3	+1.5433320E+03	+2.3155942E+00	+1.5436999E+03	+1.5430998E+03	+1.5438862E+03
152.0	3	+1.5517656E+03	+3.3417963E+00	+1.5540998E+03	+1.5487998E+03	+1.5437458E+03
167.0	3	+1.5314660E+03	+1.3515407E+01	+1.5470000E+03	+1.5235998E+03	+1.5436140E+03
175.0	3	+1.5477329E+03	+7.1416034E+00	+1.5551999E+03	+1.5410998E+03	+1.5435439E+03
202.0	3	+1.5510324E+03	+3.8773143E+00	+1.5548999E+03	+1.5485000E+03	+1.54333068E+03
217.0	1	+1.5258999E+03	+0.0000000E+07	+1.5258999E+03	+1.5258999E+03	+1.5431752E+03

STAGE 1, DISSECTED MOTOR=0012199. HEAT RELEASED AT IGNITION.

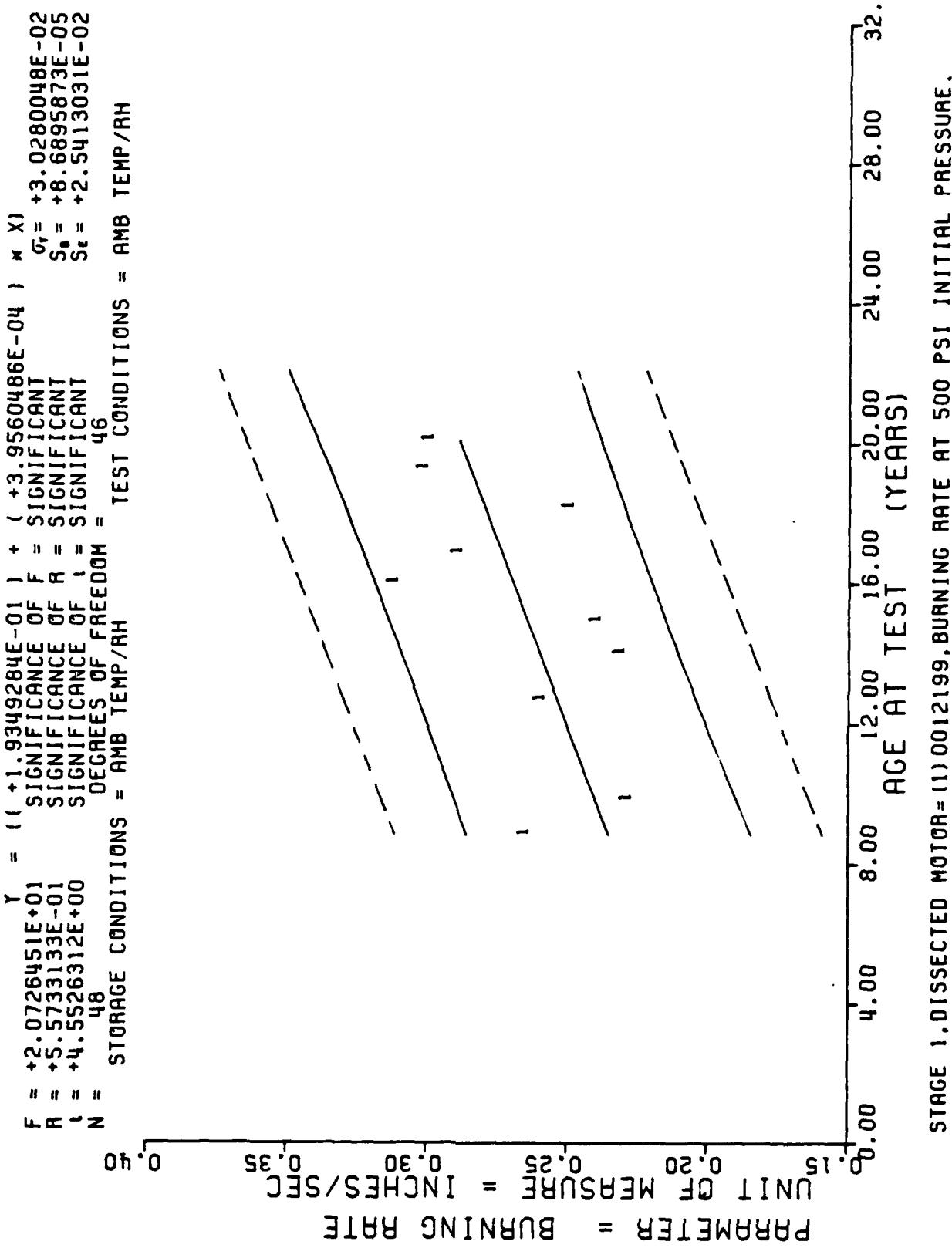


Figure 44

$\gamma = (1 + 2.5095226E-01) + (+ 4.9172293E-05) \quad * X$
 $F = +1.3598129E+00$ SIGNIFICANCE OF F = NOT SIGNIFICANT
 $R = +9.9496945E-02$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $t = +1.1661102E+00$ SIGNIFICANCE OF t = NOT SIGNIFICANT
 $N = 138$ DEGREES OF FREEDOM = 136
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

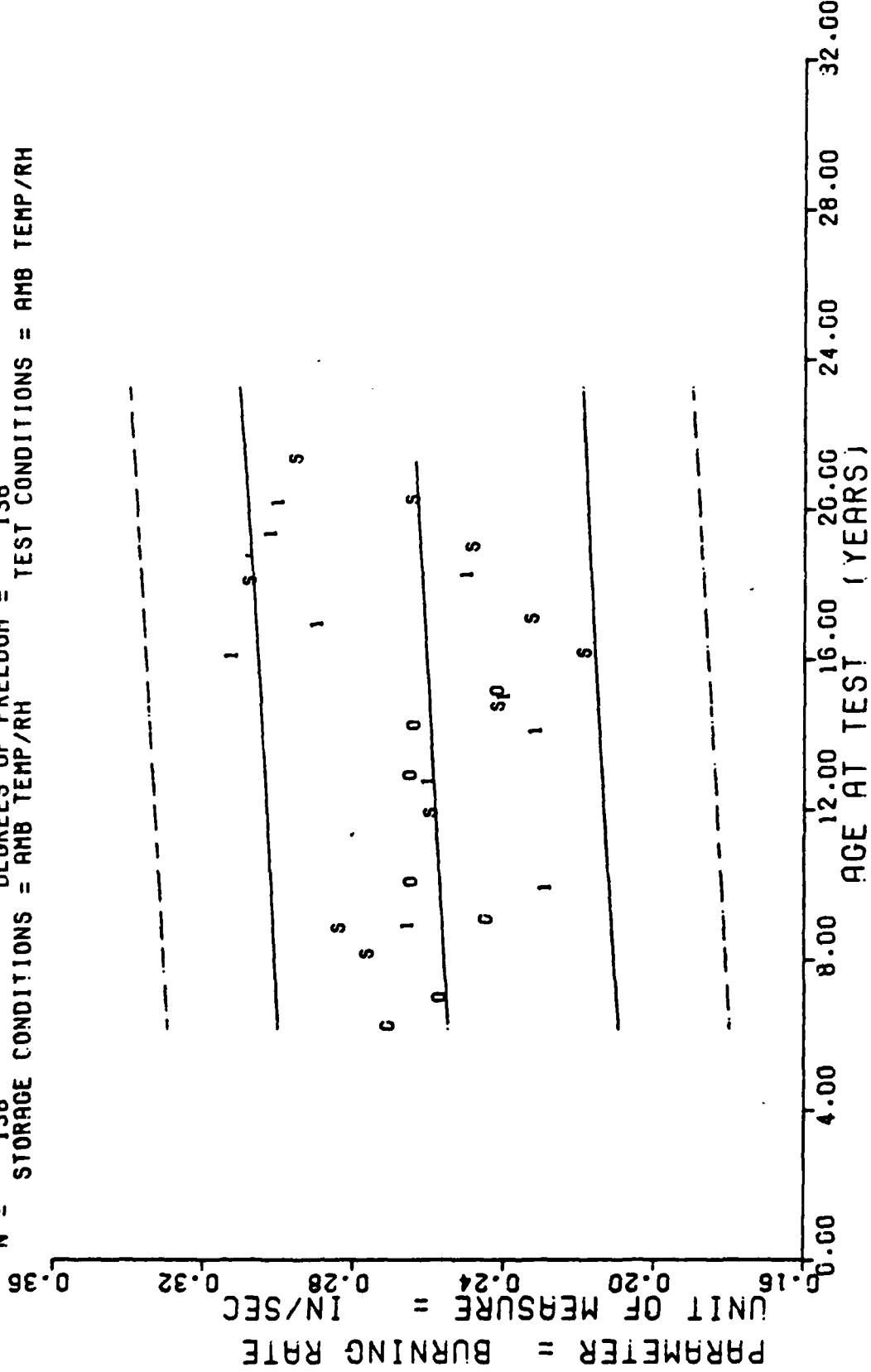


Figure 44A

**** LINEAR REGRESSION ANALYSIS ****

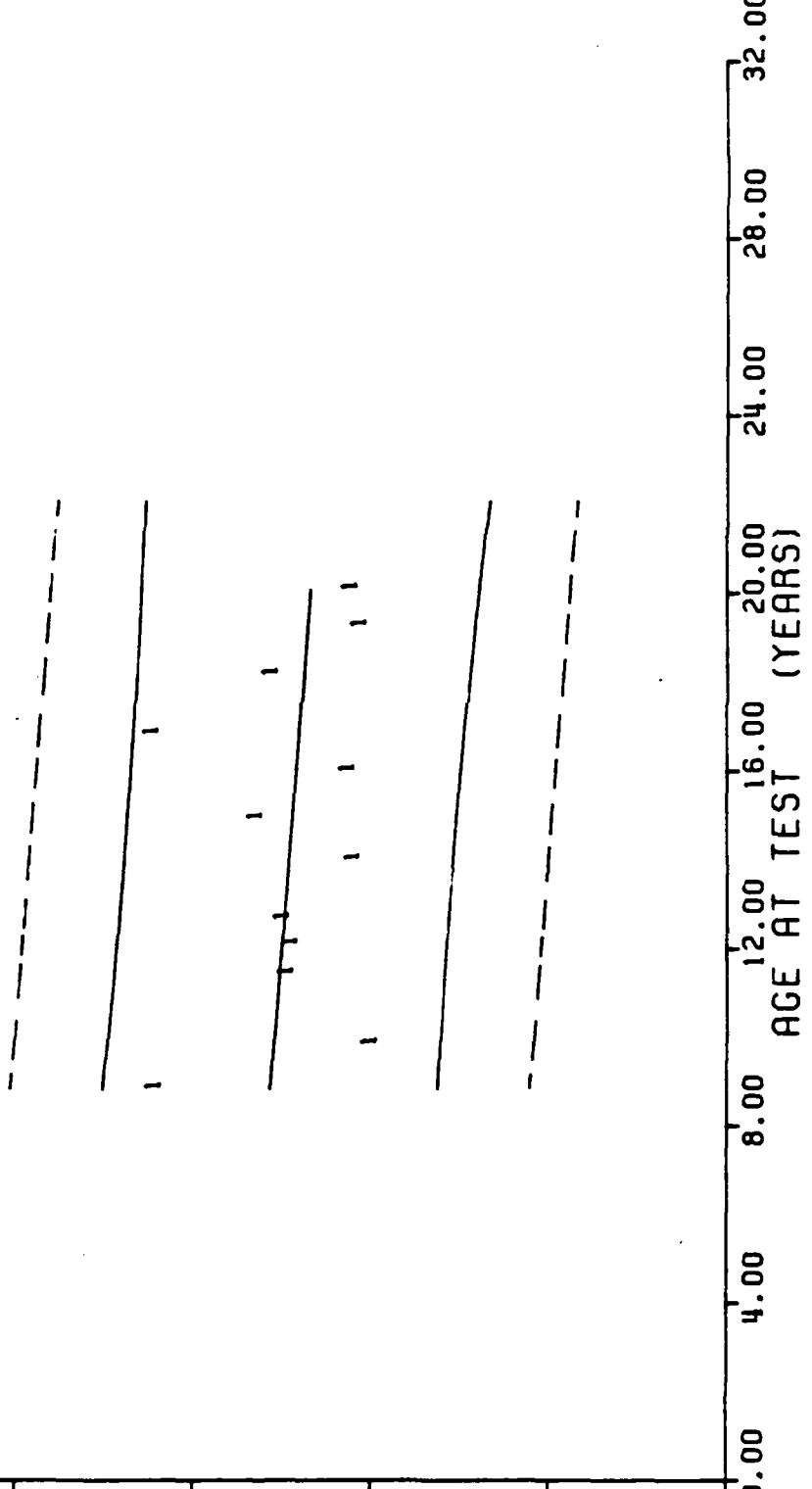
*** ANALYSIS OF TIME SERIES ***

A.U. (HOURS)	SPECIMNS PER GROUP	STANDARD		MAXIMUM Y	MINIMUM Y	REGRESSION Y
		MEAN Y	DEVIATION			
100.0	5	+2.6419979E-01	+2.2954995E-03	+2.6799994E-01	+2.6199996E-01	+2.3542690E-01
118.0	5	+2.2779977E-01	+4.9807506E-03	+2.3299998E-01	+2.2199994F-01	+2.4017417E-01
152.0	6	+2.5866651E-01	+2.3098162E-02	+3.0199998E-01	+2.4399995E-01	+2.5362473E-01
168.0	6	+2.3033314E-01	+7.9696300E-03	+2.4099999E-01	+2.1799999F-01	+2.5095445E-01
179.0	6	+2.3883306E-01	+1.6439691E-02	+2.7199995E-01	+2.2999995E-01	+2.6430606E-01
192.0	3	+3.1109994E-01	+3.7502346E-03	+3.1509995E-01	+3.0719995E-01	+2.6944893E-01
202.0	6	+2.8833305E-01	+6.8120972E-03	+2.9499995E-01	+2.7799999E-01	+2.7340501E-01
218.0	3	+2.4866664E-01	+1.1513481E-03	+2.5000000E-01	+2.4799996E-01	+2.7973467E-01
231.0	3	+3.0066663E-01	+3.0529920E-03	+3.0399996E-01	+2.9799997E-01	+2.8487753E-01
241.0	5	+2.9875981E-01	+4.3638794E-03	+3.0619996E-01	+2.9479998E-01	+2.8883355E-01

STAGE 1. DISSECTED MOTOR=(1)0012199, BURNING RATE AT 500 PSI INITIAL PRESSURE.

$F = +1.1795373E+00$ $\gamma = ((+3.0966317E-01) + (-6.7126388E-05) * X)$
 $R = -1.4000109E-01$ SIGNIFICANCE OF F = NOT SIGNIFICANT $\sigma_r = +1.9505418E-02$
 $t = +1.0860650E+00$ SIGNIFICANCE OF R = NOT SIGNIFICANT $S_a = +6.1806968E-05$
 $N = 61$ SIGNIFICANCE OF t = NOT SIGNIFICANT $S_t = +1.9476300E-02$
DEGREES OF FREEDOM = 59 TEST CONDITIONS = AMB TEMP/RH
STORAGE CONDITIONS = AMB TEMP/RH

PARAMETER = BURNING RATE
UNIT OF MEASURE = INCHES/SEC
0.24 0.28 0.32 0.36 0.40



STAGE 1 DISSECTED MOTOR = (1) 0012199. BURNING RATE AT 1000 PSI INITIAL PRESSURE.

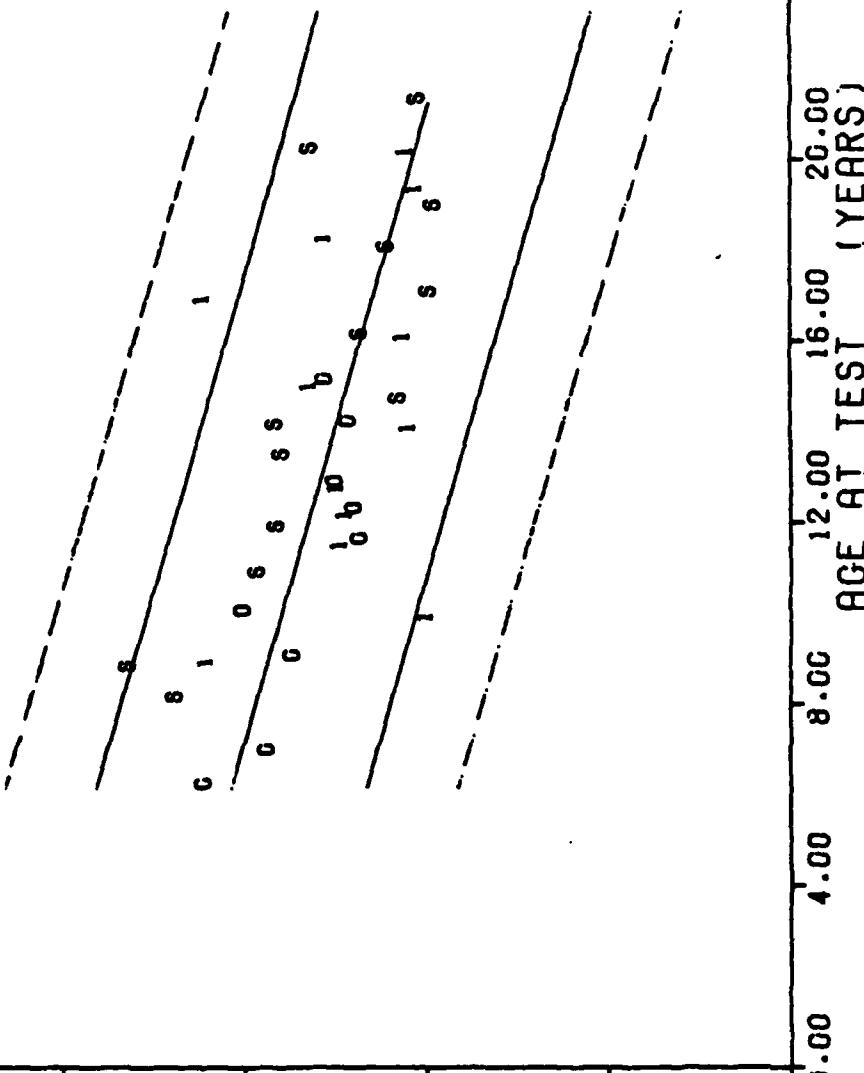
Figure 45

$y = ((+3.4068450E-01) + (-2.4042658E-04) * x) * X$
 $F = +7.6408177E+01$ SIGNIFICANT OF F = SIGNIFICANT
 $R = -5.5238982E-01$ SIGNIFICANT OF R = SIGNIFICANT
 $t = +8.7411771E+00$ SIGNIFICANCE OF t = SIGNIFICANT
 $N = 176$ DEGREES OF FREEDOM = 174 TEST CONDITIONS = AMB TEMP/RH

PARAMETER = BURNING RATE

UNIT OF MEASURE = IN/SEC

0.26 0.24 0.22 0.20 0.18 0.16 0.14 0.12 0.10 0.08 0.06 0.04 0.02 0.00



STAGE 1 DISCRETED MTRs=(0)0012099,(1)0012199,(S)STM-012,BURNING RATE AT 1000 PSI.

Figure 45A

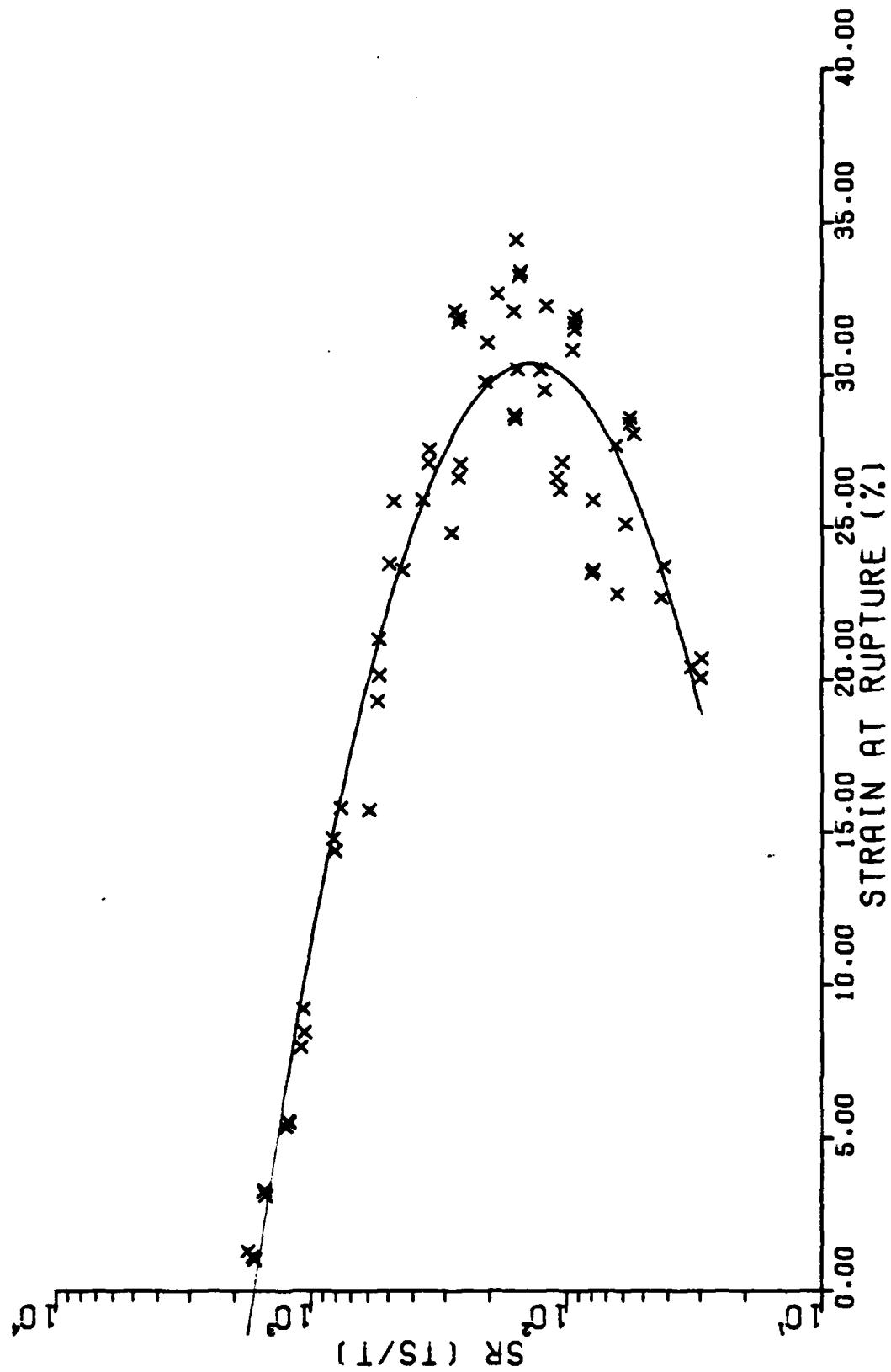
**** LINEAR REGRESSION ANALYSIS ****

*** ANALYSIS OF TIME SERIES ***

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
106.0	5	+3.2739979E-01	+5.4671778E-03	+3.3199995E-01	+3.20999997E-01	+3.0254775E-01
118.0	5	+2.7899968E-01	+7.4953729E-03	+2.8799998E-01	+2.7199995E-01	+3.0174225E-01
137.0	8	+2.9787468E-01	+4.1430658E-03	+3.0399996E-01	+2.9399996E-01	+3.0046683E-01
145.0	6	+2.9683303E-01	+4.5541523E-03	+2.999995E-01	+2.8799998E-01	+2.992979E-01
152.0	5	+2.9879987E-01	+1.4909735E-03	+3.0099999E-01	+2.9699999E-01	+2.9945993E-01
168.0	6	+2.8283292E-01	+9.2733389E-03	+2.9499995E-01	+2.7299994E-01	+2.9838591E-01
179.0	6	+3.0466634E-01	+3.3341548E-02	+3.6399996E-01	+2.7799999E-01	+2.9764753E-01
192.0	3	+2.8406661E-01	+2.0050004E-03	+2.8629994E-01	+2.8239995E-01	+2.9677486E-01
202.0	6	+3.2799971E-01	+1.0514737E-02	+3.3899998E-01	+3.1199997E-01	+2.9610359E-01
218.0	3	+3.0133324E-01	+2.3112752E-03	+3.0399996E-01	+2.9999995E-01	+2.9502958E-01
231.0	3	+2.8133326E-01	+5.6340067E-04	+2.3199994E-01	+2.8099995E-01	+2.9415696E-01
241.0	5	+2.8339976E-01	+1.1142458E-03	+2.8499996E-01	+2.8229999E-01	+2.9348570E-01

STAGE 1. DISSECTED MOTOR=(1)0012199, BURNING RATE AT 1000 PSI INITIAL PRESSURE.

TEMPERATURE CORRECTED FAILURE ENVELOPE



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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Testing was performed to determine the useful shelf/service life for LGM-30 Stage I Rocket Motors. A three year storage program for propellant and components was started in May 1961. This program was then extended to a ten year study and later continued indefinitely to assure that a deterioration in motor physical characteristics could be detected in time to take some corrective actions before the weapon system performance deteriorated below an acceptable level.		

This report covers propellant test data for motor S/N 0012199. Planned dissection of selected motors in the future will provide samples for continued component testing.

The data is presented in the form of regression analysis and the trends are projected 24 months beyond the last test date.

From the statistical analysis of all data tested to date, significant degradation of the propellant does not appear likely for at least two years past the oldest test point.

Future testing and reporting will be conducted on individual dissected motors.

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